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Victorian Geological Carbon Storage Initiative

Geological Carbon Storage in the Gippsland Basin, Australia Containment potential





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Geological Carbon Storage in the Gippsland Basin, Australia: Containment Potential

L.M. GOLDIE DIVKO, G.W. O'BRIEN, P.R. TINGATE & M.L. HARRISON

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Cover Image:

This image is a three-dimensional diagrammatic representation of the top surface of the Latrobe Group showing oil (green) and gas (red) accumulations, and the overlying regional top seal: the Lakes Entrance Formation. The view is from the sub-surface offshore Gippsland Basin looking towards the northwest onshore section of the basin and the Strzelecki Ranges in the distance.

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An interpretation of top seal potential at a basin scale, Gippsland Basin.

Executive Summary

The Gippsland Basin is widely viewed as the prime site for the development of a large-scale geological CO₂ storage industry in Victoria. To facilitate this, GeoScience Victoria's Victorian Geological Carbon Storage project is providing a detailed geological assessment of the basin's suitability for geological carbon storage. In this study, the top seal potential of the Lakes Entrance Formation in the Gippsland Basin has been evaluated to provide a basin-scale understanding of the region's potential for CO₂ containment.

Thickness, distribution, facies and Mercury Injection Capillary Pressure data from the Lakes Entrance Formation suggest that the base of the unit within the Central Deep, western Northern Terrace and the onshore Lake Wellington Depression has excellent containment characteristics, with the capacity to withhold a vertical column of CO₂ hundreds of metres high. The sealing potential of the Lakes Entrance Formation on the Southern Terrace and Southern Platform is very good. The formation is thick and seal capacity results from Groper-1 (246 m of CO₂) indicate that the seal has the potential to contain significant column heights of CO₂. The Seaspray Depression and Northern Terrace have good to moderate sealing potential. In these locations, the seal thickness and the depth to the base of the formation is variable. Seal capacity results are also variable but generally much lower than those recorded in the Central Deep. The offshore Northern Platform and the onshore Lakes Entrance Platform, Baragwanath Anticline and Alberton Depression offer very little containment potential for injected CO₂. 5

The results of the present study, when integrated with the results from other VicGCS investigations, will provide a basin-scale understanding of the Gippsland Basin's CO₂ geological storage potential.

1 Introduction

Victoria's brown coal resources in the Latrobe Valley are currently used principally for low-cost electricity generation, which is a key component for Victoria's manufacturing and industrial base. In addition, the potential exists to significantly expand the utilization of brown coal and to develop new value-added industries, such as coal-to-liquids. The pressing need to reduce carbon emissions means, however, that the usage of the coal resources in the future, will probably be contingent on reducing the coal industry's greenhouse footprint over the next 10 to 20 years.

Geological carbon storage (GCS) is a key enabling technology, which could allow the ongoing and potentially expanded exploitation of Victoria's massive brown coal resources. GCS involves the capture of CO₂ from sources such as power stations, coal-to-liquids plants and gas production from high-CO₂ gas fields, the transport of the captured CO₂ and finally, its injection in the sub-surface. Prior to transport and injection, the captured CO₂ is pressurised into a "super-critical" state (essentially a fluid somewhat less dense than water). Provided that the supercritical CO2 is injected into geological formations deeper than approximately 800 m, the CO2 will remain supercritical. Eventually, over thousands of years, the majority of the CO2 will dissolve into the formation waters or be trapped in crystallizing mineral phases. However, if the injected CO₂ should migrate to depths shallower than 800 m, the supercritical CO₂ phase transitions into a gas phase which has very different characteristics. This CO₂ gas phase can migrate much more quickly than supercritical CO₂ and it is also more difficult to contain under regional sealing units.

The most obvious site for the geological carbon storage of CO₂ generated in the Latrobe Valley is the Gippsland Basin. The Gippsland Basin has high quality Late Cretaceous and Cenozoic siliciclastic reservoirs, and has been the site of active petroleum exploration and production for over nearly forty years. Many of the oil fields within the basin are now near the end of their production lives, and hence the opportunity exists to develop areas previously used for petroleum production for GCS. However, such a process would effectively turn the basin's pore space into a multiple use zone, at least in the short to medium term. Management of potential conflicts between incumbent and future hydrocarbon producers and explorers within the basin and the needs of CO₂ emitters, and the wider society, to reduce emissions to meet mandated targets, will provide significant challenges into the future.

VicGCS (Victorian Geological Carbon Storage) is a four-year (2008-2013), \$5.2 million multi-disciplinary initiative that will characterise the geosequestration

potential of the offshore and onshore Gippsland Basin. The program will be delivered by GeoScience Victoria in partnership with key external organisations. A key goal of the VicGCS Project is to develop a sufficient geological knowledge of the onshore and offshore Gippsland Basin to allow the development and management of the region as a key GCS hub. Management of the region as a genuine multiple use zone will be an essential component – and challenge – of the project. The VicGCS project will assess the GCS potential of the Gippsland Basin under three technical themes, namely containment (sealing potential), injectivity-capacity (reservoir character and distribution) and impacts (migration characteristics).

This report specifically addresses the containment theme for the Gippsland Basin. The containment theme deals principally with key aspects of the integrity of the regional top-seal, the Lakes Entrance Formation, which spans the offshore and parts of the onshore basin. The key objective of this work is to determine where the Lakes Entrance Formation provides an effective top-seal for oil, gas and any injected CO₂ and where it does not. From a GCS viewpoint, the simple question is: 'If the CO₂ is put in, will it stay in?'

Investigations of the thickness, geometry and seal capacity of the Lakes Entrance Formation are presented, as is an interpretative sedimentary facies framework. Results include Mercury Injection Capillary Pressure (MICP) data from 37 wells in the Gippsland Basin, which have allowed a regional quantitative assessment of the sealing capacity of the Lakes Entrance Formation to be made. In addition, a secondary part of the containment theme is a brief consideration of the importance of intra-Latrobe sealing units within the basin, as well as subsidiary units which also act as top seals, such as the Gurnard Formation. Existing leakage and seepage data have been integrated with seal capacity results to produce a qualitative assessment of the seal potential of the Gippsland Basin.

This study focuses on the capillary properties of the seal. There is no evidence that, at a first-order, faulting or mechanical reactivation of the top sealing unit is an important control on seal potential in the Gippsland Basin. This aspect will, however, be further investigated in other VicGCS modules.

This report initially provides an overview of the regional geology of the Gippsland Basin. This is followed by a detailed evaluation of the sealing characteristics of the regional seal - the Lakes Entrance Formation, a subsidiary top seal - the Gurnard Formation and various intra-formational seals. These data are then combined into a new interpretative framework which presents a mapbased evaluation of the top seal potential at a basin-scale.

2 Regional Geology

The Gippsland Basin, one of Australia's most prolific hydrocarbon provinces, is situated in south-eastern Australia and is located about 200 km east of the city of Melbourne, Victoria.

The basin, which has both onshore and offshore elements, is a world-class hydrocarbon province and contains several giant oil and gas fields. The vast majority of the discoveries are reservoired within the siliciclastics of the Late Cretaceous to Paleogene Latrobe Group and almost all of the currently producing fields are located offshore in shallow water.

The details of the basin's tectonic evolution and its stratigraphic fill are provided in the following sections.

2.1 Tectonic Evolution of the Gippsland Basin

The east-west trending Gippsland Basin was formed during the break-up of Gondwana (Rahmanian et al., 1990; Willcox et al., 1992; Willcox et al., 2001; Norvick & Smith, 2001; Norvick et al., 2001) and the basin evolution is recorded by several depositional sequences that range from Early Cretaceous to Recent in age. The profound tectonic control on sedimentary systems in the basin is exemplified by several basin-wide angular unconformities that are easily recognised on seismic sections. Other timebreaks are only recognised using biostratigraphic age determinations delineating missing sections. This is of particular relevance in the context of the upper Latrobe Group, where extensive channel incision and subsequent infill processes resulted in complex sedimentary sequences that developed at slightly different time intervals, the extent of which cannot be resolved by seismic mapping alone.

As part of the Early Cretaceous rift system between Antarctica and Australia, the Gippsland Basin architecture initially featured a rift valley complex composed of multiple E-W trending half-grabens. Continued rifting into the Late Cretaceous generated a classic extensional geometry comprising a depocentre (the Central Deep) flanked by platforms and terraces. These are defined by the Rosedale and Lake Wellington Fault systems on the northern basin margin and by the Darriman and Foster Fault systems on the southern margin (Figure 2.1). The Central Deep is characterised by rapidly increasing water depths to the east that exceed 3,000 m in the Bass Canyon (Hill *et al.*, 1998). The Cape Everard Fault System, a prominent NNE-striking basement high evident on total magnetic intensity imagery (Moore & Wong, 2001), defines the eastern boundary of the basin. The western onshore extent of the basin is traditionally placed at the Mornington High, but for the units described in this report it is essentially represented by outcrops of Early Cretaceous Strzelecki Group sediments (Hocking, 1988). 7

Initial rifting in the Early Cretaceous resulted in 30% crustal extension (Power et al., 2001) and created a complex system of grabens and half-grabens. A compressional phase accompanied by uplift between 100 and 95 Ma, which has been linked to the separation of Australia from Antarctica (Duddy & Green, 1992), produced a new basin configuration and provided the accommodation space for large volumes of basement-derived sediments. Renewed extension during the Late Cretaceous, associated with the opening of the Tasman Sea, established the Central Deep as the main depocentre. Late Santonian sediments in the eastern part of the basin record the first marine incursion (Partridge, 1999). Many of the earlier generated faults were reactivated during this tectonic phase.

A margin-sag basin, characterised by rapid subsidence, followed the crustal rifting. Extensional tectonism prevailed until the early Eocene and produced pervasive NW-SE trending normal faults. By the middle Eocene, sea-floor spreading had ceased in the Tasman Sea and a compressional period began to affect the Gippsland Basin initiating a series of NE to ENE-trending anticlines (Smith, 1988). Compression and structural growth peaked in the middle Miocene and resulted in basin inversion. All the major fold structures at the top of the Latrobe Group which became the hosts for the large oil and gas accumulations, such as Barracouta, Tuna, Kingfish, Snapper and Halibut, are related to this tectonic episode.

Tectonism has continued to overprint the basin as documented by localised uplift during the late Pliocene to Pleistocene. This is also reflected in the uplift of Pliocene sediments on the Barracouta, Snapper and Marlin anticlines as well as around Lakes Entrance. Ongoing episodical tectonic activity is recorded by seismic events around the major basin bounding faults.



Figure 2.1 Structural elements map of Gippsland Basin, showing distribution of oil and gas fields.



Figure 2.2 Stratigraphic column for the Gippsland Basin, showing petroleum system elements and tectonic evolution (after Bernecker & Partridge, 2001).

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2.2 Stratigraphy and Depositional History

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Based on lithological variations, three broad stratigraphic successions are recognised in the Gippsland Basin (Figure 2.2). These stratigraphic groups comprise a) the Strzelecki Group, a thick sequence of non-marine, volcanoclastic-rich sediments; b) the Latrobe Group, a sequence of marine and non-marine siliciclastics that host all the known hydrocarbon occurrences in the offshore; and c) the Seaspray Group, a carbonate-dominated sequence that is the regional seal to the top-Latrobe Group oil and gas accumulations.

Strzelecki Group

The Strzelecki Group represents syn-rift sedimentation and unconformably overlies Palaeozoic igneous and folded sedimentary rocks. The group consists dominantly of interbedded lithic, volcanoclastic sandstones and mudstones, including several coal-rich horizons. The sediments accumulated in a non-marine environment under a fluvial depositional regime. The Strzelecki Group has strong affinities with the Otway Group in the Otway Basin (Duddy & Green, 1992). The group is regarded by the industry as 'economic basement', although considered to have potential for hydrocarbon generation and accumulation, in particular in the western part of the basin (Mehin & Bock, 1998). In fact, onshore the gas accumulations of the North Seaspray and Gangell fields are reservoired in the Strzelecki Group. The total thickness of the Strzelecki Group is ill-defined, but is likely to exceed 1500 m (Gilbert & Hill, 1994).

Latrobe Group

The Latrobe Group hosts all currently known hydrocarbons in the offshore. Four subgroups are discriminated, each of which is bound by basin-wide unconformities and each consists of formations that are distinguished according to their main depositional facies assemblages.

Emperor Subgroup

The Emperor Subgroup (Bernecker & Partridge, 2001) has only been intersected around the basin margins in the vicinity of the bounding faults of the Northern and Southern terraces. Seismic data suggests that a thick section of the subgroup exists below depths of 4 to 6 km in the Central Deep (Bernecker & Partridge, 2001). The Otway Unconformity, separating the subgroup from the underlying Strzelecki Group, developed in response to uplift along the basin margins. Large amounts of erosional material were delivered to the evolving rift-valley in which one or several deep lakes emerged as the depocentre. The Emperor Subgroup comprises coarse-grained alluvial fan/plain as well as lacustrine facies associations that are characteristic of rift-valley deposition prior to continental break-up. The Kersop Arkose (Bernecker & Partridge, 2001), a coarsegrained to conglomeritic quartz and feldspathic sandstone, was derived from erosion of uplifted granites beyond the faults bounding the Central Deep. The Admiral Formation (Bernecker & Partridge, 2001) overlies but may also be laterally equivalent to the Kersop Arkose. It is characterised by quartz-dominated lithic arenites that were derived from Palaeozoic sedimentary and metamorphic terrains as well as from newly uplifted early Cretaceous sediments. The Kipper Shale (Lowry & Longley, 1991) represents lacustrine deposition and is dominated by mudstones with intercalated fine- to medium-grained sandstones (Marshall & Partridge, 1986; Marshall, 1989; Lowry & Longley, 1991). The palaeolake, or lakes, presumably occupied most of the Turonian riftvalley and received detrital sediments from the basin margins as distribution of the formation is widespread (Bernecker & Partridge, 2001). The Curlip Formation (Bernecker & Partridge, 2001) consists of sandstones and conglomerates that are interbedded with thin shales and minor coals. The formation overlies and interfingers with the Kipper Shale; the top marked by the basin-wide Longtom Unconformity that terminates Emperor Subgroup deposition. Prior to its recognition (Partridge, 1999), this unconformity was previously merged or confused with the Seahorse Unconformity at the top of the Golden Beach Subgroup. Accordingly, numerous well intervals were erroneously assigned to the former Golden Beach Group. The hiatus between the Emperor and Golden Beach subgroups separates non-marine freshwater lacustrine sediments from marine sediments and correlates with the opening of the adjacent Tasman Sea.

Golden Beach Subgroup

The Golden Beach Subgroup (formerly Golden Beach Group of Lowry & Longley, 1991) is essentially confined to the Central Deep, reflecting tectonic movement along the basin margins where conglomerates accumulated. Finer material was transported by fluvial systems that continued to migrate across a gradually widening lower coastal plain and terminated as deltaic bodies in a shallow sea. Alternation between marine and non-marine influence persisted throughout the remainder of deposition of the Latrobe Group and had great control on the distribution of petroleum system elements. Two formations are distinguished within the Golden Beach Subgroup: the marine Anemone Formation and the fluvial/paralic Chimaera Formation. The Anemone Formation consists predominantly of mudstones (shales) and finegrained siliciclastics representing shallow to open marine deposition that prevailed in the eastern part of the basin (Bernecker & Partridge, 2001). The Chimaera Formation (formerly the Chimaera Sandstone of Lowry & Longley, 1991) is a nonmarine succession that comprises coarse-grained alluvial/fluvial sediments as well as fine-grained floodplain deposits including some coals (Bernecker & Partridge, 2001). The formation has been intersected in wells near the Rosedale Fault System but is absent from the Northern Platform and Northern Terrace: the formation is found as far south as Omeo-1, -2A and Perch-1.

The Golden Beach Subgroup also contains several volcanic horizons that have been identified as Campanian. These volcanics, most prominently developed in the Kipper Field and in the Basker/Manta/Gummy area, terminate the Golden Beach Subgroup and signal another depositional hiatus represented by the Seahorse Unconformity. The time gap recorded by the Seahorse Unconformity is longest in Golden Beach West-1, where the Upper F. longus biozone directly overlies N. senectus sediments. Closer to the Rosedale Fault System, F. longus sediments overlie the Campanian volcanics (Bernecker & Partridge, 2001).

Halibut Subgroup

The Halibut Subgroup hosts the bulk of the hydrocarbons in the Gippsland Basin and comprises five formations that are distinguished according to their dominant depositional facies regimes. These formations document the changes from non-marine to marine environments in a west-east or onshoreoffshore direction. The Barracouta Formation (revised and formalised by Hocking, 1976a) is characterised by fluvial claystones, siltstones and sandstones and minor coals and was deposited on an upper coastal plain. The Volador and Kingfish formations comprise the typical lower coastal plain coal-rich sediments and are separated by the Kate Shale (Partridge, 1999). The Kate Shale is a marine interval recognised at the Cretaceous/Cenozoic boundary. It is intersected in wells in the eastern portion of the offshore basin and is regarded as a good sealing lithology. The Mackerel Formation consists of nearshore marine sandstones, commonly typified by excellent reservoir qualities, with intercalated marine shales.

Sea-level fall in the early Eocene, driven by basin inversion, initiated a period of major canyon cutting during which parts of the lower coastal plain and the shelf were eroded. The array of submarine channels that developed has added a considerable complexity to seismic mapping, given that the major channels cut down hundreds of metres into the underlying strata. During subsequent transgression, the channels were filled with marine sediments (e.g. Flounder Formation) leading to the generation of potential stratigraphic hydrocarbon traps (Johnstone *et al.*, 2001). The Marlin Unconformity highlights the major erosional event associated with channel incision, terminating deposition of the Halibut Subgroup. 11

Cobia Subgroup

The middle Eocene to early Oligocene Cobia Subgroup (formerly the Cobia Group of Thompson, 1986) comprises the coal-bearing lower coastal plain facies of the Burong Formation (Partridge, 1999) and the shallow to open marine Gurnard Formation (James & Evans, 1971). The Gurnard Formation is a condensed section composed of fine- to mediumgrained glauconitic siliciclastics. Also included in the subgroup is the Turrum Formation (James & Evans, 1971) that consists of mid-Eocene marine channel-fill sediments. Deposition of the Cobia Subgroup ceased during the early Oligocene, as a consequence of a marked decline in sediment supply. Large areas of the central basin were left with starved or condensed sections, which led to the development of what is traditionally known as the 'Latrobe Unconformity' (Partridge, 1999). On seismic sections, this surface is expressed by a prominent reflector marking the boundary between siliciclastic and calcareous rocks. This reflector is commonly interpreted as a time-line, however, biostratigraphic data clearly indicates that the Latrobe Unconformity should be considered a composite of several, separate erosional events (Partridge, 1999).

Seaspray Group

The Seaspray Group consists of calcareous sediments that unconformably overlie the siliciclastics of the Latrobe Group. Subsequent to a change in ocean circulation along the southern Australian margin, the accumulation of marls and limestones began in the middle Eocene in the Eucla Basin, extended to the Otway Basin during the late Eocene, reaching the Gippsland Basin during the early Oligocene (Holdgate & Gallagher, 1997). Since then, cool-water carbonate production resulted in progradation of the shelf edge. In petroleum geological terms, the Seaspray Group, in particular the Lakes Entrance Formation, is considered a basinwide, high quality regional top seal to the oil and gas accumulations at the top-Latrobe Group reservoirs.

Lakes Entrance Formation

The Lakes Entrance Formation is the lowermost unit of the Seaspray Group and is composed predominantly of calcareous mudstones, with some variation in composition across the basin. The recognition of major lateral facies changes has allowed the formation to be subdivided into separate onshore and offshore components.

Onshore, the Cunningham Greenstone Member, Giffard Sandstone Member, Colquhoun Sandstone Member, Seacombe Marl and the Metung Marl are identified as constituent units of the Lakes Entrance Formation (Hocking 1976a). The constituent

formations of the onshore Seaspray Group have been divided into nine sequence stratigraphic units based on microfossil evidence (Holdgate & Gallagher, 1997). Offshore, four distinct units within the Seaspray Group are identified (Bernecker et al., 1997) according to well-log character, lithological composition and depositional facies. 'Unit I', a hemipelagic fossiliferous mudstone, is equivalent to the onshore marly Lakes Entrance Formation (Bernecker et al., 1997) and part of the offshore Lakes Entrance Formation (T. Bernecker pers. comm. Geoscience Australia, 2007). 'Unit I' of the Seaspray Group was formalised by establishing a new formation name, the Swordfish Formation (Partridge, 1999). The Swordfish Formation was identified by Partridge (1999) in a small number of wells in the Central Deep. For the purpose of this containment study, no attempt has been made to differentiate between the Lakes Entrance Formation and the Swordfish Formation. Perhaps that differentiation might be required for more detailed studies in the future.

Gippsland Limestone

The Gippsland Limestone is a thick sequence of marine carbonates comprised of fossiliferous limestones, marly limestones and marls which overlie the Lakes Entrance Formation in the offshore and onshore Gippsland Basin (Gallagher & Holdgate, 1996). There is a major increase in carbonate content from the Lakes Entrance Formation to the Gippsland Limestone (Holdgate & Gallagher, 2003). Onshore, the Gippsland Limestone is divided into members (Hocking, 1976b) that outcrop locally around the Baragwanath Anticline. The formation thickness onshore exceeds 500m (Gallagher & Holdgate, 1996), whilst offshore, may attain a thickness of more than 1500m (James & Evans, 1971). The Gippsland Limestone is early to middle Miocene in age (e.g. Hocking, 1976a). Marine carbonate trangressive and highstand systems tracts have been identified in the onshore Lake Wellington Depression through the integration of seismic, wireline log and micropalaeontological data (Gallagher & Holdgate, 1996; Holdgate & Gallagher, 1997).

Onshore, in the Lake Wellington and Seaspray Depressions, a marine sequence of middle Miocene to Pliocene aged sediments rests unconformably on the Gippsland Limestone. This sequence is comprised of the Wuk Wuk Marl, Bairnsdale Limestone, Tambo River Formation and Jemmys Point Formation.

3 Seal Analysis

The Lakes Entrance Formation provides the primary regional top seal for the majority of the hydrocarbon resources at the top of the Latrobe Group in the Gippsland Basin. The focus of this report study is on determining the Lakes Entrance Formation's seal potential at a basin scale; sealing potential is derived in part from an understanding of its characteristics (distribution, lithology, sedimentary facies, thickness, capillary properties) across the basin.

At the basin margins, particularly onshore where the Lakes Entrance Formation is absent, it is worthwhile investigating whether or not the overlying Gippsland Limestone may provide an adequate top seal. Although a complete analysis of the Gippsland Limestone is not yet completed, some initial results are presented in this report. As yet, there has been no attempt to map the distribution of the Gippsland Limestone, especially onshore, although the distribution of the Seaspray Group has been mapped previously (Gallagher & Holdgate, 1996).

A brief overview of Latrobe Group sealing units is included in this report as these units may contribute to the overall seal potential of the basin. Latrobe Group top seals: the Gurnard, Burong and Turum formations of the Cobia Subgroup and intraformational seals of the Halibut, Golden Beach and Emperor subgroups may act as important barriers or baffles to increase the length of the flowpath of injected supercritical CO₂. The lateral extent of most Latrobe Group seals is likely to be restricted and their containment potential is therefore probably poor at a regional scale. However, more widespread marine units such as the Kate Shale (Halibut Subgroup) are more likely to contribute to the overall sealing potential of the offshore Gippsland Basin.

3.1 Previous Work

Data relevant to the assessment of sealing process in the Gippsland Basin have been collected over the last forty years as part of petroleum exploration activity. In recent years, these investigations have focussed on evaluating the Lakes Entrance Formation for top seal potential and local Latrobe Group intra-formational seals as possible barriers/baffles to the flow of injected supercritical CO₂ in the Gippsland Basin.

Daniel (2005) completed a seal capacity study of the Gippsland Basin as part of the CO2CRC Latrobe Valley CO₂ Storage Assessment Program. A seal capacity study was produced to complement reservoir and other technical evaluations of the Gippsland Basin for the purpose of geological CO₂

storage (e.g. Root *et al.,* 2004; Gibson-Poole *et al.,* 2005; Gibson-Poole *et al.,* 2008).

Daniel (2005) determined column retention heights for CO₂ from Mercury Injection Capillary Pressure (MICP) analysis of 31 sealing lithology core samples from wells in the Central Deep of the Gippsland Basin. Top seal and intraformational sealing facies from the Latrobe Group were analysed. Core samples from the Lakes Entrance Formation regional top seal had CO₂ retention capacities ranging from 17 m for transgressive inner shelf facies to 1070 m for high-stand, outer shelf facies. Local top seals from the Cobia Subgroup had variable sealing capacities: the Gurnard Formation could retain only 0.2 m of CO2 in Bream-2 but up to 723 m in Kingfish-9; the Turrum Formation in Wrasse-1, could retain a 670 m column of CO₂. Seal capacity values associated with the Latrobe Group intraformational seals of the Halibut Subgroup ranged from 52 m in the Kingfish Formation to 961 m in the Mackerel Formation. The areal extent of these seals is largely unknown, with the estimates based on the likely extent of the facies which the seals represented.

In 2008, GeoScience Victoria carried out an initial assessment of containment potential for the purpose of carbon capture and storage as part of a wider study of the petroleum systems in the Gippsland Basin (O'Brien *et al.*, 2008). Hydrocarbon and CO₂ column retention heights were determined for the Lakes Entrance Formation from 16 core samples taken from wells in both the onshore and offshore portions of the basin. The thickness, geometry and a simple facies map of the Lakes Entrance Formation regional top seal were used to infer seal capacity across the basin at, or as close as possible to, the base of the formation.

From thickness, distribution and MICP capacity data for the Lakes Entrance Formation O'Brien et al. (2008) determined the base top seal within the Central Deep to have excellent containment characteristics, with the capacity to withhold hundreds of metres of gas or CO₂. The flanking Northern and Southern terraces were found to have lesser, but still adequate containment, with the potential to withhold 50-100 m gas being proven on parts of the Northern Terrace. In contrast, the Northern and Southern platforms were considered to have very poor sealing characteristics; with sealing capacity decreasing to only 5 m of gas and 13 m of CO₂ at Groper-2. Onshore, within the Lake Wellington and Seaspray depressions the relatively thick top seal was considered to offer good containment. However, outside these areas, the Lakes Entrance Formation onshore was found to have generally poor MICP characteristics and therefore, inadequate containment.

In the early 1990s, Petrofina conducted, as part of their petroleum exploration program in the eastern offshore Gippsland Basin, an evaluation of Latrobe Group intra-formational sealing lithologies. An assessment of the Late Cretaceous Golden Beach Subgroup and the Volador Formation of the Halibut Subgroup aimed to quantify seal capacity through MICP analysis of core and cuttings samples from six wells (Martin, 1992). In a separate report, the most effective sealing lithologies and facies were identified in an effort to better understand the occurrence of hydrocarbons in the eastern offshore Gippsland Basin (Jalfin, 1994). Offshore shale facies were found to have very high sealing capacities, with the ability to retain hydrocarbon columns of around 1300 m. Lower shoreface facies had lesser capacities of 110 m, perhaps due to associated textural variations (Jalfin, 1994). The offshore shale facies were found to be much thicker and widely distributed than paludal and floodplain facies. Ductility tests revealed that the interstratified brittle and ductile rocks of lagoon/paludal facies could prove to be a major risk to seal integrity (Jalfin, 1994).

Over the last three decades, numerous airborne and ground surveys were conducted to detect hydrocarbon leakage or seepage in the offshore and onshore Gippsland Basin. The results obtained from these surveys are relevant to the assessment of containment potential as hydrocarbon seeps are unequivocal indicators of a failing top seal.

3.2 Seal Thickness and Geometry

Lakes Entrance Formation

Initially, a review of Lakes Entrance Formation tops was completed in order to ascertain formation thicknesses (see Appendix 1). A previous GeoScience Victoria compilation of formation tops from 155 wells in the offshore Gippsland Basin provided the basis for this review. The top of the Lakes Entrance Formation was refined in 43 of these wells. Some were reviewed because well tops and formation thicknesses in adjacent wells where inconsistent although structural data and well completion report information suggested no reason for large differences. In other wells, channel bases were erroneously identified as the top of the Lakes Entrance Formation, and in some, formation thicknesses were unreasonable [i.e. too thick for average accumulation rates (see Bernecker et al, 1997)]. The top of the Lakes Entrance Formation was then identified or compiled for an additional 111 wells. Well completion report lithology descriptions and wireline logs were used to determine the presence/absence of the formation onshore. In some areas onshore, the base of the Lakes Entrance Formation is considered a reservoir rather than a

seal (e.g. the Lakes Entrance Platform). In this area, it is therefore likely that true seal thickness may be less than the formation thickness and that further review may be warranted.

In general, the thickness of the regional seal increases from the onshore to the offshore portion of the Gippsland Basin (Figure 3.1). Onshore, the thickness of the Lakes Entrance Formation ranges between 19 and 176 m; it is thickest in the Lake Wellington and Seaspray depressions. Relative to the onshore, the average thickness of the Lakes Entrance Formation is increased nearshore and on the southern and northern platforms offshore. The formation attains its greatest thickness in the offshore Central Deep, reaching a maximum of 430 m; it is thinner on the flanking Southern and Northern terraces. In general, the Lakes Entrance Formation is between 100 to 200 m thick over the north-western gas fields (i.e. Barracouta, Snapper and Turrum) and 200 to 300 m thick over the eastern fields (i.e. Tuna, East Pilchard, Basker and Gummy) and the south-eastern oil fields (i.e. Kingfish, Fortescue, Cobia, Halibut and Blackback).

The depth to the base of the Lakes Entrance Formation increases from the onshore to the offshore (see Figure 3.1 for top Latrobe Group structure map and Figure 3.2 for base Lakes Entrance Formation contours). In the Central Deep, the base of the Lakes Entrance Formation occurs at approximately 2,000 to 3,500 m sub-sea, whereas towards the margin of the Gippsland Basin, depths of 500-1,000 m are typical. Onshore, where the Lakes Entrance Formation is thinnest, the depths decrease to less than 400 m. The depth to the base of the regional top seal is considered significant as it is regarded that for CO2 to remain in supercritical phase, it is necessary to inject at depths greater than 800m (e.g. van der Meer, 1992; Holloway & Savage, 1993). However, Bachu (2003), for example, notes that the depth at which supercritical conditions are met may vary significantly depending on surface temperature and geothermal gradients.

In the current study, the marine facies present at the level of the basal Lakes Entrance Formation were identified from well completion reports. A simple representation of the basal Lakes Entrance Formation facies is presented in Figure 3.2. Overall, these facies are broadly similar to those proposed by Bernecker *et al.* (1997) and Gibson-Poole & Svendsen (2005).

Latrobe Group

Gurnard Formation

The Gurnard Formation underlies the Lakes Entrance Formation in some areas of the Gippsland Basin and acts as a top seal for several giant fields in the Central Deep. The thickness and distribution of the Gurnard Formation are highly variable. Partridge (1999) noted that 'The (Gurnard) Formation is generally not present or very thin over most of the eroded topographic highs of Blackback/Terakihi, Kingfish, Mackerel, Halibut/Cobia/Fortescue and Marlin'. The western limit of the Gurnard Formation is roughly aligned with the current day shoreline in an arc to the west of the Barracouta field. Partridge (1999) reported a minimum thickness of 7m in Moray-1 and a maximum of 78m in Bullseye-1.

Intra-formational seals

There are several intra-formational sealing units within the deeper Latrobe Group, which include floodplain sediments deposited in upper and lower coastal plain environments, as well as lagoonal to offshore marine shales. These local seals are commonly thin and mostly occur within stacked sandstone/mudstone successions. Other effective seals are formed by several distinct volcanic horizons of Campanian to Paleocene age; these are often less than 50 metres thick, although they are known to exceed 100 m at the Kipper field. Excellent Latrobe Group intra-formational seals include the Turonian Kipper Shale and the late Maastrichtian to early Paleocene Kate Shale (Bernecker & Partridge, 2001). The Kipper Shale accumulated in shallow to deep-water lacustrine environments and is widespread in its distribution. It covers the offshore portion of the basin between the basin-bounding faults and its thickness exceeds 500 m in Kipper-1 (Bernecker & Partridge, 2001). In contrast, the shelfal marine Kate Shale is limited in extent (Figure 3.3), with its principal depocentre located around the Halibut and Flounder fields (Bernecker & Partridge, 2005). The Kate Shale reaches its maximum thickness around and underneath the oil fields, which dominate the Central Deep. The thickest intersection of the sequence is 120 m at Trumpeter-1.



Figure 3.1 Lakes Entrance Formation thickness and top of Latrobe Group depth structure map.



Figure 3.2 Sedimentary facies identified at the base of the marine Lakes Entrance Formation.

3.3 Mercury Injection Capillary Pressure (MICP) Analysis

Maximum column retention capacities for oil, gas and CO₂ are routinely derived from Mercury Injection Capillary Pressure (MICP) analysis of sealing lithologies. The maximum column height that can be contained by a seal is called the seal capacity and is an important factor in the evaluation of seal potential for the geosequestration of carbon dioxide (Kaldi & Atkinson, 1997). As part of the present study, 37 samples were submitted to ACS Laboratories in Perth for MICP analysis (see Appendix 2 for threshold pressure data tables and charts). Maximum column retention capacities for oil and gas were determined using standard ACS methodologies. CO₂ retention capacities were determined after the method outlined in Daniel (2005). See Appendix 3 for the table of values used for CO₂ column height calculation. As it is not routine for exploration companies to acquire conventional cores within sealing lithologies such as the Lakes Entrance Formation, the number of suitable core samples was limited. Samples were chosen close to the base of the formation; otherwise, samples were selected as near as possible to the base of the available cored interval. In onshore locations where suitable lithologies within the Lakes Entrance Formation were not available, samples from the Gippsland Limestone were chosen.

Early in 2008, MICP data from 16 core samples were analysed and interpreted (O'Brien *et al.*, 2008). An additional 21 samples were acquired subsequently, significantly increasing the database of MICP values available for the onshore and offshore Gippsland Basin. In Table 3.1, newly acquired results are highlighted. In total, 31 samples of the Lakes Entrance Formation were taken from 26 wells, 2 samples from the underlying Gurnard Formation, and 4 samples from the overlying Gippsland Limestone.

3.4 Seal Capacity Results

The seal capacity results for the Lakes Entrance Formation, Gurnard Formation and Gippsland Limestone are best summarised in Figures 3.4, 3.5 and 3.6. The seal capacity in the offshore Central Deep is excellent. Column heights for gas in this area range from 185 m in Tuna-1 to 751 m in Wrasse-1. For CO₂, column heights range from 250 m in Barracouta-1 to 947 m in Wrasse-1. Sealing capacity on the offshore Southern Platform was previously reported as poor, based on MICP results from the base of the Lakes Entrance Formation in Groper-1 and Groper-2 (O'Brien *et al.*, 2008). A new result from further up-section in Groper-1 (287 m of gas and 246 m of CO₂) elevates the potential of the regional seal on the southern flank. In the onshore Lake Wellington Depression, the seal capacity varies from excellent (377 m of gas and 306 m of CO₂) where the Lakes Entrance Formation is thickest in the central portion of the depression, to poor (5 m of gas and 4 m of CO₂) at the margin near the terminal edge of the seal. Moderately effective seal capacity is characteristic of the onshore Seaspray Depression and the offshore Northern Terrace. The Alberton Depression appears to have poor sealing capacity (3 m of gas and 6 m of CO₂ in Woodside South-1). The Lakes Entrance Platform also has poor sealing capacity, although one result from Colquhoun East-6 of 123 m of gas and 164 m of CO₂ is an exception. Sealing capacity results are discussed in more detail in Section 4 of this report.

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Lakes Entrance Formation

Seal capacity values for the Lakes Entrance Formation are greatest in the Central Deep, where the formation generally attains its maximum thickness and is at its greatest down-hole depths. The relationships between MICP capacity of the Lakes Entrance Formation and its thickness, and MICP capacity and the depth of the Lakes Entrance Formation are presented in Figures 3.7 and 3.8 respectively. There is a strong positive relationship between potential column height and the thickness of the regional seal. Offshore, where the seal is thicker, its retention capacity is high. In contrast, in marginal parts of the basin the thickness of the Lakes Entrance Formation decreases and retention capacity tends to decrease (Figure 3.7). The positive relationship between depth and retention capacity (Figure 3.8) is probably due to the fact that the Lakes Entrance Formation was deposited in an early postrift setting, where it progressively filled the palaeotopographic lows. The strong relationship between the thickness of the Lakes Entrance Formation and the depth of the top Latrobe Group surface is evident from Figure 3.1.

Gippsland Limestone

Samples of the Gippsland Limestone were selected for MICP analysis where no suitable samples of the Lakes Entrance Formation were available or where the regional seal was absent. The four samples tested to date were all from wells in the western Lake Wellington Depression. Seal capacities for hydrocarbons and CO2 from Wooundellah-10 and Wooundellah-11 at a depth of 389 m are poor (see Table 1). Retention capacities of the Gippsland Limestone at greater depths, 599 m in Bundalaguah-10 and 628 m in Sale-15 are moderate, with respective column heights for CO2 of 41 m and 53 m. A more complete assessment of the sealing capacity of the Gippsland Limestone may be possible, as a limited selection of core samples from onshore and offshore wells remain available for analysis.



Figure 3.3 Thickness of the Kate Shale (as derived from well data).

| | SAMPLE | AMPLE LEF | | | | | COLUMN HEIGHT (m) | | |
|-------------------------|--------------|------------------|----------------------------|-------------|---|---|-------------------|-----|-----------------|
| WELL | DEPTH (m) | THICKNESS (m) | LOCATION | FACIES | LITHOLOGY | COMMENT | GAS | OIL | CO ₂ |
| Barracouta-1 | 1021.95 | 114 | Central Deep | Shelf | Calcareous shale, fossiliferous, glauconitic, indurated | 33m above gas column | 207 | 334 | 250 |
| Bengworden South-6 | 914.9 | 157 | Lake Wellington Depression | Inner Shelf | Fossiliferous marl, silty, soft | 52m above base of LEF | 302 | 486 | 282 |
| Bundalaguah-10** | 599.8 | 134 | Lake Wellington Depression | - | Fossiliferous marl, indurated | Gippsland Limestone 40m above top LEF | 10 | 16 | 41 |
| Cod-1 | 1711.89 | 285 | Central Deep | Basin | Fossiliferous calcareous shale, fissile and brittle | 171m above base of LEF | 433 | 696 | 683 |
| Colquhoun East-6 | 180.7 | 35 | Lakes Entrance Platform | Inner Shelf | Calcareous siltstone, glauconitic, well indurated | Base of the Metung Marl Member | 123 | 198 | 164 |
| Dulungalong-2 | 478.1 | 85 | Seaspray Depression | Inner Shelf | Fossiliferous marl, friable to indurated | 47m above base of LEF | 69 | 110 | 78 |
| Flounder-6 | 1929.38 | 394 | Central Deep | Basin | Calcareous mudstone, indurated | 3m above gas | 207 | 334 | 460 |
| Fortescue-2 | 2420 | 252 | Central Deep | Basin | Calcareous mudstone, well indurated | Base of LEF | 328 | 311 | 425 |
| Fortescue-2* | 2430 | - | Central Deep | - | Glauconitic calcareous mudstone, well indurated | Gurnard Formation 10m below base of LEF | 193 | 528 | 303 |
| Fortescue-3 | 2411.50 | 252 | Central Deep | Basin | Calcareous mudstone, well indurated | 1m above base of LEF | 437 | 702 | 641 |
| Gippsland Frome Lakes-4 | 503.5 | 95 | Lake Wellington Depression | Inner Shelf | Marl, silty and glauconitic, friable | 23m above base of LEF | 17 | 28 | 18 |
| Gippsland Frome Lakes-4 | 506.6 | 95 | Lake Wellington Depression | Inner Shelf | Marl, glauconitic, friable | 20m above base of LEF | 93 | 150 | 120 |
| Golden Beach West-1 | 667.68 | 119 | Seaspray Depression | Inner Shelf | Fossiliferous silty marl, slightly glauconitic, friable to indurated | 27m above base of LEF | 22 | 35 | 87 |
| Goon Nure-9 | 726.3 | 129 | Lake Wellington Depression | Inner Shelf | Marl, indurated | 21m above base of LEF | 251 | 404 | 213 |
| Groper-1 | 909.15 | 123 | Southern Platform | Inner Shelf | Calcareous mudstone, indurated | 22m above base of LEF | 287 | 461 | 246 |
| Groper-1 | 926.10 | 123 | Southern Platform | Inner Shelf | Glauconitic mudstone, calcareous, fossiliferous, friable | 5m above base LEF | 30 | 49 | 29 |
| Groper-1* | 932.00 | - | Southern Platform | - | Glauconitic sandstone, indurated | Gurnard Formation 1m below base LEF | 19 | 30 | 24 |
| Groper-2 | 747.86 | 73 | Southern Platform | Inner Shelf | Glauconitic mudstone, calcareous, fossiliferous, friable to indurated | 13m above base of LEF | 5 | 8 | 13 |
| Hunters Lane-1 | 377.00 | 76 | Lakes Entrance Platform | Inner Shelf | Fossiliferous bioturbated mudstone, glauconitic, micaceous, friable | 34m above granodiorite basement | 6 | 10 | 18 |

 Table 3.1
 Supportable column heights for Gippsland Basin samples, based upon MICP results. The majority of samples were taken from Lakes Entrance

 Formation intervals with the following exceptions: *Gurnard Formation **Gippsland Limestone. Shaded samples from O'Brien et al., 2008.

| | SAMPLE | MPLE LEF EPTH THICKNESS) (m) | LOCATION | FACIES | LITHOLOGY | COMMENT | COLUMN HEIGHT (m) | | |
|--------------------|--------------|-------------------------------------|----------------------------|-------------|--|--|-------------------|------|-----------------|
| WELL | DEPTH (m) | | | | | | GAS | OIL | CO ₂ |
| Kingfish-3 | 2143.05 | 264 | Central Deep | Basin | Calcareous mudstone, indurated | 101m above base of LEF | 207 | 334 | 463 |
| Meerlieu-4 | 722 | 141 | Lake Wellington Depression | Inner Shelf | Fossiliferous silty marl, slightly glauconitic, friable to indurated | 38m below top of LEF | 222 | 358 | 186 |
| Meerlieu-4 | 769 | 141 | Lake Wellington Depression | Inner Shelf | Marl, friable to indurated | 56m above base of LEF | 331 | 532 | 301 |
| Meerlieu-15001 | 699.9 | 140 | Lake Wellington Depression | Inner Shelf | Fossiliferous silty marl, slightly glauconitic, friable to indurated | 20m above base of LEF | 74 | 119 | 95 |
| Mullungdung-7 | 363 | 17 | Seaspray Depression | Inner Shelf | Marl, fossiliferous, glauconitic, silty, friable | 2m above base of LEF | 5 | 9 | 12 |
| Sale-13 | 748.1 | 125 | Lake Wellington Depression | Inner Shelf | Marl, slightly fossiliferous and glauconitic, indurated | 64m above base of LEF | 174 | 279 | 172 |
| Sale-13 | 795.6 | 125 | Lake Wellington Depression | Inner Shelf | Glauconitic marl, indurated | 16m above base of LEF | 214 | 343 | 170 |
| Sale-15** | 628.6 | 85 | Lake Wellington Depression | - | Fossiliferous marl, friable | Gippsland Limestone 31m above top of LEF | 57 | 91 | 53 |
| Seacombe-7 | 947.6 | 176 | Lake Wellington Depression | Inner Shelf | Marl, friable to indurated | 91m above base of LEF | 377 | 607 | 306 |
| Sole-1 | 805.9 | 170 | Northern Terrace | Shelf | Fossiliferous marl, glauconitic, sandy | 4m above gas column | 32 | 52 | 54 |
| Sperm Whale Head-1 | 653.8 | 127 | Lake Wellington Depression | Inner Shelf | Marl, friable to indurated | 11m below top of LEF | 230 | 370 | 196 |
| Sperm Whale Head-1 | 718.1 | 127 | Lake Wellington Depression | Inner Shelf | Marl, friable to indurated | 51m above base of LEF | 316 | 509 | 285 |
| Tuna-1 | 1160.00 | 259 | Central Deep | Basin | Calcareous mudstone, indurated | 151m above gas column | 185 | 298 | 289 |
| Woodside South-1 | 522.12 | 80 | Alberton Depression | Inner Shelf | Fossiliferous marl, soft and friable | 70m above base of LEF; 10m from top of LEF | 3 | 5 | 6 |
| Wooundellah-10** | 389.3 | - | Lake Wellington Depression | - | Fossiliferous silty marl, soft and friable | Gippsland Limestone | 5 | 8 | 4 |
| Wooundellah-11** | 389 | - | Lake Wellington Depression | - | Marl, fossiliferous, glauconitic, silty, friable | Gippsland Limestone | 8 | 12 | 11 |
| Wrasse-1 | 2589.89 | 249 | Central Deep | Basin | Calcareous mudstone, indurated | 140m above base of LEF | 751 | 1207 | 947 |
| Wurruk Wurruk-13 | 584.9 | 137 | Lake Wellington Depression | Inner Shelf | Marl, fossiliferous, glauconitic, silty, friable | 40m below top of LEF | 19 | 30 | 21 |



Figure 3.4 Retention capacities for CO₂: Combined results from the Gurnard Formation, Lakes Entrance Formation and Gippsland Limestone.



Figure 3.5 Retention capacities for gas: Combined results from the Gurnard Formation, Lakes Entrance Formation and Gippsland Limestone.



Figure 3.6 Retention capacities for oil: Combined results from the Gurnard Formation, Lakes Entrance Formation and Gippsland Limestone.



Figure 3.7 Relationship between the thickness of the Lakes Entrance Formation and its MICP retention capacity.



Figure 3.8 Relationship between the depth of the Lakes Entrance Formation and its MICP retention capacity.

Latrobe Group Gurnard Formation

Previously, MICP results measured by Daniel (2005) illustrate the variability of the seal capacity of the Gurnard Formation (from a retention column height of 723 m CO₂ in Kingfish-9 to 0.19 m and 40 m respectively in Bream-2 and Fortescue-2). A result from further up-sequence in Fortescue-2 at 2430m (see Table 1) of a retention capacity of 193 m for gas and 303 m for CO₂ suggests that seal capacity increases up the vertical succession. However, a low CO₂ retention column height (24 m) is recorded at the top of the Gurnard Formation in Groper-1 (see Table 3.1), on the Southern Platform.

Intra-formational seals

Daniel (2005) and Gibson-Poole *et al.* (2008) have demonstrated that intra-formational seals can locally hold back hundreds of metres of CO₂ (see Figure 3.9). However, whilst their seal capacities can be high, the laterally discontinuous nature of these intra-Latrobe seals probably produces a substantial decrease in their seal potential at a regional scale. If MICP results below 100 m capacity are discounted in Figure 3.9, the overall trend is for the CO₂ column heights to increase as the depth decreases, (i.e. the capacities of the Latrobe Group seals are better at shallower depths); possible facies variations may control this trend.

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The predominance of hydrocarbon discoveries at the base of the regional seal testifies to the overall ineffectiveness of the intra-Latrobe sealing system at a basin scale. Similarly, the combination of the variation in the seal capacity and the patchy geographic distribution of the Gurnard Formation suggest that the Lakes Entrance Formation will provide the ultimate regional barrier to the migration of hydrocarbons or injected fluids such as CO₂.



Figure 3.9 Relationship between the depth of Latrobe Group seals and their MICP retention capacity.

4 Containment Evaluation

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The interpreted effective seal potential of the regional top seal in the Gippsland Basin is summarised in Figure 4.1.

The seal potential appears to be excellent over the offshore Central Deep, the western Northern Terrace and the onshore Lake Wellington Depression. The sealing capacities for CO2 and gas recorded from 22 wells in these areas is high (i.e. column heights of greater than 150 m) and the depth to the top seal is 800 m or greater. The number of samples available for analysis is greatest in these two areas of the basin. Sealing potential on the Southern Terrace and most of the Southern Platform appears to be very good. Although few seal capacity results are available, values from Groper-1 indicate excellent capacity. The depth to the top seal is again greater than 800 m. The evaluation of this area cannot however be regarded as excellent because the spread of available data is insufficient to make such an assessment. Seal potential is regarded as good where the capacity of the Lakes Entrance Formation is likely to be effective yet is variable (i.e. 50-200 m column heights), and the base of the seal is intersected around 800 m. The seal is considered moderately effective in the Seaspray Depression and a small portion of the offshore Central Deep over the Golden Beach field and surrounds. In this area the base of the seal is intersected above 800 m and the sealing capacity column heights are less than 100 m. The seal is either absent or has poor sealing potential on the offshore Northern Platform and the onshore Lakes Entrance Platform; and the Baragwanath Anticline onshore between the Lake Wellington and Seaspray depressions. The westernmost Seaspray Depression, Alberton Depression and the southern margin of the offshore Southern Platform are also considered to have poor sealing potential due to low capacities and shallow top seal depths. In general, seal capacity decreases towards the basin margin and the limit that is currently the best estimate of the terminal edge of effective top seal.

4.1 Offshore Gippsland Basin

Central Deep

In terms of both the thickness and capacity of the regional top seal, containment characteristics for both hydrocarbons and CO₂ within the Central Deep appear to be excellent. However, the formation thins towards the onshore so that at Golden Beach-1 the thickness of the regional seal is reduced to less than 100 m thick. Between the Barracouta and Golden Beach fields, the depth at the base of the Lakes Entrance Formation shallows to less than 800 m. A possible explanation for the reduction in seal potential at the western extremity of the offshore Central Deep is discussed here with reference to palaeocharge histories, a migration model, seismic imagery and trap closure/hydrocarbon column heights.

The Lakes Entrance Formation within the Central Deep has a retention capacity of several hundred metres of oil and CO2 and approximately 200 - 750 m of gas (see Figures 3.4, 3.5 and 3.6). Samples taken from near the base of the Lakes Entrance Formation in Wrasse-1, Flounder-6 and Fortescue-3 have large hydrocarbon and CO2 column retention heights, as do samples analysed from slightly shallower depths within the Lakes Entrance Formation in Barracouta-1, Cod-1, Kingfish-3 and Tuna-1. These results are consistent with those of Daniel (2005). There are, however, variations in the retention capacities within the Central Deep that could be due to subtle variations in facies and lithologies. In addition, at a greater depth the Lakes Entrance Formation can withhold greater column heights. For example, the deepest sample from 2,589 m in Wrasse-1 in the Central Deep can contain 947 m of CO₂ and 751 m of gas, whereas 250 m of CO $_{\!\!2}$ and 204 m of gas can be contained at a depth of 1021 m in Barracouta-1. The MICP results indicate that the top seal capacity of the Lakes Entrance formation is excellent in the Central Deep. Moreover, the fact that numerous large gas and oil accumulations occur at top-Latrobe Group level, immediately beneath the regional top seal, also suggests that the Lakes Entrance Formation is an effective top seal, as confirmed by the MICP data.

This interpretation is supported by a general lack of leakage and seepage indicators in the region and by recent charge history work. Two AGSO (Geoscience Australia) water column geochemical sniffer surveys that traversed the Kingfish field failed to detect any anomalous zones. Furthermore, QGF and QGF-E analysis of the Kingfish oilfield has revealed that the charge history of this trap is relatively simple and that there is no evidence that Kingfish wells have ever had a palaeo-gas cap (Figure 4.2). It appears, therefore, that the Kingfish field was filled with an oil charge that has remained in place until the present day. The combination of the oil-prone charge history for Kingfish and the very high top seal capacities described here suggest that the reason that the central oil fields are in fact oil-filled and not gas-charged is simply due to the inherent nature of the charge into the traps. This rules-out the active seepage of gas from Kingfish through the regional seal, unless this occurred when the Lakes Entrance Formation was still unconsolidated (and there is no evidence to support this). A single gas chimney has been reported on seismic data near the Kingfish field by Cowley & O'Brien (2000), although it appears that the hydrocarbons associated with this leakage are not from the field itself.

The results of other palaeocharge history analysis (O'Brien *et al*, 2008) also confirm that all the large oil fields within the Central Deep have never had a gas cap, an observation entirely consistent with the large retention capacities obtained from the Lakes Entrance Formation over these traps.



Figure 4.1 An interpretation of top seal potential at a basin scale, Gippsland Basin.



Figure 4.2 Composite well summary of the Kingfish Field. The Gamma Ray (GR) Log shown here is from the Kingfish-2 well. MICP Analysis was conducted on core from the Lakes Entrance Formation in the Kingfish-3 well at a depth of 2143.05 m, which correlates with a depth of approximately 2135 m at Kingfish-2. Nine reservoir samples were collected from within the Kingfish Formation over a depth range 2252.47 m - 2319.22 m in the Kingfish-2 well.



Figure 4.3 Petromod 10 output showing predicted present day accumulations at Top Latrobe horizon, Gippsland Basin. Note the potential for fill-spill between Halibut/Fortescue/Cobia, Kingfish, Bream and Barracouta fields and Marlin, Snapper and Barracouta fields. It is emphasised that large volumes of hydrocarbons generated over millions of years cannot be compared directly with limited volumes of CO_2 .

Palaeocharge histories from oil and gas fields in the Gippsland Basin (O'Brien *et al.*, 2008) provide information on the type of hydrocarbons produced by the kitchens, as well as trap integrity through time. By constraining hydrocarbon kitchens, the data can be used to infer migration pathways through the basin. A very simple migration model of the petroleum systems in the Gippsland basin, produced in Petromod 10 (Figure 4.3) shows the linked nature of the traps along southern and northern spill-fill chains (consistent with Gibson-Poole *et al.*, 2008).

The modelled fill-spill chain at top Latrobe Group level, extending from the offshore Barracouta gas field, continues through the Golden Beach gas field and onshore to the Seaspray Depression (Figure 4.3). With the Golden Beach field on the main fill-spill pathway from the offshore, it is highly likely the structure would be filled-to-spill. However, only a 19 m live gas column is present in a total mapped closure of 40 m, suggesting that there is a very good chance that the structure is not filled-to-spill because of leakage by means of capillary failure of the seal (Figure 4.4)

Seismic reflection data over the Golden Beach gas field indicates the presence of a small fault cutting the top Latrobe Group horizon (Figure 4.5). Although there is no apparent gas chimney associated with this fault, there are various anomalous amplitudes close-by at shallow depth, which may indicate the presence of shallow hydrocarbons. Seal capacity and leakage and seepage data from the onshore Seaspray Depression and Baragwanath Anticline further support the trend of reduction of containment further onshore. It is therefore likely that fluids migrating through this point in the fill-spill chain towards the onshore Seaspray Depression and Baragwanath Anticline will not be contained as depicted in Figure 4.4.



Figure 4.4 Schematic cross-section extending from the Barracouta gas field to the onshore showing evidence of hydrocarbon seepage through the regional top seal.



Figure 4.5 Seismic data over the Golden Beach gas field revealing evidence of possible hydrocarbon seepage.



Figure 4.6 ALF Survey on the Northern Terrace between the Sole gas field and Northright-1, including visible oil slicks, anomalies, fluors and gas chimneys.

Northern Terrace

The containment potential of the Northern Terrace is best described as variable (see Figure 4.1). At the eastern extremity of the Northern Terrace, containment is lost somewhere between the Sole gas field and Northright-1 on the Northern Platform where the regional seal is absent. This is supported by remote and direct sensing survey leakage and seepage data that indicates the presence of active seepage in this area (i.e. the seal is failing). Further to the west, hydrocarbons reservoired at the top of the Latrobe Group, under the regional seal indicate that the seal is effective. Even further westward, near shore, few wells have been drilled on the Northern Terrace; it is therefore only possible to speculate on the effectiveness of the seal in this location. However, the sealing ability of the Lakes Entrance Formation in Cuttlefish-1 was noted to be very good (Irwin, 1999). In addition, there is no evidence of gas chimneys or anomalous amplitudes in the 2-D seismic images from this area.

Hydrocarbons are reservoired at the top of the Latrobe Group under the regional seal in several oil and gas fields in the 'central to eastern' Northern Terrace: Sole, Leatherjacket, Patricia-Baleen and Sperm Whale. Gas columns contained in the Patricia-Baleen Field and Sole-2 reach heights of 50 m and 75 m respectively, apparently without attendant top seal failure. Both the Patricia-Baleen and Sole fields are filled-to-spill suggesting that the regional seal across this part of the Northern Terrace can withhold gas columns with heights over 50 m. An MICP analysis of a sidewall core sample from the Lakes Entrance Formation in Sole-1 shows that the seal here can contain 32 m of gas and 54 m of CO₂, suggesting that the seal is effective across this area. Therefore, the seal potential across the Northern Terrace appears to be adequate for the retention of modest gas columns.

Numerous remote and direct sensing surveys conducted in the north of the basin have detected apparent leak points in discrete locations on the Northern Terrace. For instance, between the Sole gas field and Northright-1, anomalies detected during an Airbourne Laser Fluorescence (ALF) Survey (Figure 4.6) provide some evidence for seal failure in this area. The fluor pattern and presence of slicks from the survey were interpreted as oil migrating dominantly to the northeast, towards the vicinity of Northright (Messent, 2000). Also, several apparent gas chimneys (Figure 4.6) near Flathead-1 (Figure 4.7), Moby-1 and Wahoo-1 may relate to migration of hydrocarbons from filledto-spill structures, potentially defining the effective edge of the seal for gas in this part of the basin. Indeed, the chimney near Flathead-1 is currently active and hydrocarbon anomalies detected during AGSO 1989 and 1991 "sniffer" surveys are present in the water column directly above the chimney (see O'Brien et al, 2008). A seafloor sampling survey conducted by AGSO in 1988 also indicated the presence of possible hydrocarbons in seafloor sediments near Wahoo-1, perhaps strengthening the notion of active hydrocarbon seepage in this area. This is consistent with the review of the seal geometry, that the Lakes Entrance Formation is absent from the margin of the Northern Terrace around Northright-1.

AGSO sniffer surveys also traversed part of the Rosedale Fault System and detected anomalies between the Sunfish and Tuna fields, perhaps indicating seepage along parts the fault system due to top seal failure. However, if the source of hydrocarbons on the Northern Terrace is from the Central Deep, with migration occurring at the top of the Latrobe Group then the presence of gas and oil fields north of the Rosedale Fault System indicates that the top seal is, at least partly effective along portions of the fault system.



Figure 4.7 Offshore gas chimney near Flathead-1 on the Northern Terrace.
Southern Terrace

On the Southern Terrace, seal potential is interpreted to be very good. However, only a qualitative estimate is possible as there are no Lakes Entrance Formation core samples available for MICP analysis and there is currently no remote sensing evidence to identify points of seal failure. However, the thickness and depth of the base of the formation in this location (e.g. 388 m at 2140 m in Tarra-1) are similar to those of the Central Deep, suggesting that excellent seal capacity could be expected across the Southern Terrace. The trend for seal capacity to reduce with decreased formation thicknesses and depth near-shore in the Central Deep may also apply to the Southern Terrace. Given that the seal capacity further to the south on the Southern Platform in Groper-1 at 909 m is 246 m for CO₂, it is likely that an estimate of very good potential is a conservative one.

Northern Platform

The Northern Platform has poor sealing characteristics. The seal is present but not necessarily effective on the western Northern Platform, offshore from the Lakes Entrance Township (see Figure 4.1 for top seal limits). In the nearshore area close to Lakes Entrance, it is likely that seal capacity is further reduced. The regional seal is lost over the eastern Northern Platform, to the south of the Lakes Entrance and Marlo Townships (i.e. there is no seal present to the east of Marlo on the offshore Northern Platform). Only one well, Northright-1, has been drilled on the Northern Platform (where there is no seal present). Therefore, no core was available for MICP analysis of the Lakes Entrance Formation from the Northern Platform, and so seal potential can only be estimated, where it is present. Anomalies, flours and slicks from likely oil seepage to the northeast, towards Northright-1 were detected during an ALF survey on the eastern extremity of the Northern Platform (Messent, 2000). These observations are consistent with the likely absence of top seal across the eastern part of the Northern Platform.

Southern Platform

There are few wells drilled on the Southern Platform. However, from seal capacity data gained from MICP analysis of core samples from Groper-1 and Groper-2, some evaluation of the seal potential of the Southern Platform is possible. The thickness of the regional seal decreases both towards the shore and towards the margin of the basin on the Southern Platform. The Lakes Entrance Formation is relatively thin at Groper-1 and Groper-2 with thicknesses of 123 m and 73 m respectively. However, MICP analysis of a core sample from 909 m in Groper-1 has demonstrated that the seal is capable of holding 287 m of gas or 246 m of CO₂. This additional Lakes Entrance Formation core was sampled further uphole than those previously analysed. This data implies that the seal in this location is just as effective as it is in parts of the Central Deep, the potential of which is considered excellent. This assessment differs from a previous evaluation of the Southern Platform (i.e. O'Brien *et al.*, 2008) where the sealing capacity of the Lakes Entrance Formation on the Southern Platform was considered poor to moderate, based on initial MICP results from Groper-1 (30 m of gas) and Groper-2 (5 m of gas).

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4.2 Onshore Gippsland Basin

Lake Wellington Depression

Onshore, in the Lake Wellington Depression, the Lakes Entrance Formation is relatively thick (greater than 100 m) and the sealing capacity appears to be effective. In the nearshore area of the Lake Wellington Depression, the seal capacity is excellent but is reduced further to the west where the Lakes Entrance Formation thins significantly. Seventeen core samples from the Lake Wellington Depression yielded significantly greater retention heights than for any other onshore area. MICP data from friable to indurated marls indicates that the seal through this area can retain a maximum gas column height of 377 m and a CO₂ column of 306 m in Seacombe-7. These seal capacity results are as good as or better than some MICP values obtained across the Central Deep. Moving from east to west, further onshore, and north and south towards the bounding faults of the Lake Wellington Depression, retention capacities decrease to values of less than 20-metre column heights.

Murray (1997) and Summons *et al.* (1998) detected possible thermogenically-derived petroleum in sediments from the floor of Lake Wellington. This oil was interpreted to be geochemically similar to that in the offshore Turrum Field (Murray, 1997). However, Summons *et al.* (1998) suggested that the results did not constitute absolute proof of natural petroleum seepage into the Gippsland Lakes from the offshore basin. If this seepage were to be confirmed, migration from the northern spill-fillchain across the Rosedale Fault and into the Lake Wellington Depression could have significant implications for assessing the seal potential at the southern margin of the depression.

Based on sealing capacities alone, in the onshore Gippsland Basin, the regional seal in the Lake Wellington Depression has the greatest potential to retain hydrocarbons and CO₂.

Seaspray Depression

The sealing capacity in the Seaspray Depression appears to be adequate but decreases towards the margins. In the Seaspray Depression, adjacent to the current day coastline, the Lakes Entrance Formation is generally around 100 m thick. The regional top seal attains a maximum thickness of 159 m in Lake Reeve-1 on the coast about 16 km to the northwest of the Golden Beach gas field. The depth to the base of the regional seal is greater than 800 m at Lake Reeve-1 but reduces to less than 800 m further onshore to the west and towards both the Baragwanath Anticline to the north and the Alberton Depression to the southwest.

The regional top seal at Golden Beach West-1 can potentially contain 87 m of CO₂, 35 m of oil and 22 m of gas. Dulungalong-2, located 2 km from Golden Beach West-1, can potentially contain 78 m of CO₂, similar to that seen at Golden Beach West-1. Close to the terminal edge of the seal in Mullungdung-7, only 5 m of gas or a 12 m column of CO₂ could be contained. Whilst still representing an effective seal, at least for CO₂, the retention capacities in the Seaspray Depression appear to be significantly less than those present in the Central Deep and the adjacent Lake Wellington Depression.

There are no known hydrocarbon accumulations under the base of the regional seal in the Seaspray Depression. The gas accumulations in fields such as North Seaspray and Gangell are found within Strzelecki Group sands rather than at the top of the Latrobe Group. Whether the lack of accumulations is due to an absence of effective seal over the Latrobe Group in the Seaspray Depression or inadequate migration pathways into the top Latrobe Group structures is unknown. Although not proven, a lack of effective seal, especially toward the depression margins, is most likely and would be consistent with the sealing capacity results.

Numerous gas chimneys, shallow anomalous amplitudes and possible Hydrocarbon-Related Diagenetic Zones (HRDZs) are present on seismic reflection data in the nearshore and within the Seaspray Depression, implying active hydrocarbon migration, leakage and seepage. Most of the mapped onshore gas chimneys also correlate strongly with mapped soil geochemistry anomalies.

Alberton Depression

Onshore to the south of the Darriman Fault, in the Alberton Depression, the regional seal is very thin (less than 20 m) where it is present, close to the present day coast. The top seal capacity is poor: for example, at Woodside South-1 retention capacities of 3 m for gas and 6 m for CO₂ suggest that the friable fossiliferous marl at this location is more characteristic of a reservoir than a seal. The Alberton Depression therefore has very little, if any, potential for sealing hydrocarbons or CO₂.

Lakes Entrance Platform

The seal potential of the Lakes Entrance Platform is poor. There is no effective seal in this part of the onshore Gippsland Basin as that limit is found further to the south offshore (see Figure 4.1). Numerous wells have been drilled onshore on the Lakes Entrance Platform, with the only discovery being the Lakes Entrance Oil field. The oil rests stratigraphically in the basal greensand of the Lakes Entrance Formation. No other discoveries or shows have been made onshore to indicate the presence of hydrocarbons.

Of the wells located on the Lakes Entrance Platform only two samples were available for MICP analysis (Hunters Lane-1 and Colquhoun East-6). The Lakes Entrance Formation sample from Hunters Lane-1 yielded very low column retention heights (gas column height of only 6 m and a CO2 column height of 18 m). The sample was a friable fossiliferous glauconitic marl. In Colquhoun East-6, a stratigraphically higher sample at the shallow depth of 180 metres down-hole, yielded column heights of 123 m of gas and 164 m of CO₂. This sample was an indurated calcareous and glauconitic siltstone. It is unknown whether the cementation displayed in this sample is widespread in lateral and vertical extent or whether it is a local diagenetic feature. In any case, the shallow depth of the formation at this location suggests that containment of supercritical CO2 would not be possible.

Baragwanath Anticline

The Lakes Entrance Formation top seal is absent over the Baragwanath Anticline (between the Lake Wellington and Seaspray depressions) and top seal containment has been lost east of the anticline. Cover across the top of the Latrobe horizon on the anticline is thin (see Thomas & Baragwanath, 1949 and Hocking, 1988). For example, in Deadman Hill-1 the top of the Latrobe Group is intersected at around 100 m down-hole with only a 19 m cover of Lakes Entrance Formation with overlying Gippsland Limestone and Haunted Hill Formation.

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Lakes Oil N.L. tested for oil shows in the vicinity of a seep approximately 10 km southeast of Sale (Mulready, 2002). The location of this seep is consistent with an anomaly present on the radiometrics data from Geoscience Australia's 1999 airborne survey and possible gas chimneys in this area (Figure 4.8). All data suggests that an active hydrocarbon seep occurs along the fill-spill chain at top-Latrobe Group level, up-dip from the Golden Beach and Barracouta gas fields, through the Seaspray Depression and on to the Baragwanath Anticline. From the radiometrics image (Figure 4.8), the uranium counts peak in and around the seep, which is located 1-2.5 km north or northeast of the mapped fill-spill chain. Whether this seep, or seepage chain, is principally the result of seepage up

the Rosedale Fault or seepage along the fill-spill chain, is currently uncertain. Nearby, seal capacity results from Dulungalong-2 in the Seaspray Depression, do indicate a reduction in the effective containment relative to the nearshore Central Deep and the Wellington Depression to the north. 35

Seismic reflection data located over the interpreted seepage chain reveal two possible gas chimneys above two separate faults (Figure 4.9), part of the Rosedale Fault System and have a strong association with high uranium concentrations (Figure 4.8), providing further evidence for poor sealing potential both on the anticline and on immediately adjacent areas.



Figure 4.8 Radiometrics data for the onshore Gippsland Basin, along with modelled fill-spill chain from the Barracouta gas field. Known and interpreted hydrocarbon seeps correspond to a broadly east-southeast trending zone exhibiting strongly anomalous radiometrics response.

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Figure 4.9 Seismic reflection line GCRP91a-09 showing possible gas chimneys above high-angle reverse faults of the Rosedale Fault System (RFS).

5 Conclusions and Future Directions

The conclusions drawn from this study are as follows.

The Lakes Entrance Formation currently acts as the primary top seal for hydrocarbons in the Gippsland Basin and will act as an effective regional barrier for the containment of CO₂ over large parts of the basin.

- The Lakes Entrance Formation consists of thick calcareous mudstones and shales in the Central Deep and where the formation thins toward the basin margin, fossiliferous and glauconitic marls. The Lakes Entrance Formation is thickest in the Central Deep, where the base is also deepest (2,000 to 3,500 m sub-sea). At the basin margins, the regional seal thins and the formation base occurs at depths of around 500 to 1,000 m sub-sea.
- The seal capacity of the Lakes Entrance Formation is greatest in the offshore Central Deep, the western Northern Terrace and the onshore Lake Wellington Depression (250 m to 947 m for CO₂). These areas therefore have the best potential to contain injected CO₂ in the Gippsland Basin.
- On the Southern Terrace and Southern Platform, the sealing potential of the Lakes Entrance Formation is very good. The formation is thick and seal capacity results (246 m of CO₂) from Groper-1 indicate that the seal has the potential to contain significant column heights of CO₂.
- The Seaspray Depression and Northern Terrace have good to moderate sealing potential. In these locations, the seal thickness and depths are variable. Seal capacity results are also variable but generally much lower than those recorded in the Central Deep, Lake Wellington Depression and Southern Platform.

- The offshore Northern Platform and the onshore Lakes Entrance Platform, Baragwanath Anticline and Alberton Depression, offer very little containment potential for injected CO₂.
- Locally, Latrobe Group intraformational seals have high seal capacities but values are variable. The generally thin nature and limited lateral extent of these seal leads to regionally low seal potential, as evidenced by the hydrocarbon accumulation patterns in the basin.

As part of the VICGCS program, further studies to investigate and understand the containment potential in the Gippsland Basin are underway.

- A QEMSCAN analysis of samples from the Lakes Entrance Formation and Gippsland Limestone used in this study is in progress. The QEMSCAN analysis will allow investigation of mineralogical controls on seal integrity and correlation with wireline log signatures.
- Further MICP analysis of the Seaspray Group (Lakes Entrance Formation and Gippsland Limestone) and intraformational Latrobe Group seals will be undertaken and the geometry of a major intraformational Latrobe Group seal, the Kate Shale, will be investigated. The seal potential of the onshore Lake Wellington Depression will be examined further by identifying and assessing Latrobe Group intraformational seals.
- Further work is planned on the mechanical properties of the regional seal and assessing the geomechanical stability of faults within the seal.
- The work in this report has concentrated on issues concerning top-seal. Further work is planned on issues relating to fault-seal within the Lakes Entrance Formation.

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Appendix 1

Lakes Entrance Formation tops and thicknesses identified in onshore and offshore wells, Gippsland Basin

| Well Name | Longitude | Latitude | KB | LEF | LEF | LEF | LEF | LEF |
|------------------------------|---------------|--------------|----|-----------|------|------|-------|-------|
| | | | | thickness | τορ | Dase | (msl) | (msl) |
| Admiral 1 | 148 38 55.23E | 38 09 06.62S | 21 | 238 | 998 | 1236 | 977 | 1215 |
| Albacore 1 | 148 19 58.61E | 38 33 54.46S | 30 | 269 | 2250 | 2519 | 2220 | 2489 |
| Albatross 1 | 148 03 05.59E | 37 57 34.36S | 10 | 79 | 628 | 707 | 618 | 697 |
| Amberjack 1 | 147 18 59.71E | 38 29 27.94S | 21 | 123 | 1136 | 1259 | 1115 | 1238 |
| Anemone 1A | 148 19 53.25E | 38 45 46.92S | 27 | 180 | 2401 | 2581 | 2374 | 2554 |
| Angelfish 1 | 148 22 53.40E | 38 14 37.38S | 21 | 171 | 1477 | 1648 | 1456 | 1627 |
| Angler 1 | 148 26 33.71E | 38 39 29.86S | 27 | 290 | 2477 | 2767 | 2450 | 2740 |
| Archer 1 | 148 18 41.52E | 38 46 01.56S | 28 | 169 | 2390 | 2559 | 2362 | 2531 |
| Athene 1 | 148 27 24.78E | 38 35 46.60S | 23 | 285 | 2475 | 2760 | 2452 | 2737 |
| Avon 1 | 147 08 17.61E | 38 02 49.50S | 9 | 125 | 610 | 735 | 601 | 726 |
| Ayu 1 | 148 17 07.27E | 38 36 29.48S | 28 | 350 | 2140 | 2490 | 2112 | 2462 |
| Baleen 1 | 148 26 12.97E | 38 00 31.085 | 9 | 126 | 512 | 638 | 503 | 629 |
| Baleen 2 | 148 24 42.12E | 38 01 50.215 | 20 | /5 | 647 | 122 | 621 | 696 |
| Barracouta 1 | 140 20 00.90E | 37 40 04.073 | 10 | 114 | 040 | 1054 | 020 | 1044 |
| Barracouta 2 | 147 42 49.03E | 30 10 30.403 | 10 | 114 | 940 | 1004 | 930 | 1044 |
| Barracouta 3 | 147 40 30.03L | 38 10 13 485 | 9 | 04 | 910 | 1020 | 907 | 1011 |
| Barracouta 4 | 147 42 07 81F | 38 17 15 275 | 25 | 65 | 976 | 1041 | 951 | 1005 |
| Barracouta 5 | 147 39 40 67F | 38 17 58 015 | 21 | 139 | 1044 | 1183 | 1023 | 1162 |
| Basker 1 | 148 41 57 77E | 38 18 20 945 | 25 | 313 | 1807 | 2120 | 1782 | 2095 |
| Basker 2 | 148 42 30.94E | 38 17 58.81S | 22 | 333 | 1755 | 2088 | 1733 | 2066 |
| Basker 5 | 148 42 23.80E | 38 17 59.35S | 22 | 317 | 1786 | 2103 | 1764 | 2081 |
| Basker South 1 | 148 41 26.13E | 38 19 05.84S | 25 | 143 | 2067 | 2210 | 2042 | 2185 |
| Batfish 1 | 148 24 17.58E | 38 13 28.48S | 10 | 229 | 1225 | 1454 | 1215 | 1444 |
| Baudin 1 | 147 52 23.60E | 37 51 35.47S | 42 | 64 | 304 | 368 | 262 | 326 |
| Beardie 1 | 147 48 29.26E | 38 15 10.69S | 25 | 124 | 1176 | 1195 | 1151 | 1170 |
| Bengworden South 6 | 147 25 40.04E | 38 03 31.18S | 2 | 110 | 849 | 959 | 847 | 957 |
| Bignose 1 | 148 36 10.07E | 38 21 15.86S | 25 | 263 | 2260 | 2523 | 2235 | 2498 |
| Billfish 1 | 148 33 19.23E | 38 40 07.45S | 31 | 182 | 2705 | 2887 | 2674 | 2856 |
| Blackback 1 | 148 33 46.72E | 38 32 57.98S | 21 | 327 | 2570 | 2897 | 2549 | 2876 |
| Blackback 2 | 148 32 40.69E | 38 33 22.70S | 22 | 236 | 2543 | 2779 | 2521 | 2757 |
| Blackback 3 | 148 31 10.10E | 38 33 29.30S | 25 | 281 | 2540 | 2821 | 2515 | 2796 |
| Blenny 1 | 147 24 56.69E | 38 28 18.15S | 23 | 130 | 1100 | 1230 | 1077 | 1207 |
| Bonita 1A | 148 17 14.31E | 38 33 41.86S | 30 | 278 | 2162 | 2440 | 2132 | 2410 |
| Bream 2 | 147 47 50.73E | 38 31 16.19S | 9 | 242 | 1560 | 1802 | 1551 | 1793 |
| Bream 3 | 147 46 19.64E | 38 30 41.48S | 28 | 232 | 1615 | 1847 | 1587 | 1819 |
| Bream 4A | 147 44 55.60E | 38 30 21.28S | 21 | 268 | 1590 | 1858 | 1569 | 1837 |
| Bream 5 | 147 52 03.58E | 38 30 49.515 | 21 | 304 | 1560 | 1864 | 1539 | 1843 |
| Broadbill 1 | 147 01 22.09E | 38 35 19.795 | 32 | 68 | /82 | 850 | 750 | 818 |
| Builseye 1 Bundalaguah 10 | 147 34 04.12E | 38 35 23.845 | 10 | 3/5 | 1697 | 2072 | 1687 | 2062 |
| Burong 1 | 147 01 14.30E | 38 18 33 359 | 7 | 103 | 552 | 655 | 513 | 616 |
| Carrs Creek 1 | 147 11 50.27E | 38 17 26 485 | 27 | 103 | 584 | 686 | 557 | 659 |
| Chimaera 1 | 147 13 39.39E | 38 15 50 815 | 25 | 430 | 1493 | 1923 | 1468 | 1898 |
| Cobia 1 | 148 17 05 88F | 38 27 21 215 | 10 | 151 | 2232 | 2383 | 2222 | 2373 |
| Cobia 2 | 148 18 20 94F | 38 27 25 955 | 25 | 228 | 2152 | 2380 | 2127 | 2355 |
| Cod 1 | 147 58 37.62E | 38 21 37.47S | 10 | 285 | 1597 | 1882 | 1587 | 1872 |
| Colliers Hill 1 | 147 17 34.65E | 38 11 50.48S | 17 | 85 | 451 | 536 | 435 | 520 |
| Colguhoun East 6 | 148 07 11.56E | 37 47 09.46S | 40 | 35 | 144 | 179 | 104 | 139 |
| Colguhoun North 1 | 147 56 30.56E | 37 48 46.47S | 30 | 44 | 134 | 178 | 104 | 148 |
| Comley 1 | 147 33 31.75E | 37 53 58.21S | 52 | 38 | 438 | 476 | 386 | 424 |
| Conger 1 | 148 03 50.94E | 38 21 22.22S | 21 | 209 | 1605 | 1814 | 1584 | 1793 |
| Cuttlefish 1 | 148 03 06.89E | 37 59 35.26S | 26 | 47 | 792 | 839 | 766 | 813 |
| Darriman 1 | 147 00 34.61E | 38 26 58.49S | 36 | 85 | 452 | 537 | 416 | 501 |
| Dart 1 | 148 55 32.78E | 38 08 06.40S | 10 | 191 | 731 | 922 | 721 | 912 |
| Deadman Hill 1 | 147 10 55.30E | 38 11 45.42S | 59 | 19 | 82 | 101 | 23 | 42 |
| Denison 53 | 146 53 50.31E | 38 06 24.03S | 17 | 0 | | | | |
| Devilfish 1 | 147 55 15.19E | 38 47 52.69S | 28 | 184 | 1461 | 1645 | 1433 | 1617 |
| Dolphin 1 | 147 22 47.66E | 38 29 26.49S | 10 | 142 | 1050 | 1192 | 1040 | 1182 |

| Well Name | Longitude | Latitude | KB | LEF | LEF | LEF | LEF | LEF |
|---|---|--|---|--|--|--|--|--|
| | | | | thickness | top | base | top | base |
| | | | | | | | (msl) | (msl) |
| Dome Frome 1 | 148 01 02.54E | 37 47 29.45S | 39 | 0 | | | | |
| Dome Frome 2 | 148 02 34.56E | 37 46 33.46S | 15 | 0 | | | | |
| Dome Frome 3 | 148 07 40.56E | 37 46 00.46S | 6 | 0 | | | | |
| Dome Frome 4 | 148 05 08.57E | 37 49 08.46S | 43 | 52 | 304 | 356 | 261 | 313 |
| Drummer 1 | 148 15 02.94E | 38 28 28.46S | 21 | 305 | 2127 | 2432 | 2106 | 2411 |
| Duck Bay 1 | 147 39 40.69E | 37 56 39.18S | 24 | 103 | 579 | 682 | 555 | 658 |
| Dulungalong 2 | 147 18 09.88E | 38 11 57.89S | 8 | 85 | 440 | 525 | 432 | 517 |
| Dutson Downs 1 | 147 21 49.58E | 38 11 54.51S | 5 | 130 | 578 | 708 | 573 | 703 |
| East End 1 | 148 21 18.52E | 37 47 58.45S | 3 | 0 | | | | |
| East Halibut 1 | 148 21 03.13E | 38 24 28.96S | | 225 | 2170 | 2395 | 2149 | 2374 |
| East Kingfish 1 | 148 12 41.34E | 38 35 01.84S | 21 | 444 | 2046 | 2490 | 2025 | 2469 |
| East Lake Tyers 1 | 148 07 37.66E | 37 50 32.16S | 5 | 97 | 296 | 393 | 291 | 388 |
| East Nowa 1 | 148 09 46 64F | 37 47 41 158 | 62 | 54 | 221 | 275 | 160 | 214 |
| Fast Pilchard 1 | 148 33 47 39E | 38 11 48 625 | 25 | 239 | 1405 | 1644 | 1380 | 1619 |
| East Reeve 1 | 147 32 55 57E | 38 05 44 475 | 4 | 193 | 989 | 1182 | 985 | 1178 |
| Edina 1 | 147 52 35.57E | 38 36 17 025 | 31 | 430 | 1848 | 2278 | 1817 | 2247 |
| Emperor 1 | 147 32 40.33E | 38.05.48.465 | 0 | 145 | 1372 | 1517 | 1363 | 1508 |
| Eniperor 1 | 147 35 21 07E | 37 54 42 528 | 13 | 37 | 406 | 533 | 453 | 400 |
| Flathoad 1 | 147 33 21.07 | 38 01 15 449 | 43 | 52 | 305 | 447 | 400 | 490 |
| Flatileau I | 140 32 00.30E | 30 01 15.443 | 9 | 316 | 1612 | 447 | 300 | 400 |
| | 146 25 33.59E | 30 10 40.455 | 20 | 310 | 1013 | 1929 | 1000 | 1901 |
| Flounder 2 | 140 20 37.07E | 30 19 11.145 | 30 | 341 | 1020 | 1909 | 1090 | 1939 |
| Flounder 3 | 148 28 27.68E | 38 18 52.145 | 30 | 362 | 1634 | 1996 | 1604 | 1966 |
| Flounder 4 | 148 29 51.51E | 38 18 18.025 | 10 | 335 | 1595 | 1930 | 1585 | 1920 |
| Flounder 5 | 142 00 23.61E | 38 12 28.495 | 9 | 322 | 1590 | 1912 | 1581 | 1903 |
| Flounder 6 | 148 26 13.75E | 38 19 01.535 | 25 | 394 | 1538 | 1932 | 1513 | 1907 |
| Flying Fish 1 | 147 21 56.85E | 38 20 45.09S | 10 | 148 | 946 | 1094 | 936 | 1084 |
| Fortescue 1 | 148 14 23.99E | 38 22 22.76S | 25 | 251 | 2164 | 2415 | 2139 | 2390 |
| Fortescue 2 | 148 16 03.74E | 38 25 51.42S | 31 | 252 | 2168 | 2420 | 2137 | 2389 |
| Fortescue 3 | 148 16 06.90E | 38 23 17.57S | 31 | 252 | 2160 | 2412 | 2129 | 2381 |
| Fortescue 4 | 148 16 40.08E | 38 24 52.34S | 25 | 270 | 2138 | 2408 | 2113 | 2383 |
| Frome Lakes 4 | 147 15 34.59E | 37 59 02.51S | 38 | 95 | 432 | 527 | 394 | 489 |
| Gangell 1 | 147 11 53.14E | 38 18 47.85S | 40 | 108 | 568 | 676 | 528 | 636 |
| Gannet 1 | 148 08 13.12E | 37 54 15.01S | 10 | 89 | 586 | 675 | 576 | 665 |
| Golden Beach 1A | 147 25 24.77E | 38 15 27.11S | 12 | 89 | 556 | 645 | 544 | 633 |
| Golden Beach West 1 | 147 21 27.58E | 38 14 49.48S | 12 | 119 | 585 | 704 | 573 | 692 |
| Goon Nure 9 | 147 37 53.97E | 37 58 16.23S | 29 | 129 | 618 | 747 | 589 | 718 |
| Great White 1 | 148 37 42.45E | 38 27 01.68S | 31 | 417 | 2805 | 3222 | 2774 | 3191 |
| Groper 1 | 147 25 00.69E | 38 56 14.50S | 10 | 123 | 808 | 931 | 798 | 921 |
| Groper 2 | 147 14 17.53E | 38 58 34.44S | 10 | 73 | 687 | 760 | 677 | 750 |
| Grunter 1 | 148 31 00.83E | 38 16 15.74S | 21 | 283 | 1570 | 1853 | 1549 | 1832 |
| Gummy 1 | 148 44 25.85E | 38 17 54.00S | 28 | 326 | 1755 | 2081 | 1727 | 2053 |
| Gurnard 1 | 147 58 42.63E | 38 35 27.47S | 10 | 295 | 1890 | 2185 | 1880 | 2175 |
| Halibut 1 | 148 19 01.60E | 38 23 52.46S | 10 | 372 | 1910 | 2282 | 1900 | 2272 |
| Halibut 2 | 148 19 52.58E | 38 23 39.98S | 25 | 291 | 2040 | 2331 | 2015 | 2306 |
| Hammerhead 1 | 148 50 03.79E | 38 10 28.66S | 22 | 233 | 1058 | 1291 | 1036 | 1269 |
| Hapuku 1 | 148 33 00.88E | 38 33 14.51S | 9 | 283 | 2527 | 2810 | 2518 | 2801 |
| Harlequin 1 | 147 42 32.68E | 38 11 54.42S | 21 | 195 | 1213 | 1408 | 1192 | 1387 |
| Helios 1 | 148 16 38.68E | 38 41 34.91S | 23 | 394 | 2180 | 2574 | 2157 | 2551 |
| Hermes 1 | | | | | | | | 0.405 |
| Hunters Lane 1 | 148 17 58.89E | 38 36 02.48S | 23 | 348 | 2160 | 2508 | 2137 | 2485 |
| | 148 17 58.89E 147 58 30.00E | 38 36 02.48S 37 51 54.21S | 23 50 | 348 76 | 2160 318 | 2508 394 | 2137 268 | 2485 344 |
| Investigator 1 | 148 17 58.89E 147 58 30.00E 147 36 50.69E | 38 36 02.48S 37 51 54.21S 37 54 44.17S | 23 50 35 | 348 76 66 | 2160 318 510 | 2508 394 576 | 2137 268 476 | 2485 344 542 |
| Investigator 1 Judith 1 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S | 23 50 35 21 | 348 76 66 228 | 2160 318 510 1223 | 2508 394 576 1451 | 2137 268 476 1202 | 2485 344 542 1430 |
| Investigator 1 Judith 1 Kahawai 1 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S | 23 50 35 21 21 | 348 76 66 228 304 | 2160 318 510 1223 1086 | 2508 394 576 1451 1390 | 2137 268 476 1202 1065 | 2485 344 542 1430 1369 |
| Investigator 1 Judith 1 Kahawai 1 Kingfish 1 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E 148 12 39 62F | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S 38 35 44 47S | 23 50 35 21 21 10 | 348 76 66 228 304 279 | 2160 318 510 1223 1086 1971 | 2508 394 576 1451 1390 2250 | 2137 268 476 1202 1065 1961 | 2485 344 542 1430 1369 2240 |
| Investigator 1 Judith 1 Kahawai 1 Kingfish 1 Kinofish 2 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E 148 12 39.62E 148 10 17 | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S 38 35 44.47S 38 35 51 16S | 23 50 35 21 21 10 9 | 348 76 66 228 304 279 269 | 2160 318 510 1223 1086 1971 1975 | 2508 394 576 1451 1390 2250 2244 | 2137 268 476 1202 1065 1961 | 2485 344 542 1430 1369 2240 2235 |
| Investigator 1 Judith 1 Kahawai 1 Kingfish 1 Kingfish 2 Kinofish 3 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E 148 12 39.62E 148 10 17.73E 148 06 11 72E | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S 38 35 44.47S 38 35 51.16S 38 34 57 | 23 50 35 21 21 10 9 9 | 348 76 66 228 304 279 269 264 | 2160 318 510 1223 1086 1971 1975 1980 | 2508 394 576 1451 1390 2250 2244 2244 | 2137 268 476 1202 1065 1961 1966 1971 | 2485 344 542 1430 1369 2240 2235 2235 |
| Investigator 1 Judith 1 Kahawai 1 Kingfish 1 Kingfish 2 Kingfish 3 Kinofish 4 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E 148 12 39.62E 148 10 17.73E 148 06 11.72E 148 05 53 42E | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S 38 35 44.47S 38 35 51.16S 38 34 57.16S 38 35 49.38S | 23 50 35 21 21 10 9 9 | 348 76 66 228 304 279 269 264 315 | 2160 318 510 1223 1086 1971 1975 1980 1922 | 2508 394 576 1451 1390 2250 2244 2244 2237 | 2137 268 476 1202 1065 1961 1966 1971 1912 | 2485 344 542 1430 1369 2240 2235 2235 2235 |
| Investigator 1 Judith 1 Kahawai 1 Kingfish 1 Kingfish 2 Kingfish 3 Kingfish 4 Kingfish 5 | 148 17 58.89E 147 58 30.00E 147 36 50.69E 148 33 24.68E 148 22 12.75E 148 12 39.62E 148 10 17.73E 148 06 11.72E 148 05 53.42E 148 14 34 24F | 38 36 02.48S 37 51 54.21S 37 54 44.17S 38 09 12.91S 38 10 15.30S 38 35 54.447S 38 35 51.16S 38 34 57.16S 38 35 49.38S 38 34 59.67S | 23 50 35 21 21 10 9 9 9 10 | 348 76 66 228 304 279 269 264 315 337 | 2160 318 510 1223 1086 1971 1975 1980 1922 1990 | 2508 394 576 1451 1390 2250 2244 2244 2237 2327 | 2137 268 476 1202 1065 1961 1966 1971 1912 1980 | 2485 344 542 1430 1369 2240 2235 2235 2225 2227 2317 |

| Well Name | Longitude | Latitude | KB | LEF | LEF | LEF | LEF | LEF |
|------------------|----------------|--------------|--------------|-----------|------|-------|--------------|---------------|
| | | | | thickness | top | base | top (msl) | base (msl) |
| Kingfish 7 | 148 05 04.13E | 38 35 08.18S | 25 | 266 | 1993 | 2259 | 1968 | 2234 |
| Kingfish 8 | 148 03 42.57E | 38 35 30.30S | 23 | 348 | 1923 | 2271 | 1900 | 2248 |
| Kingfish 9 | 148 08 59.72E | 38 37 39.77S | 23 | 392 | 1912 | 2304 | 1889 | 2281 |
| Kipper 1 | 148 35 51.35E | 38 10 30.30S | 21 | 356 | 1064 | 1420 | 1043 | 1399 |
| Kipper 2 | 148 36 49.77E | 38 11 26.03S | 22 | 304 | 1235 | 1539 | 1213 | 1517 |
| Kyarra 1A | 147 11 16.97E | 38 40 47.04S | 31 | 94 | 919 | 1013 | 888 | 982 |
| Lake Reeve 1 | 147 15 24.60E | 38 19 36.50S | 5 | 159 | 749 | 908 | 744 | 903 |
| Lakes Entrance 1 | 147 59 46.69E | 37 51 54.15S | 52 | 64 | 324 | 388 | 272 | 336 |
| Leatherjacket 1 | 148 46 46.38E | 38 05 11.29S | 21 | 110 | 635 | 745 | 614 | 724 |
| Longtom 1 | 148 18 58.79E | 38 05 54.77S | 25 | 61 | 1184 | 1245 | 1159 | 1220 |
| Luderick 1 | 147 43 02.49E | 38 26 15.10S | 21 | 248 | 1529 | 1777 | 1508 | 1756 |
| Macalister 1 | 147 08 19.92E | 38 20 57.325 | 20 | 117 | 675 | 792 | 655 | 0070 |
| Mackerel 1 | 148 21 30.60E | 38 28 48.465 | 30 | 182 | 2224 | 2406 | 2194 | 2376 |
| Mackerel 2 | 140 20 22.44E | 20 29 00.403 | 10 | 144 | 2100 | 2310 | 2100 | 2300 |
| | 140 21 40.07 E | 38 30 44 385 | 10 | 201 | 2214 | 2379 | 2204 | 2309 |
| Manta 1 | 148 43 24 26E | 38 16 21 755 | 25 | 422 | 1534 | 1956 | 1509 | 1031 |
| Marlin 1 | 148 13 37 68F | 38 13 57 175 | 10 | 135 | 1244 | 1379 | 1234 | 1369 |
| Marlin 2 | 148 10 49 60F | 38 15 53 46S | 10 | 100 | 1298 | 1442 | 1288 | 1432 |
| Marlin 3 | 148 10 20.71E | 38 14 38.15S | 10 | 100 | 1340 | 1440 | 1330 | 1430 |
| Marlin 4 | 148 16 07.19E | 38 14 18.91S | 10 | 185 | 1643 | 1828 | 1633 | 1818 |
| Mccreesh 1 | 147 06 21.75E | 38 22 21.21S | 31 | 130 | 670 | 800 | 639 | 769 |
| Meerlieu 4 | 147 18 52.11E | 38 01 18.85S | 20 | 141 | 684 | 825 | 664 | 805 |
| Meerlieu 15001 | 147 17 07.23E | 38 00 22.92S | 33 | 140 | 580 | 720 | 547 | 687 |
| Megamouth 1 | 148 16 31.85E | 38 35 44.23S | 22 | 378 | 2087 | 2465 | 2065 | 2443 |
| Melville 1 | 147 59 13.13E | 38 40 57.15S | 25 | 388 | 1830 | 2218 | 1805 | 2193 |
| Merriman 1 | 147 10 47.59E | 38 20 46.51S | 24 | 70 | 625 | 695 | 601 | 671 |
| Moonfish 1 | 148 00 35.21E | 38 08 54.95S | 23 | 220 | 1385 | 1605 | 1362 | 1582 |
| Moonfish 2 | 148 01 23.53E | 38 08 52.16S | 31 | 189 | 1370 | 1559 | 1339 | 1528 |
| Moray 1 | 148 03 25.25E | 38 51 42.58S | 10 | 218 | 1422 | 1640 | 1412 | 1630 |
| Morwong 1 | 148 18 49.91E | 38 13 37.08S | 10 | 160 | 1493 | 1653 | 1483 | 1643 |
| Mudskipper 1 | 148 08 02.84E | 38 54 26.07S | 27 | 255 | 1220 | 1475 | 1193 | 1448 |
| Mullet 1 | 147 51 26.68E | 39 12 56.49S | 10 | 70 | 620 | 690 | 610 | 680 |
| Mulloway 1 | 147 29 06.43E | 38 19 18.75S | 21 | 137 | 990 | 1127 | 969 | 1106 |
| Mullungdung 7 | 146 55 46.63E | 38 22 55.09S | 85 | 17 | 348 | 365 | 263 | 280 |
| Mullungdung 8 | 146 53 27.94E | 38 23 14.87S | 131 | 0 | 1000 | 0.400 | 1000 | |
| Nannygai 1 | 147 59 50.63E | 38 33 05.47S | 10 | 260 | 1932 | 2192 | 1922 | 2182 |
| NINDOO 2 | 147 19 26.90E | 37 52 27.715 | 75 | 58 | 292 | 350 | 217 | 275 |
| Northinght 1 | 149 09 03.4 IE | 37 55 52.465 | 25 | 105 | 470 | E7E | 146 | 551 |
| Oilco 1 | 147 12 20.40E | 37 51 42 485 | <u>4</u> | 83 | 321 | 404 | 270 | 362 |
| Omeo 1 | 147 43 06 90F | 38 36 39 505 | 31 | 306 | 1882 | 2188 | 1851 | 2157 |
| Omeo 2A | 147 42 43 01F | 38 36 16 355 | 22 | 300 | 1882 | 2182 | 1860 | 2160 |
| Opah 1 | 148 16 47 17F | 38 31 38 875 | 25 | 253 | 2152 | 2405 | 2127 | 2380 |
| Orange Roughy 1 | 148 02 35.61E | 38 34 51.59S | 25 | 365 | 1910 | 2275 | 1885 | 2250 |
| Palmer 1 | 147 19 51.52E | 38 33 43.83S | 21 | 131 | 1055 | 1186 | 1034 | 1165 |
| Patricia 1 | 148 26 51.83E | 38 01 47.44S | 22 | 45 | 655 | 700 | 633 | 678 |
| Patrobus 1 | 148 33 18.85E | 37 47 44.13S | 21 | 0 | | | | |
| Patties Pies 1 | 147 40 32.11E | 37 50 58.46S | 5 | 23 | 250 | 273 | 245 | 268 |
| Paynesville 1 | 147 40 25.89E | 37 54 47.18S | 30 | 39 | 530 | 569 | 500 | 539 |
| Perch 1 | 147 19 28.67E | 38 34 31.50S | 10 | 131 | 975 | 1106 | 965 | 1096 |
| Perch 2 | 147 20 02.28E | 38 34 17.61S | 21 | 118 | 1000 | 1118 | 979 | 1097 |
| Perch 3 | 147 19 21.42E | 38 34 09.47S | 42 | 122 | 974 | 1096 | 932 | 1054 |
| Petro Tech 1 | 147 59 39.67E | 37 24 49.48S | 49 | 80 | 301 | 381 | 252 | 332 |
| Pike 1 | 147 57 05.37E | 38 46 23.53S | 10 | 217 | 1611 | 1828 | 1601 | 1818 |
| Pilotfish 1A | 148 28 13.13E | 38 25 52.90S | 21 | 380 | 2535 | 2915 | 2514 | 2894 |
| Pisces 1 | 148 30 47.19E | 39 03 30.38S | 22 | 321 | 1475 | 1796 | 1453 | 1774 |
| Protea 1 | 147 08 53.98E | 38 11 24.82S | 51 | 0 | | | | |
| Remora 1 | 148 11 33.80E | 38 09 08.53S | 22 | 384 | 1700 | 2084 | 1678 | 2062 |

| Well Name | Longitude | Latitude | KB | LEF | LEF | LEF | LEF | LEF |
|-------------------------|---------------|----------------|----|-----------|------|------|-------|-------|
| | | | | thickness | top | base | top | base |
| | | | | | | | (msl) | (msl) |
| Rockling 1 | 148 13 50.38E | 38 27 29.08S | 31 | 277 | 2215 | 2492 | 2184 | 2461 |
| Roundhead 1 | 148 13 32.70E | 38 36 59.85S | 21 | 346 | 2032 | 2378 | 2011 | 2357 |
| Sale 13 | 147 13 05.71E | 38 06 53.64S | 1 | 125 | 687 | 812 | 686 | 811 |
| Sale 15 | 147 02 43.03E | 38 04 34.17S | 12 | 85 | 660 | 745 | 648 | 733 |
| Salmon 1 | 147 59 19.62E | 38 25 09.47S | 30 | 229 | 1760 | 1989 | 1730 | 1959 |
| Salt Lake 1 | 147 05 16.67E | 38 26 47.50S | 23 | 127 | 650 | 777 | 627 | 754 |
| Sawbelly 1 | 148 02 10.52E | 38 22 25.47S | 21 | 284 | 1700 | 1984 | 1679 | 1963 |
| Seacombe 7 | 147 28 01.58E | 38 05 08.17S | 9 | 176 | 862 | 1038 | 853 | 1029 |
| Seacombe South 1 | 151 39 07.95E | 85 17 12.95S | 2 | 121 | 960 | 1081 | 958 | 1079 |
| Seahorse 1 | 147 40 26.95E | 38 11 42.43S | 25 | 209 | 1180 | 1389 | 1155 | 1364 |
| Seahorse 2 | 147 39 24.79E | 38 12 07.76S | 21 | 233 | 1160 | 1393 | 1139 | 1372 |
| Selene 1 | 148 26 15.95E | 38 37 19.62S | 23 | 336 | 2486 | 2822 | 2463 | 2799 |
| Shark 1 | 149 03 12.05E | 38 15 28.73S | 28 | 290 | 1526 | 1816 | 1498 | 1788 |
| Signal Hill 1 | 147 18 49.59E | 38 14 19.50S | 28 | 126 | 555 | 681 | 527 | 653 |
| Smiler 1 | 148 23 21.71E | 38 28 49.64S | 25 | 199 | 2308 | 2507 | 2283 | 2482 |
| Snapper 1 | 148 00 54.63E | 38 11 57.47S | 10 | 125 | 1088 | 1213 | 1078 | 1203 |
| Snapper 2 | 148 02 41.71E | 38 11 10.17S | 10 | 153 | 1047 | 1200 | 1037 | 1190 |
| Snapper 3 | 147 59 15.70E | 38 12 39.17S | 10 | 205 | 1067 | 1272 | 1057 | 1262 |
| Snapper 4 | 148 00 18.62E | 38 12 48.85S | 21 | 214 | 1046 | 1260 | 1025 | 1239 |
| Snapper 5 | 147 59 27.08E | 38 13 12.13S | 21 | 190 | 1102 | 1292 | 1081 | 1271 |
| Snapper 6 | 148 00 46 61F | 38 13 50 03S | 21 | 177 | 1155 | 1332 | 1134 | 1311 |
| Snook 1 | 147 24 22.52E | 38 19 35.95S | 21 | 127 | 1000 | 1127 | 979 | 1106 |
| Sole 1 | 149 02 08 94F | 38 06 53 92S | 10 | 170 | 640 | 810 | 630 | 800 |
| Sole 2 | 149 00 33 55E | 38 06 13 08S | 25 | 205 | 570 | 775 | 545 | 750 |
| South West Bairnsdale 1 | 147 22 02 60F | 37 52 00 48S | 72 | 59 | 315 | 374 | 243 | 302 |
| Sneke 1 | 147 37 16 39E | 38 30 29 135 | 22 | 198 | 1622 | 1820 | 1600 | 1798 |
| Sperm Whale 1 | 148 21 56 24E | 38.03.20.325 | 9 | 93 | 708 | 801 | 600 | 792 |
| Sperm Whale Head 1 | 147 42 24 68F | 37 57 54 185 | 9 | 127 | 642 | 769 | 633 | 760 |
| Spoon Bay 1 | 147 28 01 88E | 38 04 50 685 | q | 147 | 875 | 1022 | 866 | 1013 |
| St Margaret Island 1 | 146 50 09 83E | 38 38 10 215 | 8 | 56 | 548 | 604 | 540 | 596 |
| Stonefish 1 | 148 33 39 36E | 38 14 56 64 5 | 10 | 95 | 1708 | 1803 | 1698 | 1793 |
| Stringy Bark 1 | 146 54 06 56E | 38 30 56 525 | 30 | 58 | 320 | 378 | 281 | 330 |
| Sunfich 1 | 140 34 00.30L | 38.08.20.205 | 10 | 151 | 1521 | 1682 | 1521 | 1672 |
| Sunfish 2 | 140 13 42.17 | 38 08 17 045 | 21 | 151 | 1/59 | 1610 | 1/27 | 1580 |
| Swoon 1 | 140 14 44.09L | 38 03 21 179 | 21 | 102 | 615 | 756 | 500 | 731 |
| Sweep 1 | 140 30 17.34 | 38 05 41 769 | 20 | 141 | 1361 | 1505 | 1340 | 1/0/ |
| Sweetlips 1 | 140 02 13.20L | 20 22 20 520 | 21 | 260 | 1720 | 1000 | 1705 | 1074 |
| Toilor 1 | 140 00 20.03E | 20 20 26 465 | 20 | 209 | 2110 | 1999 | 2100 | 2206 |
| | 140 10 29.01L | 20 20 21 646 | 21 | 200 | 1750 | 2400 | 1701 | 2390 |
| Tanuking 1 | 147 42 12.00E | 20 24 11 045 | 21 | 300 | 1132 | 2140 | 1140 | 2109 |
| Tarwillite 1 | 147 31 45.93E | 20 22 4 11.043 | 21 | 175 | 2125 | 2421 | 21149 | 2400 |
| Teragilii 1 | 140 20 34.73E | 30 22 45.455 | 21 | 200 | 2100 | 2421 | 2114 | 2400 |
| | 140 32 47.70E | 30 30 15.135 | 21 | 300 | 2007 | 2037 | 2010 | 2010 |
| | 140 15 27.07E | 27 46 21 466 | 20 | 219 | 21/0 | 2397 | 2100 | 2379 |
| | 140 10 00.00E | 37 40 31.105 | 40 | 0C 101 | 102 | 200 | 775 | 076 |
| | 147 08 38.38E | 38 36 41.915 | 21 | 101 | 796 | 897 | 1/5 | 8/6 |
| | 147 29 54.66E | 38 26 43.455 | 21 | 253 | 1078 | 1331 | 1057 | 1310 |
| | 148 23 44.59E | 38 17 17.455 | 10 | 284 | 1650 | 1934 | 1640 | 1924 |
| | 147 11 34.43E | 38 18 10.055 | 30 | 140 | 546 | 080 | 516 | 050 |
| Turne 4 | 148 21 02.01E | 38 24 42 995 | 21 | 263 | 2185 | 2448 | 2164 | 2427 |
| | 148 25 U7.58E | 38 10 19.455 | 10 | 259 | 1052 | 1311 | 1042 | 1301 |
| | 148 23 18.65E | 38 10 46 165 | 10 | 260 | 1070 | 1330 | 1060 | 1320 |
| Tuna 3 | 148 26 54.67E | 38 10 04.135 | 10 | 240 | 1085 | 1325 | 1075 | 1315 |
| iuna 4 | 148 22 12.68E | 38 11 15.45S | 21 | 270 | 1100 | 1370 | 1079 | 1349 |
| | 148 14 45.60E | 38 12 04 46S | 30 | 342 | 1600 | 1942 | 1570 | 1912 |
| Turrum 2 | 148 15 01.02E | 38 14 33.60S | 10 | 173 | 1373 | 1546 | 1363 | 1536 |
| I urrum 3 | 148 15 03.57E | 38 15 35.50S | 21 | 248 | 1323 | 1571 | 1302 | 1550 |
| Turrum 4 | 148 15 48.75E | 38 16 34.04S | 23 | 391 | 1528 | 1919 | 1505 | 1896 |
| Turrum 5 | 148 12 08.68E | 38 14 50.00S | 25 | 94 | 1292 | 1386 | 1267 | 1361 |
| Turrum 6 | 148 10 29.56E | 38 14 05.55S | 25 | 146 | 1314 | 1460 | 1289 | 1435 |

| Well Name | Longitude | Latitude | KB | LEF | LEF | LEF | LEF | LEF |
|-------------------|---------------|--------------|----|-----------|------|------|--------------|---------------|
| | | | | thickness | top | base | top (msl) | base (msl) |
| Turrum 7 | 148 15 53.91E | 38 15 46.42S | 26 | 244 | 1520 | 1764 | 1494 | 1738 |
| Veilfin 1 | 148 00 13.00E | 38 24 56.90S | 21 | 278 | 1708 | 1986 | 1687 | 1965 |
| Volador 1 | 148 32 41.35E | 38 25 22.71S | 25 | 375 | 2563 | 2938 | 2538 | 2913 |
| Wahoo 1 | 148 44 52.55E | 38 01 36.43S | 9 | 60 | 369 | 429 | 360 | 420 |
| Wellington Park 2 | 147 20 59.63E | 38 08 02.48S | 5 | 67 | 624 | 691 | 619 | 686 |
| West Fortescue 1 | 148 14 28.34E | 38 21 50.79S | 21 | 205 | 2216 | 2421 | 2195 | 2400 |
| West Halibut 1 | 148 17 01.47E | 38 24 07.73S | 25 | 247 | 2127 | 2374 | 2102 | 2349 |
| West Seahorse 1 | 147 37 26.33E | 38 12 11.65S | 9 | 210 | 1170 | 1380 | 1161 | 1371 |
| West Seahorse 2 | 147 36 43.16E | 38 12 16.32S | 9 | 212 | 1193 | 1405 | 1184 | 1396 |
| Whale 1 | 148 33 38.73E | 38 01 11.62S | 9 | 35 | 404 | 439 | 395 | 430 |
| Whaleshark 1 | 148 53 30.64E | 38 23 39.52S | 22 | 110 | 2612 | 2722 | 2590 | 2700 |
| Whiptail 1A | 147 31 14.23E | 38 19 24.84S | 21 | 140 | 985 | 1125 | 964 | 1104 |
| Whiting 1 | 147 53 05.55E | 38 14 06.24S | 21 | 118 | 1164 | 1282 | 1143 | 1261 |
| Whiting 2 | 147 51 19.16E | 38 14 59.15S | 21 | 86 | 1177 | 1263 | 1156 | 1242 |
| Wirrah 1 | 147 49 01.74E | 38 11 16.80S | 21 | 174 | 1291 | 1465 | 1270 | 1444 |
| Wirrah 2 | 147 49 31.21E | 38 10 55.41S | 21 | 191 | 1297 | 1488 | 1276 | 1467 |
| Wirrah 3 | 147 48 31.91E | 38 11 43.87S | 21 | 183 | 1306 | 1489 | 1285 | 1468 |
| Wrixondale 1 | 147 29 52.80E | 37 59 37.00S | 26 | 154 | 629 | 783 | 603 | 757 |
| Wombat 1 | 147 09 37.19E | 38 21 09.71S | 15 | 90 | 603 | 693 | 588 | 678 |
| Wonga Binda 1 | 147 02 30.50E | 38 26 57.04S | 30 | 60 | 530 | 590 | 500 | 560 |
| Woodside 2 | 146 53 46.66E | 38 37 37.53S | 9 | 58 | 701 | 759 | 692 | 750 |
| Woodside 12 | 146 59 23.36E | 38 32 05.64S | 4 | 116 | 752 | 868 | 748 | 864 |
| Woodside South 1 | 146 54 34.80E | 38 34 19.21S | 14 | 80 | 512 | 592 | 498 | 578 |
| Wooundellah 10 | 146 57 36.83E | 38 05 54.97S | 29 | 38 | 362 | 400 | 333 | 371 |
| Wooundellah 11 | 146 55 51.67E | 38 06 06.63S | 30 | 31 | 372 | 403 | 342 | 373 |
| Wrixondale 1 | 147 29 52.68E | 37 59 37.29S | 26 | 141 | 629 | 770 | 603 | 744 |
| Wurruk Wurruk 13 | 147 01 06.69E | 38 06 56.11S | 21 | 68 | 585 | 653 | 564 | 632 |
| Wyrallah 1 | 147 05 09.59E | 38 40 31.31S | 21 | 103 | 771 | 874 | 750 | 853 |
| Yellowtail 1 | 148 16 31.34E | 38 31 28.97S | 21 | 254 | 2151 | 2405 | 2130 | 2384 |
| Yellowtail 2 | 148 16 59.55E | 38 31 54.14S | 21 | 245 | 2163 | 2408 | 2142 | 2387 |

Appendix 2

ACS Laboratories (A) Interpreted Capillary Pressure charts, (B) Capillary Pressure plots and (C) Pore Size Distribution plots from Mercury Injection Capillary Pressure analysis of 37 core samples.

| Well | |
|--------------|--|
| Sample Depth | |

Barracouta-1 1021.95 m



| Client | Geoscience Victoria | | | | | | Conversion Parameters | | | | | | |
|------------------|---------------------|---------------------|------------------|------------------|------------------|-----------|-----------------------|-------------------------|--------------|-----------|-------------------|-------------------|--|
| Well | Barracouta-1 | | | | | | | | | air/water | air/oil | oil/water | |
| | | | | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 | |
| Test Method | Air/Mercury Ca | pillary Pressure Dr | ainage | | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 | |
| e 1 | Demas and a | | | | | | Reservoir Theta | | | 0.0 | | 30.0 | |
| Sample | 1021 95 | m | | Ambient Permer | admity v | | Laboratory TcosT | Theta | | 72.0 | 24.0 | 42.0 | |
| Deptil | 1021.95 | | | Amblent i orosit | 3 | | Reservoir TcosTh | ieta | | 50.0 | 24.0 | 26.0 | |
| pore radius (µm) |) | | | | | | D | ensity Gradients, psi/f | oot | | | | |
| 0.063 | Entry Pressure (| psia) | Displacement Pre | essure (psia) | Threshold Pressu | re (psia) | | _ | Typical |] | | | |
| System | Lab 1702 | Resv | Lab | Resv | Lab 2001 | Resv | Water: | | 0.440 | | | | |
| G-W | 334.1 | 232.0 | 549.3 | 381.5 | 588.8 | 408.9 | Gas: | | 0.100 | | | | |
| O-W | 111.4 | 120.6 | 183.1 | 198.4 | 196.3 | 212.6 | | | | 1 | | | |
| | | | | | | | | | | | | | |
| Processo | | Intrusion | | Saturation | | Pore | Equivalent | Injection Pressures | O/P Lab | O/P Par | Height Above Free | Height Above Free | |
| (psia) | | (percent) | | (percent) | | (μm) | A/B Lab | A/D Res | O/B Lab | 0/B Res | Oil-Water | Gas-Water | |
| 1.00 | | 0.0 | | 0.0 | | 212 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 | |
| 1.00 | | 0.0 | | 0.0 | | 213 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 | |
| 1.98 | | 0.0 | | 0.0 | | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 | |
| 2.73 | | 0.0 | | 0.0 | | 77.7 | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.09 | |
| 3.18 | | 0.0 | | 0.0 | | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 | |
| 3.73 | | 0.0 | | 0.0 | | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 | |
| 5.18 | | 0.0 | | 0.0 | | 40.9 | 1.0 | 0.71 | 0.59 | 0.37 | 3.34 | 2.07 | |
| 5.98 | | 0.0 | | 0.0 | | 35.5 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | |
| 6.97 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.49 | 2.79 | |
| 8.27 | | 0.0 | | 0.0 | | 25.6 | 1.6 | 1.1 | 0.95 | 0.59 | 5.33 | 3.31 | |
| 9.9/ | | 0.0 | | 0.0 | | 21.5 | 2.0 | 1.4 | 1.1 | 0.71 | 0.42 | 5.99 4.61 | |
| 13.5 | | 0.0 | | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 | |
| 15.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 1.8 | 1.1 | 9.98 | 6.21 | |
| 18.5 | | 0.0 | | 0.0 | | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 | |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 16.29 | 8.65 | |
| 30.0 | | 0.0 | | 0.0 | | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 | |
| 39.9 | | 0.0 | | 0.0 | | 5.32 | 7.8 | 5.4 | 4.6 | 2.8 | 25.70 | 15.98 | |
| 48.5 | | 0.0 | | 0.0 | | 4.38 | 9.5 | 6.6 | 5.6 | 3.4 | 31.24 | 19.42 | |
| 58.9 | | 0.0 | | 0.0 | | 3.60 | 12 | 8.0 | 6.7 | 4.2 | 37.93 | 23.59 | |
| 79.7 | | 0.0 | | 0.0 | | 2.66 | 16 | 11 | 9.1 | 5.6 | 51.33 | 31.92 | |
| 92.5 | | 0.0 | | 0.0 | | 2.29 | 18 | 13 | 11 | 6.6 | 59.57 | 37.05 | |
| 112 | | 0.0 | | 0.0 | | 1.89 | 22 | 15 | 13 | 7.9 | 72.13 | 44.85 | |
| 130 | | 0.0 | | 0.0 | | 1.63 | 25 | 18 | 15 | 9.2 | 83.73 | 52.06 | |
| 181 | | 0.0 | | 0.0 | | 1.17 | 35 | 25 | 21 | 13 | 116.6 | 72.49 | |
| 211 | | 0.0 | | 0.0 | | 1.00 | 41 | 29 | 24 | 15 | 135.9 | 84.50 | |
| 247 | | 0.0 | | 0.0 | | 0.858 | 48 | 34 | 28 | 17 | 159.1 | 98.92 | |
| 290 | | 0.0 | | 0.0 | | 0.730 | 57 | 39 47 | 33 | 21 | 186.8 | 137.0 | |
| 402 | | 0.0 | | 0.0 | | 0.527 | 79 | 55 | 46 | 28 | 258.9 | 161.0 | |
| 473 | | 0.0 | | 0.0 | | 0.448 | 93 | 64 | 54 | 34 | 304.6 | 189.4 | |
| 554 | | 0.0 | | 0.0 | | 0.383 | 109 | 75 | 63 | 39 | 356.8 | 221.9 | |
| 757 | | 0.0 | | 0.0 | | 0.280 | 148 | 103 | 87 | 46 54 | 487.5 | 303.2 | |
| 889 | | 0.0 | | 0.0 | | 0.239 | 174 | 121 | 102 | 63 | 572.6 | 356.0 | |
| 1048 | | 0.0 | | 0.0 | | 0.202 | 205 | 143 | 120 | 74 | 675.0 | 419.7 | |
| 1228 | | 0.0 | | 0.0 | | 0.173 | 241 | 16/ | 141 | 87 | 790.9 | 491.8 | |
| 1687 | | 0.0 | | 0.0 | | 0.146 | 331 | 230 | 193 | 120 | 1086 | 675.6 | |
| 1828 | | 0.6 | | 0.0 | | 0.116 | 358 | 249 | 209 | 130 | 1177 | 732.1 | |
| 2143 | | 1.0 | | 1.0 | | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 | |
| 2507 | | 1.0 | | 2.6 | | 0.0846 | 492 | 541 401 | 26/ 337 | 209 | 1896 | 1004 | |
| 3447 | | 22.3 | | 29.3 | | 0.0615 | 676 | 469 | 394 | 244 | 2220 | 1380 | |
| 4038 | | 27.1 | | 56.4 | | 0.0525 | 792 | 550 | 462 | 286 | 2601 | 1617 | |
| 4732 | | 18.9 | | 75.3 | | 0.0448 | 928 | 644 697 | 542 586 | 335 | 3048 | 1895 | |
| 6004 | | 7.5 | | 87.8 | | 0.0414 | 1177 | 818 | 687 | 425 | 3867 | 2405 | |
| 7032 | | 5.7 | | 93.5 | | 0.0301 | 1379 | 958 | 805 | 498 | 4529 | 2816 | |
| 7896 | | 3.6 | | 97.0 | | 0.0268 | 1548 | 1075 | 904 | 559 | 5085 | 3162 | |
| 8927 | | 2.2 | | 99.2 | | 0.0237 | 1/50 | 1216 | 1022 | 632 | 5749 | 35/5 | |
| 10459 | | 0.2 | | 100.0 | | 0.0213 | 2051 | 1424 | 1197 | 741 | 6736 | 4189 | |
| 12283 | | 0.0 | | 100.0 | | 0.0173 | 2408 | 1673 | 1406 | 870 | 7911 | 4919 | |
| 14332 | | 0.0 | | 100.0 | | 0.0148 | 2810 | 1952 | 1640 | 1015 | 9230 | 5740 | |
| 16382 | | 0.0 | | 100.0 | | 0.0129 | 3212 3624 | 2231 | 18/5 | 1161 | 10551 | 0001 7401 | |
| 20484 | | 0.0 | | 100.0 | | 0.0113 | 4016 | 2789 | 2344 | 1451 | 13193 | 8204 | |
| 23149 | | 0.0 | | 100.0 | | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 | |
| 25065 | | 0.0 | | 100.0 | | 0.0085 | 4915 | 3413 | 2868 | 1776 | 16143 | 10038 | |
| 2/136 | | 0.0 | | 100.0 | | 0.0078 | 5321 | 3695 4000 | 3105 | 1922 | 1/477 | 10868 | |
| 31805 | | 0.0 | | 100.0 | | 0.0072 | 6236 | 4331 | 3640 | 2081 | 20484 | 12737 | |
| 34422 | | 0.0 | | 100.0 | | 0.0062 | 6749 | 4687 | 3939 | 2439 | 22169 | 13786 | |
| 37194 | | 0.0 | | 100.0 | | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14896 | |
| 40343 | | 0.0 | | 100.0 | | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25983 | 16157 | |
| 45592 47293 | | 0.0 | | 100.0 | | 0.0049 | 6547 9273 | 5936 6440 | 4989 5412 | 3088 | 28075 30459 | 1/458 18940 | |
| 51171 | | 0.0 | | 100.0 | | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32956 | 20493 | |
| 55384 | | 0.0 | | 100.0 | | 0.0038 | 10860 | 7541 | 6338 | 3924 | 35670 | 22181 | |
| 59879 | | 0.0 | | 100.0 | | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38565 | 23981 | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



| Well Sample | Depth | | B 9 | engword 14.9 m | en South-6 | | | | | | |
|----------------|-------------|----------------|-------------|--------------------|----------------------|-----------------|--------------------|----------------|-----------------|--------------|------------------------|
| Client | Geoscience | AVictoria | | Density (| Gradients (psi/foot) | | Con | ersion Paramet | ers (dvnes/cm |) | |
| Well | Bengworden | South-6 | | Density | Typical | | Con | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Pres | sure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | BS6 | | | Gas. | 0.100 | Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 914.90 m | | | CO2 Density | 0.237 | Laboratory Tco: | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| · · | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| n | | 0.042 | | R (| Estimated Column | Entry I | Pressure (psia) | Displacement | Pressure (psia) | Threshold P | ressure (psia) |
| Pore radius (µ | ım) | 0.043 | | A-Hg | na | 2477 | Res Con | Lab 3115 | Resv | 120 3248 | Kesv |
| | | | | G-W | 993 | 486 | 337 | 611 | 424 | 637 | 442 |
| | | | | O-W | 1595 | 162 | 175 | 204 | 221 | 212 | 230 |
| | | | | CO ₂ -W | 531 | 486 | 175 | 611 | 221 | 637 | 230 |
| | | | | | | Equivalant | Injustion Programs | Oil/Prine | Oil/Prine | Haight Abova | Haight Abour |
| | Rav | / Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2.73 | 0.3 | 0.8 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.1 | 1.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.1 | 1.1 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.1 | 1.2 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.1 | 1.5 | 0.0 | 0.0 | 35.5 | 1.02 | 0.71 | 0.59 | 0.37 | 3.54 | 2.08 |
| 6.97 | 0.1 | 1.5 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.42 | 4.49 | 2.80 |
| 8.27 | 0.1 | 1.6 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.1 | 1.7 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.1 | 1.8 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 15.5 | 0.1 | 2.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.54 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.1 | 2.2 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.1 | 2.3 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.5 | 2.8 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.2 | 3.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 47.2 | 0.0 | 3.0 | 0.0 | 0.0 | 4 49 | 9 25 | 6.42 | 5 40 | 3 34 | 30.4 | 18.9 |
| 56.6 | 0.0 | 3.0 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 | 0.0 | 3.1 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 | 0.1 | 3.2 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 0.1 | 3.5 | 0.0 | 0.0 | 2.28 | 21.8 | 12.0 | 10.6 | 0.30 7.86 | 59.6 71.5 | 57.1 44.4 |
| 129 | 0.1 | 3.5 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.1 | 3.6 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 179 | 0.1 | 3.7 | 0.0 | 0.0 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 | 0.1 | 3.8 | 0.0 | 0.0 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.2 | 4.0 | 0.0 | 0.0 | 0.800 | 40.4 57 3 | 39.8 | 28.5 | 20.7 | 139 | 117 |
| 343 | 0.2 | 4.3 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 | 0.2 | 4.5 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 0.2 | 4.7 | 0.0 | 0.0 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 647 | 0.2 | 5.0 | 0.0 | 0.0 | 0.383 | 108 | /5.0 | 63.3 74.0 | 39.2 45.8 | 356 416 | 221 |
| 757 | 0.3 | 5.5 | 0.0 | 0.0 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 887 | 0.4 | 5.9 | 0.0 | 0.0 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 0.5 | 6.4 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 0.5 | 6.9 7.6 | 0.0 | 0.0 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 576 |
| 1688 | 0.9 | 8.5 | 0.0 | 0.0 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 0.6 | 9.1 | 0.0 | 0.0 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 1.6 | 10.7 | 1.7 | 1.7 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 2.6 | 13.3 | 2.8 | 4.5 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 3449 | 4.5 | 30.9 | 4.8 14.7 | 24.0 | 0.0615 | 676 | 469 | 395 | 209 | 2227 | 1379 |
| 4040 | 35.6 | 66.5 | 39.2 | 63.2 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 33.1 | 99.6 | 36.4 | 99.6 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.1 | 99.7 | 0.2 | 99.7 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 7033 | 0.2 | 99.9 100 0 | 0.2 | 99.9 100.0 | 0.0353 | 1177 | 817 | 687 805 | 425 | 3864 4527 | 2403 |
| 7895 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0269 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| 8920 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.01/3 | 2408 | 10/2 | 1406 | 870 | 7909 9227 | 4918 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3695 | 2808 | 1//5 | 10130 | 10038 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 43501 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 4980 | 2858 | 25982 | 16156 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |

Bengworden South-6







ACS LABORATORIES PTY. LTD.

| /ell ample | Depth | | B 5 | undalagu 99.8 m | ah-10 | | | | | | LAE |
|-----------------------------|--|--|-----------------------------------|---|--|---|--|--|---|---|---|
| lient /ell est Method | Geoscience A Bundalaguah Air/Mercury | 4 Victoria 1-10 Capillary Pressure | ð | Density G Water: Oil: Gas: | radients (psi/foot) Typical 0.440 0.330 0.100 | Laboratory The Laboratory IFT Reservoir Theta | Con | version Paramet air/water 0.0 72.0 0.0 | ers (dynes/cm) air/oil 0.0 24.0 | oil/water 30.0 48.0 30.0 | CO ₂ /water 0.0 72.0 0.0 |
| ample epth | B10 599.80 m | | | CO2 Density | 0.155 | Reservoir IFT Laboratory Tco Reservoir Tcos | sTheta | 50.0 72.0 50.0 | 24.0 | 30.0 42.0 26.0 | 26.0 72.0 26.0 |
| ore radius (µ | .m) | 1.33 | | System A-Hg G-W | Estimated Column Height (feet) na 32 | Entry I Lab 79.9 15.7 | Pressure (psia) Res Con - 10.9 | Displacement I Lab 343 67.4 | Pressure (psia) Resv - 46.8 | Threshold P Lab 467 91.7 | ressure (psia) Resv - 63.7 |
| | | | | CO ₂ -W | 15 | 15.7 | 5.66 | 67.4 | 24.3 | 91.7 | 33.1 |
| Pressure (psia) | Raw Intrusion (percent) | Data Saturation (percent) | Conform Intrusion (percent) | ance Corrected Saturation (percent) | Pore Diameter (µm) | Equivalent Air/Brine Lab (psi) | Injection Pressures Air/Brine Res Con (psi) | Oil/Brine Lab Conditions (psi) | Oil/Brine Reservoir Conditions (psi) | Height Above Free Water Oil-Water (feet) | Height Above Free Water Gas-Water (feet) |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2.73 | 0.1 | 0.4 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.25 | 0.14 | 1.28 | 1.09 |
| 3.18 | 0.1 | 0.5 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 4.38 | 0.1 | 0.5 | 0.0 | 0.0 | 48.4 | 0.73 | 0.60 | 0.43 | 0.26 | 2.40 | 1.49 |
| 5.18 | 0.1 | 0.7 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 6.97 | 0.1 | 0.8 0.8 | 0.0 0.0 | 0.0 | 35.5 30.4 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 4.49 | 2.39 |
| 8.27 | 0.1 | 0.9 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.1 | 1.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.1 | 1.1 | 0.0 | 0.0 | 15.7 | 2.25 | 1.30 | 1.52 | 0.82 | 8.66 | 4.39 |
| 15.5 | 0.1 | 1.3 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 21.6 | 0.1 | 1.4 | 0.0 0.0 | 0.0 0.0 | 11.5 9.83 | 3.63 4.24 | 2.52 2.94 | 2.12 2.47 | 1.31 | 11.9 13.9 | 7.41 |
| 25.3 | 0.1 | 1.6 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.2 | 1.8 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 47.2 | 0.1 | 2.0 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 4.20 | 3.34 | 30.4 | 14.9 |
| 56.6 | 0.2 | 2.2 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 80.4 | 0.2 | 2.4 | 0.0 | 0.0 | 3.20 2.64 | 13.0 | 9.03 | 7.59 9.20 | 4.70 | 42.7 | 26.6 |
| 93.0 | 0.6 | 3.4 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.6 | 3.9 | 0.6 | 0.6 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 152 | 1.1 | 5.7 | 1.1 | 2.5 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 179 | 1.4 | 7.1 | 1.4 | 3.9 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 247 | 1.4 | 8.5 10.2 | 1.4 | 5.3 7.1 | 0.860 | 41.2 48.4 | 28.6 33.6 | 24.0 28.3 | 14.9 | 135 | 84.1 98.8 |
| 292 | 2.0 | 12.2 | 2.0 | 9.1 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 401 | 2.1 2.3 | 14.3 16.6 | 2.2 | 11.3 | 0.619 | 67.3 78.6 | 46.7 54.6 | 39.3 45.9 | 24.3 28.4 | 221 | 137 |
| 472 | 2.5 | 19.2 | 2.6 | 16.3 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 647 | 2.8 | 22.0 24.6 | 2.9 2.7 | 19.3 22.0 | 0.383 | 108 127 | 75.0 88.2 | 63.3 74.0 | 39.2 45.8 | 356 416 | 221 259 |
| 757 | 3.0 | 27.6 | 3.1 | 25.1 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 887 | 3.3 | 30.9 | 3.4 | 28.5 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 5.0 4.0 | 34.5 38.6 | 5.8 4.2 | 32.3 36.4 | 0.202 | 205 | 142 | 120 | /4.3 86.7 | 0/5 788 | 418 |
| 1439 | 4.5 | 43.0 | 4.6 | 41.0 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 5.2 2.9 | 48.2 51.1 | 5.4 3.0 | 46.4 49.4 | 0.126 0.116 | 331 358 | 230 249 | 193 209 | 119 | 1082 | 676 732 |
| 2142 | 6.0 | 57.2 | 6.3 | 55.7 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 2945 | 6.8 7.0 | 64.0 71.0 | 7.0 | 62.7 70.0 | 0.0845 | 492 577 | 342 401 | 287 337 | 178 209 | 1618 1900 | 1006 1179 |
| 3449 | 6.6 | 77.6 | 6.8 | 76.8 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4040 4728 | 5.8 | 83.3 89.6 | 6.0 6.4 | 82.8 | 0.0525 | 792 927 | 550 644 | 462 | 286 | 2600 | 1618 |
| 5114 | 1.7 | 91.3 | 1.8 | 91.0 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 3.2 | 94.5 | 3.3 | 94.3 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7895 | 2.0 | 98.6 | 1.5 | 97.0 | 0.0269 | 1548 | 1075 | 805 904 | 498 560 | 4327 5091 | 3162 |
| 8920 | 0.9 | 99.4 | 0.9 | 99.4 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 10452 | 0.3 | 99.7 99.9 | 0.3 | 99.7 99.9 | 0.0220 | 2049 | 1314 1423 | 1104 | 683 740 | 6209 6727 | 3865 4185 |
| 12283 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 16381 | 0.0 0.0 | 100.0 100.0 | 0.0 0.0 | 100.0 100.0 | 0.0148 0.0129 | 2810 3212 | 1951 2231 | 1640 1875 | 1015 1161 | 9227 10555 | 5738 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 4530 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 31804 | 0.0 | 100.0 | 0.0 0.0 | 100.0 | 0.0072 0.0067 | 5760 6236 | 4000 4331 | 3362 3640 | 2081 2253 | 18918 20482 | 11765 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0055 | 8547 | 5935 | 4989 | 2038 | 23982 28073 | 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51172 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 7542 | 5856 6339 | 3625 3924 | 32955 35673 | 20494 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |









WellCSample Depth1



Cod-1 1771.89 m

| Client Well | Geoscience Victoria | | | - | | Conversio | n Parameters air/water | air/oil | oil/water |
|------------------|-----------------------------------|-----------------|---------------|------------------|------------------------|------------|---------------------------|-------------------|-------------------|
| wen | 0001 | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 |
| Test Method | Air/Mercury Capillary Pressure Dr | ainage | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 |
| 6 | Cod 1 | A mikima A Demo | - L 114- | Reservoir Theta | | | 0.0 | | 30.0 |
| Depth | 1711.89 m | Ambient Perme | abinty tv | Laboratory TcosT | Theta | | 72.0 | 24.0 | 42.0 |
| | - | | | Reservoir TcosTh | neta | | 50.0 | | 26.0 |
| pore radius (µm) | | D: 1 (D ()) | 71 1 110 (`) | D | ensity Gradients, psi/ | foot | 4 | | |
| 0.030 System | Lab Resv | Lab Resv | Lab Resv | Water | | 0 440 | ł | | |
| A-Hg | 3547.7 - | 5070 - | 5787 - | Oil: | | 0.330 | | | |
| G-W | 696.0 483.3 | 994.7 690.7 | 1135.3 788.4 | Gas: | | 0.100 | 1 | | |
| 0-W | 232.0 251.3 | 331.6 359.2 | 3/8.4 410.0 | | | | | | |
| | | | Dora | Equivalant | Injustion Processor | | | Haight Abova Fraa | Haight Abova Fraa |
| Pressure | Intrusion | Saturation | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) |
| (psia) | (percent) | (percent) | (µm) | | | | | Oil-Water | Gas-Water |
| | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 213 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.00 | 0.0 | 0.0 | 213 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2 73 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 3.18 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 |
| 5.98 | 0.0 | 0.0 | 35.5 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.0 | 0.0 | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.49 | 2.79 |
| 8.27 | 0.0 | 0.0 | 25.6 | 1.6 | 1.1 | 0.95 | 0.59 | 5.33 | 3.31 |
| 11.5 | 0.0 | 0.0 | 18.5 | 2.0 | 1.4 | 1.3 | 0.81 | 7.41 | 4.61 |
| 13.5 | 0.0 | 0.0 | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 |
| 15.5 | 0.0 | 0.0 | 13.7 | 3.0 | 2.1 | 1.8 | 1.1 | 9.98 | 6.21 |
| 21.6 | 0.0 | 0.0 | 9.83 | 4.2 | 2.5 | 2.1 | 1.5 | 13.91 | 8.65 |
| 25.3 | 0.0 | 0.0 | 8.39 | 5.0 | 3.4 | 2.9 | 1.8 | 16.29 | 10.13 |
| 30.0 | 0.0 | 0.0 | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 |
| 48.3 | 0.0 | 0.0 | 5.33 | 7.8 9.5 | 5.4 | 4.5 | 2.8 | 25.57 | 15.90 |
| 58.7 | 0.0 | 0.0 | 3.61 | 12 | 8.0 | 6.7 | 4.2 | 37.81 | 23.51 |
| 68.6 | 0.0 | 0.0 | 3.09 | 13 | 9.3 | 7.9 | 4.9 | 44.18 | 27.47 |
| 79.6 92.3 | 0.0 | 0.0 | 2.66 | 16 | 11 | 9.1 | 5.6 | 51.27 | 31.88 |
| 112 | 0.0 | 0.0 | 1.90 | 22 | 15 | 13 | 7.9 | 72.13 | 44.85 |
| 130 | 0.0 | 0.0 | 1.64 | 25 | 18 | 15 | 9.2 | 83.73 | 52.06 |
| 152 | 0.0 | 0.0 | 1.40 | 30 | 21 | 21 | 11 | 97.89 | 60.87 72.49 |
| 211 | 0.0 | 0.0 | 1.00 | 41 | 29 | 24 | 15 | 135.9 | 84.50 |
| 247 | 0.0 | 0.0 | 0.859 | 48 | 34 | 28 | 17 | 159.1 | 98.92 |
| 290 | 0.0 | 0.0 | 0.731 | 57 | 39 47 | 33 | 21 | 186.8 | 116.1 |
| 402 | 0.0 | 0.0 | 0.527 | 79 | 55 | 46 | 28 | 258.9 | 161.0 |
| 473 | 0.0 | 0.0 | 0.448 | 93 | 64 | 54 | 34 | 304.6 | 189.4 |
| 554 647 | 0.0 | 0.0 | 0.383 | 109 | 75 | 63 74 | 39 | 356.8 | 221.9 |
| 757 | 0.0 | 0.0 | 0.280 | 148 | 103 | 87 | 54 | 487.5 | 303.2 |
| 889 | 0.0 | 0.0 | 0.239 | 174 | 121 | 102 | 63 | 572.6 | 356.0 |
| 1228 | 0.0 | 0.0 | 0.202 | 203 | 143 | 120 | 87 | 790.9 | 491.8 |
| 1436 | 0.0 | 0.0 | 0.148 | 282 | 196 | 164 | 102 | 924.8 | 575.1 |
| 1687 | 0.0 | 0.0 | 0.126 | 331 | 230 | 193 | 120 | 1086 | 675.6 |
| 2143 | 0.0 | 0.0 | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 |
| 2507 | 0.0 | 0.0 | 0.0846 | 492 | 341 | 287 | 178 | 1615 | 1004 |
| 2944 | 0.0 | 0.0 | 0.0720 | 577 | 401 | 337 | 209 | 1896 | 1179 |
| 4040 | 0.9 | 0.9 | 0.0525 | 792 | 550 | 462 | 286 | 2602 | 1618 |
| 4735 | 2.1 | 3.0 | 0.0448 | 928 | 645 | 542 | 335 | 3050 | 1896 |
| 5120 | 3.2 | 4.5 | 0.0414 | 1004 | 697 818 | 586 687 | 363 426 | 3297 | 2050 |
| 7035 | 12.1 | 22.2 | 0.0301 | 1379 | 958 | 805 | 498 | 4531 | 2817 |
| 7898 | 14.1 | 36.3 | 0.0268 | 1549 | 1075 | 904 | 560 | 5087 | 3163 |
| 8929 | 10.9 | 47.3 | 0.0237 | 1751 | 1216 | 1022 | 633 | 5751 | 3576 |
| 10461 | 5.0 | 58.4 | 0.0203 | 2051 | 1424 | 1197 | 741 | 6737 | 4189 |
| 12285 | 7.8 | 66.2 | 0.0173 | 2409 | 1673 | 1406 | 870 | 7912 | 4920 |
| 14333 | 8.3 | 74.5 | 0.0148 | 2810 | 1952 | 1640 | 1015 | 9231 | 5740 |
| 18481 | 4.7 | 85.6 | 0.0129 | 3624 | 2516 | 2115 | 1309 | 11903 | 7401 |
| 20484 | 2.8 | 88.5 | 0.0103 | 4016 | 2789 | 2344 | 1451 | 13193 | 8204 |
| 23149 | 2.6 | 91.1 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 27136 | 1.5 | 92.5 | 0.0085 | 5321 | 3695 | 3105 | 1922 | 17477 | 10868 |
| 29378 | 1.2 | 95.1 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18921 | 11766 |
| 31805 | 1.1 | 96.2 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20484 | 12737 |
| 37194 | 0.8 | 98.0 | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14896 |
| 40343 | 0.7 | 98.8 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25983 | 16157 |
| 43592 | 0.5 | 99.3 00 ¢ | 0.0049 | 8547 | 5936 | 4989 | 3088 | 28075 | 17458 |
| 51171 | 0.4 | 99.8 99.8 | 0.0043 | 10034 | 6968 | 5856 | 3625 | 32956 | 20493 |
| 55385 | 0.1 | 99.9 | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35670 | 22181 |
| 59879 | 0.1 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38565 | 23981 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



| Well Sample | Depth | | | Colqu 180.7 | houn East-6 ' m | | | | | | LAE |
|----------------|--------------|------------------|------------|--------------------|----------------------|-----------------|---------------------|-----------------|-----------------|--------------|------------------------|
| Client | Geoscience A | A Victoria | | Density C | Gradients (psi/foot) | r | Conv | version Paramet | ers (dynes/cm) | 1 | |
| Well | Colquhoun E | East-6 | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Pressu | ıre | Oil: Gas: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | CE6 | | | 0.03. | 0.100 | Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 180.70 m | | | CO2 Density | 0.035 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| - | | | | - | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| в P (| | 0.105 | | Contant | Estimated Column | Entry F | ressure (psia) | Displacement I | Pressure (psia) | Threshold P | ressure (psia) |
| Pore radius (p | um) | 0.105 | | A-Hg | na na | 1011 | Kes Con | 1185 | Resv | 1389 | Resv |
| | | | | G-W | 405 | 198 | 138 | 232 | 161 | 272 | 189 |
| | | | | O-W | 651 | 66.1 | 71.6 | 77.5 | 83.9 | 90.8 | 98.4 |
| | | | | CO ₂ -W | 171 | 198 | 71.6 | 232 | 83.9 | 272 | 98.4 |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| | Raw | / Data | Conforma | nce Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (ps1) | (psi) | (ps1) | (feet) | (feet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.7 | 0.7 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 3.18 | 0.5 | 1.1 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.09 |
| 3.73 | 0.1 | 1.3 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.2 | 1.5 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.1 | 1.5 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.2 | 1.7 | 0.0 | 0.0 | 35.5 30.4 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 4.49 | 2.39 |
| 8.27 | 0.1 | 1.8 | 0.0 | 0.0 | 25.6 | 1.57 | 1.13 | 0.80 | 0.49 | 5.33 | 3.32 |
| 9.97 | 0.2 | 2.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.1 | 2.1 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.2 | 2.3 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.1 | 2.3 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.// | 1.10 | 10.0 | 6.21 7.41 |
| 21.6 | 0.0 | 2.4 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.3 | 2.7 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.1 | 2.8 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.1 | 2.9 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.1 | 2.9 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 6.48 | 3.34 4.01 | 30.4 36.5 | 18.9 |
| 66.3 | 0.0 | 3.1 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 | 0.1 | 3.2 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 0.1 | 3.3 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.2 | 3.5 | 0.2 | 0.2 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.1 | 3.7 | 0.1 | 0.3 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 179 | 0.2 | 4.0 | 0.2 | 0.7 | 1.18 | 35.1 | 24.4 | 20.5 | 10.0 | 115 | 71.8 |
| 210 | 0.2 | 4.3 | 0.2 | 1.0 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.2 | 4.5 | 0.2 | 1.2 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 0.4 | 4.8 | 0.4 | 1.5 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 401 | 0.3 | 5.3 | 0.3 | 2.1 | 0.528 | 78.6 | 54.6 | 45.9 | 24.5 | 258 | 161 |
| 472 | 0.3 | 5.6 | 0.3 | 2.4 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.4 | 6.1 | 0.5 | 2.8 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 | 0.5 | 6.5 | 0.5 | 3.3 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| 887 | 0.7 | 7.5 | 0.8 | 4.1 | 0.280 | 148 | 103 | 102 | 55.0 63.1 | 487 | 303 |
| 1048 | 1.4 | 9.7 | 1.5 | 6.6 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 2.6 | 12.3 | 2.6 | 9.2 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 4.2 | 16.4 | 4.3 | 13.5 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1828 | 0.8 5.8 | 23.2 | 6.0 | 20.6 | 0.126 | 358 | 230 | 209 | 119 | 1082 | 732 |
| 2142 | 9.6 | 38.6 | 10.0 | 36.5 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 11.8 | 50.5 | 12.3 | 48.8 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | 10.7 | 61.2 | 11.1 | 59.9 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 5449 4040 | 8.1 5 Q | 09.3 75.2 | 8.3 6.1 | 68.2 74.3 | 0.0615 | 0/6 792 | 469 | 595 462 | 245 286 | 2227 | 13/9 |
| 4728 | 6.2 | 81.4 | 6.5 | 80.8 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 2.0 | 83.4 | 2.1 | 82.9 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 3.4 | 86.8 | 3.5 | 86.4 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 3.0 | 89.8 | 3.1 | 89.5 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 8920 | 1.7 | 93.2 | 1.8 | 93.0 | 0.0238 | 1548 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 1.0 | 94.1 | 1.0 | 93.9 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.8 | 95.0 | 0.8 | 94.8 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 1.3 | 96.3 | 1.4 | 96.2 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 1.2 | 97.5 | 1.2 | 97.4 98.2 | 0.0148 | 2810 | 1951 | 1640 1875 | 1015 | 9227 | 5/38 6562 |
| 18481 | 0.6 | 98.9 | 0.6 | 98.8 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.4 | 99.3 | 0.4 | 99.3 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 | 0.3 | 99.6 | 0.4 | 99.6 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.2 | 99.8 | 0.2 | 99.8 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.1 | 99.9 100.0 | 0.1 | 99.9 100.0 | 0.0078 | 5321 5760 | 3695 | 3362 | 1922 2081 | 1/4/3 | 10868 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 45591 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 804/ 9773 | 5955 6440 | 4989 | 3350 | 28073 | 1/450 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |

Wall

Colauboun East 6



(B) Capillary Pressure Plot



ACS LABORATORIES

| Sample | Depth | | | 478. | lm | | | | | | |
|----------------|------------------|-----------------|-------------|---------------|-----------------------------------|------------------------------------|---------------------------|----------------|-------------------------|--------------|------------------------|
| Client | Geoscience | Victoria | | Density G | radients (psi/foot) | | Conv | ersion Paramet | ers (dynes/cm) |) | |
| Well | Dulungalon | g-2 | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| | | G | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | sure | Oil: Gas: | 0.330 | Laboratory IF I Reservoir Theta | | /2.0 | 24.0 | 48.0 | 72.0 |
| Sample | | | | 045. | 0.100 | Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 478.10 m | | | CO2 Density | 0.107 | Laboratory Tcos | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| Ambient Pern | neability | | | System | Estimated Column Height (feet) | Entry P | ressure (psia) Res Con | Displacement F | Pressure (psia) Resv | Threshold P | ressure (psia) Resv |
| pore radius (µ | im) | 0.190 | | A-Hg | na | 561 | - | 709 | - | 806 | - |
| | | | | G-W | 225 | 110 | 76.5 | 139 | 96.7 | 158 | 110 |
| | | | | 0-W | 361 | 36.7 | 39.8 | 46.4 | 50.3 | 52.7 | 57.1 |
| | | | | 002-11 | 105 | 110 | 59.0 | 157 | 50.5 | 150 | 57.1 |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| Decement | Rav | v Data | Conforma | nce Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (um) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 4 | <i>a</i> · · · 3 | 4 | Q · · · · 3 | 4 | u , | Q-) | <i>u</i> - <i>y</i> | <i>a</i> - 1 | 4-3 | (, | (|
| 1.01 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.41 |
| 1.98 | 6.5 | 6.5 | 0.0 | 0.0 | 107 | 0.20 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 1.3 | 7.9 | 0.0 | 0.0 | 77.7 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.4 | 8.2 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.5 | 8.8 | 0.0 | 0.0 | 56.9 48 4 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.58 | 0.5 | 9.5 10.0 | 0.0 | 0.0 | 40.4 | 0.80 | 0.00 | 0.50 | 0.31 | 2.82 | 2.08 |
| 5.97 | 0.5 | 10.5 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.7 | 11.2 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.6 | 11.8 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.7 | 12.4 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.5 | 13.0 | 0.0 | 0.0 | 18.5 | 2.23 | 1.50 | 1.52 | 0.82 | 7.43 | 4.39 5.41 |
| 15.5 | 0.5 | 14.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.6 | 14.6 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.6 | 15.1 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.6 | 15.8 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.9 | 16.7 | 0.0 | 0.0 | 7.08 | 5.88 7.69 | 4.08 | 5.43 4.49 | 2.12 | 19.3 | 12.0 |
| 49.0 | 0.4 | 17.4 | 0.0 | 0.0 | 4.33 | 9.61 | 6.67 | 5.61 | 3.47 | 31.5 | 19.6 |
| 56.8 | 0.2 | 17.6 | 0.0 | 0.0 | 3.73 | 11.1 | 7.71 | 6.50 | 4.02 | 36.5 | 22.7 |
| 67.3 | 0.3 | 18.0 | 0.0 | 0.0 | 3.15 | 13.2 | 9.17 | 7.70 | 4.77 | 43.4 | 27.0 |
| 79.7 | 0.3 | 18.3 | 0.0 | 0.0 | 2.66 | 15.6 | 10.8 | 9.12 | 5.65 | 51.4 | 31.8 |
| 95.5 | 0.4 | 18.0 | 0.0 | 0.0 | 1.93 | 21.6 | 12.7 | 12.6 | 0.02 7.80 | 70.9 | 37.4 44.1 |
| 130 | 0.4 | 19.4 | 0.0 | 0.0 | 1.64 | 25.5 | 17.7 | 14.9 | 9.22 | 83.8 | 52.1 |
| 154 | 0.5 | 19.9 | 0.0 | 0.0 | 1.37 | 30.2 | 21.0 | 17.6 | 10.9 | 99.1 | 61.8 |
| 180 | 0.5 | 20.4 | 0.0 | 0.0 | 1.18 | 35.3 | 24.5 | 20.6 | 12.8 | 116 | 72.1 |
| 211 | 0.5 | 20.9 | 0.0 | 0.0 | 1.01 | 41.4 | 28.8 | 24.1 | 14.9 | 135 | 84.7 |
| 248 | 0.6 | 21.5 | 0.0 | 0.0 | 0.855 | 48.0 | 33.8 | 28.4 | 20.7 | 180 | 99.4 117 |
| 344 | 1.0 | 23.3 | 1.3 | 2.3 | 0.616 | 67.5 | 46.9 | 39.4 | 24.4 | 222 | 138 |
| 404 | 1.2 | 24.5 | 1.5 | 3.9 | 0.524 | 79.2 | 55.0 | 46.2 | 28.6 | 260 | 162 |
| 474 | 1.7 | 26.2 | 2.1 | 6.0 | 0.447 | 92.9 | 64.5 | 54.2 | 33.6 | 305 | 190 |
| 556 | 2.0 | 28.2 | 2.6 | 8.6 | 0.381 | 109 | /5./ | 63.6 74.3 | 39.4 | 358 | 223 |
| 759 | 3.7 | 34.8 | 4.7 | 17.0 | 0.279 | 149 | 103 | 86.9 | 53.8 | 489 | 303 |
| 889 | 4.4 | 39.2 | 5.6 | 22.6 | 0.238 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 5.9 | 45.1 | 7.5 | 30.1 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1228 | 7.4 | 52.6 | 9.5 | 39.6 | 0.173 | 241 | 167 | 141 | 87.3 | 794 | 491 |
| 1438 | 9.5 | 74 9 | 16.4 | 68.1 | 0.147 | 331 | 230 | 103 | 102 | 1082 | 676 |
| 1828 | 7.7 | 82.6 | 9.8 | 77.8 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 16.4 | 98.9 | 20.8 | 98.7 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2507 | 0.6 | 99.6 | 0.8 | 99.4 | 0.0846 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 3445 | 0.0 | 99.0 99.6 | 0.0 | 99.4 99.4 | 0.0721 | 675 | 469 | 394 | 209 | 2218 | 1379 |
| 4040 | 0.0 | 99.6 | 0.0 | 99.4 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4726 | 0.3 | 99.8 | 0.3 | 99.8 | 0.0449 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5104 | 0.0 | 99.8 | 0.0 | 99.8 | 0.0415 | 1001 | 695 | 584 | 362 | 3291 | 2044 |
| 5994 7022 | 0.0 | 99.8 | 0.0 | 99.8 | 0.0334 | 1175 | 956 | 804 | 425 | 3804 4527 | 2400 |
| 7886 | 0.0 | 99.9 | 0.0 | 99.8 | 0.0269 | 1546 | 1074 | 902 | 558 | 5073 | 3159 |
| 8916 | 0.1 | 100.0 | 0.2 | 100.0 | 0.0238 | 1748 | 1214 | 1020 | 631 | 5736 | 3571 |
| 9648 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 14332 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2409 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18479 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3623 | 2516 | 2115 | 1309 | 11900 | 7400 |
| 20480 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23148 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25005 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4713 | 3695 | 2008 | 1923 | 17482 | 10868 |
| 29377 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31803 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34423 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6750 | 4688 | 3939 | 2438 | 22164 | 13788 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40542 43592 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 8547 | 5935 | 401/ 4989 | 2838 3088 | 23982 | 17456 |
| 47295 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9274 | 6440 | 5413 | 3351 | 30464 | 18941 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55386 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11/41 | 8153 | 0853 | 4242 | 58504 | 25979 |

Well Sample Depth

Dulungalong-2 478 1 m







Well Sample Depth

Flounder-6 1929.38 m



| Client | Geoscience Victoria | | Conversion Parameters | | | | | | |
|-----------------|-----------------------------------|------------------------------|---------------------------|-----------------------|---|------------|------------|--------------|--------------|
| Well | Flounder-6 | | | | | conversio | air/water | air/oil | oil/water |
| | | | | Laboratory Thet | a | | 0.0 | 0.0 | 30.0 |
| Test Method | Air/Mercury Capillary Pressure Dr | ainage | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 |
| | | | | Reservoir Theta | L | | 0.0 | | 30.0 |
| Sample | Flounder-6 | Ambient Perme | ability | Reservoir IFT | Th sta | | 50.0 | 24.0 | 30.0 |
| Deptn | 1929.58 m Ambient Porosity | | | | Laboratory I cos I neta Reservoir Tees Theta | | | 24.0 | 26.0 |
| pore radius (um | 7 | | | Reservoir reost | Density Gradients, psi/ | foot | 50.0 | - | 20.0 |
| 0.063 | Entry Pressure (psia) | Displacement Pressure (psia) | Threshold Pressure (psia) | | | Typical | 1 | | |
| System | Lab Resv | Lab Resv | Lab Resv | Water: | | 0.440 | 1 | | |
| A-Hg | 1703 - | 3833 - | 4223.0 - | Oil: | | 0.330 | | | |
| G-W | 334.1 232.0 | 752.0 522.2 | 828.5 575.3 | Gas: | | 0.100 | | | |
| 0-W | 111.4 120.6 | 250./ 2/1.5 | 276.2 299.2 | | | | | | |
| | | | | | ** ** | | | | |
| Programa | Intrusion | Saturation | Pore | Equivalent A/P Lab | A/P P oc | O/P Lab | O/P Pag | Watar (faat) | Watar (faat) |
| (nsia) | (nercent) | (percent) | (um) | A/B Lab | A/D Kcs | O/B Lab | O/B Res | Oil-Water | Gas-Water |
| (pom) | (percent) | (percent) | (μ) | | | | | on water | Gub Water |
| | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 213 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 0.0 | 0.0 | //./ | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.09 |
| 3 73 | 0.0 | 0.0 | 56.9 | 0.02 | 0.51 | 0.43 | 0.25 | 2.40 | 1.27 |
| 4.38 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 |
| 5.18 | 0.0 | 0.0 | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.07 |
| 5.98 | 0.0 | 0.0 | 35.5 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.0 | 0.0 | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.49 | 2.79 |
| 8.27 | 0.0 | 0.0 | 25.6 | 1.6 | 1.13 | 0.95 | 0.59 | 5.33 6.42 | 3.31 |
| 9.97 | 0.0 | 0.0 | 21.3 | 2.0 | 1.4 | 1.14 | 0.81 | 7.41 | 4,61 |
| 13.5 | 0.0 | 0.0 | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 |
| 15.5 | 0.0 | 0.0 | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 |
| 18.5 | 0.0 | 0.0 | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 |
| 21.6 | 0.0 | 0.0 | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 |
| 25.3 | 0.0 | 0.0 | 8.39 | 5.0 | 3.4 | 2.9 | 1.8 | 16.29 | 10.13 |
| 38.0 | 0.0 | 0.0 | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 25.05 | 12.01 |
| 48.9 | 0.0 | 0.0 | 4.33 | 9.6 | 6.7 | 5.6 | 3.5 | 31.49 | 19.58 |
| 58.2 | 0.0 | 0.0 | 3.64 | 11.4 | 7.9 | 6.7 | 4.1 | 37.48 | 23.31 |
| 69.2 | 0.0 | 0.0 | 3.06 | 14 | 9.4 | 7.9 | 4.9 | 44.57 | 27.71 |
| 80.8 | 0.0 | 0.0 | 2.62 | 16 | 11.0 | 9.2 | 5.7 | 52.04 | 32.36 |
| 91.4 | 0.0 | 0.0 | 2.32 | 18 | 12 | 10.5 | 6.5 | 58.87 | 36.60 |
| 131 | 0.0 | 0.0 | 1.92 | 22 | 13 | 15 | 93 | 84.37 | 52.46 |
| 154 | 0.0 | 0.0 | 1.02 | 30 | 21 | 18 | 10.9 | 99.18 | 61.67 |
| 179 | 0.0 | 0.0 | 1.18 | 35 | 24 | 20 | 13 | 115.28 | 71.69 |
| 211 | 0.0 | 0.0 | 1.00 | 41 | 29 | 24 | 15 | 135.9 | 84.50 |
| 249 | 0.0 | 0.0 | 0.853 | 49 | 34 | 28 | 18 | 160.4 | 99.72 |
| 294 | 0.0 | 0.0 | 0.722 | 58 | 40 | 34 | 21 | 189.3 | 117.74 |
| 345 | 0.0 | 0.0 | 0.614 | 68 79 | 47 | 39 | 24 | 222.2 | 158.2 |
| 403 | 0.0 | 0.0 | 0.525 | 93 | 64 | 54 | 34 | 304.6 | 189.4 |
| 556 | 0.0 | 0.0 | 0.381 | 109 | 76 | 64 | 39 | 358.1 | 222.7 |
| 651 | 0.0 | 0.0 | 0.326 | 128 | 89 | 75 | 46 | 419.3 | 260.7 |
| 757 | 0.0 | 0.0 | 0.280 | 148 | 103 | 87 | 54 | 487.5 | 303.2 |
| 889 | 0.0 | 0.0 | 0.239 | 1/4 | 121 | 102 | 63 | 5/2.6 | 356.0 |
| 1228 | 0.0 | 0.0 | 0.202 | 203 | 167 | 141 | 87 | 790.9 | 491.8 |
| 1439 | 0.0 | 0.0 | 0.147 | 282 | 196 | 165 | 102 | 926.8 | 576.3 |
| 1692 | 0.0 | 0.0 | 0.125 | 332 | 230 | 194 | 120 | 1089.7 | 677.6 |
| 1828 | 1.0 | 0.7 | 0.116 | 358 | 249 | 209 | 130 | 1177 | 732.1 |
| 2143 | 1.7 | 2.4 | 0.098 | 9 420 1 492 | 292 | 245 | 152 | 1580 | 858.2 |
| 2947 | 1.0 | 4.9 | 0.034 | 9 578 | 401 | 337 | 209 | 1898 | 1180 |
| 3449 | 1.1 | 6.0 | 0.061 | 5 676 | 470 | 395 | 244 | 2221 | 1381 |
| 4041 | 1.8 | 7.8 | 0.052 | 5 792 | 550 | 462 | 286 | 2603 | 1618 |
| 4735 | 4.9 | 12.8 | 0.044 | 8 928 | 645 | 542 | 335 | 3050 | 1896 |
| 5112 | 6.U 8 3 | 15.1 | 0.041 | 3 1002 | 696 818 | 585 687 | 362 425 | 3292 | 2047 |
| 7025 | o.5 7.4 | 20.5 | 0.030 | 2 1377 | 957 | 804 | 498 | 4524 | 2813 |
| 7888 | 7.0 | 37.8 | 0.026 | 9 1547 | 1074 | 903 | 559 | 5080 | 3159 |
| 8919 | 8.1 | 45.9 | 0.023 | 8 1749 | 1214 | 1021 | 632 | 5744 | 3572 |
| 9650 | 5.9 | 51.8 | 0.022 | 0 1892 | 1314 | 1104 | 684 | 6215 | 3865 |
| 10451 | 5.7 | 57.5 | 0.020 | 3 2049 | 1423 | 1196 | 740 | 6731 | 4185 |
| 14335 | 9.0 | 73.8 | 0.017 | 5 2409 8 2811 | 1075 | 1406 | 1016 | 0232 | 4920 |
| 16380 | 4.8 | 78.6 | 0.014 | 3 3212 | 2230 | 1875 | 1160 | 10549 | 6560 |
| 18483 | 3.3 | 81.8 | 0.011 | 5 3624 | 2517 | 2115 | 1309 | 11904 | 7402 |
| 20484 | 2.4 | 84.3 | 0.010 | 3 4016 | 2789 | 2344 | 1451 | 13193 | 8204 |
| 23149 | 2.6 | 86.9 | 0.009 | 2 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25066 | 1.5 | 88.4 | 0.008 | 5 4915 | 3413 | 2869 | 1776 | 16144 | 10039 |
| 2/13/ 29378 | 1.5 | 89.9 | 0.007 | 5 5321 5 5760 | 3695 | 3362 | 1923 | 1/4// | 10868 |
| 31805 | 1.3 | 92.5 | 0.007. | 7 6236 | 4331 | 3640 | 2253 | 20484 | 12737 |
| 34424 | 1.2 | 93.7 | 0.006 | 2 6750 | 4687 | 3940 | 2439 | 22171 | 13786 |
| 37194 | 1.1 | 94.8 | 0.005 | 7 7293 | 5065 | 4257 | 2635 | 23955 | 14896 |
| 40342 | 1.1 | 95.8 | 0.005 | 3 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43593 | 0.9 | 96.7 | 0.004 | 9 8548 | 5936 | 4989 | 3088 | 28076 | 17458 |
| 4/294 51170 | 0.9 | 97.7 | 0.004 | 9273 1 10033 | 0440 6968 | 5856 | 3625 | 32956 | 20493 |
| 55385 | 0.8 | 99.3 | 0.004 | 8 10860 | 7542 | 6338 | 3924 | 35670 | 22181 |
| 50970 | 0.7 | 100.0 | 0.002 | 5 11741 | 9152 | (952 | 12.12 | 20565 | 22081 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well Sample | Depth | | F 2 | ortescue 420 m | -2 | | | | | | |
|-------------------------------|------------------|----------------------|------------|------------------------------|----------------------|---------------------------|----------------------|------------------------|-------------------------|-------------------------|-------------------------|
| Client | Geoscience | AVictoria | | Density G | Gradients (psi/foot) | | Con | version Paramet | ers (dynes/cm) | | - 6 0 () |
| Well | Fortescue-2 | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | F2-1 | | Gas: | 0.100 | Reservoir IFT | | 50.0 | | 30.0 | 26.0 | |
| Depth | 2420.00 m | | | CO2 Density | 0.556 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | Estimated Column | Reservoir Tcos Entry F | ressure (psia) | 50.0 Displacement I | Pressure (psia) | 26.0 Threshold P | 26.0 ressure (psia) |
| Pore radius (μm) 0.040 | | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv | |
| | | | | A-Hg G-W | na 1078 | 528 | - 367 | 653 | - 453 | 713 | - 495 |
| | | | | 0-W | 1733 | 176 | 191 | 218 | 236 | 238 | 258 |
| | | | | C0 ₂ -w | 992 | 528 | 191 | 653 | 236 | /13 | 258 |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| Pressure | Raw Intrusion | V Data Saturation | Intrusion | ance Corrected Saturation | Pore Diameter | Air/Brine Lab | Air/Brine Res Con | Lab Conditions | Reservoir Conditions | Free Water Oil-Water | Free Water Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.0 | 0.0 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 3.18 | 0.0 | 0.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.09 |
| 3.73 | 0.0 | 0.0 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 5.18 | 0.0 | 0.0 | 0.0 | 0.0 | 48.4 41.0 | 1.02 | 0.60 | 0.50 | 0.31 | 2.82 | 2.08 |
| 5.98 | 0.0 | 0.0 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 8 27 | 0.0 | 0.0 | 0.0 | 0.0 | 30.4 25.6 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 9.97 | 0.0 | 0.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.0 | 0.0 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.0 | 0.0 | 0.0 | 0.0 | 13.7 | 2.65 | 2.11 | 1.54 | 0.95 | 8.66 | 6.21 |
| 18.5 | 0.0 | 0.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 25.3 | 0.0 | 0.0 | 0.0 | 0.0 | 9.83 8.39 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 16.4 | 8.65 |
| 30.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.1 | 0.1 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 56.6 | 0.4 | 0.5 | 0.0 | 0.0 | 3.75 | 9.25 | 7.71 | 5.40 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 | 0.2 | 0.9 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 93.0 | 0.3 | 1.2 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 10.6 | 5.70 | 51.8 59.6 | 32.4 37.1 |
| 111 | 0.2 | 1.6 | 0.2 | 0.2 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.2 | 1.8 | 0.2 | 0.4 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 10.8 | 83.3 98.2 | 51.8 |
| 179 | 0.2 | 2.0 | 0.2 | 0.8 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 | 0.2 | 2.5 | 0.2 | 1.1 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.2 | 2.7 | 0.2 | 1.5 | 0.880 | 48.4 57.3 | 39.8 | 28.5 33.4 | 20.7 | 139 | 98.8 |
| 343 | 0.3 | 3.2 | 0.3 | 1.8 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 472 | 0.3 | 3.4 3.7 | 0.3 | 2.0 | 0.528 | 78.6 92.5 | 54.6 64.2 | 45.9 54.0 | 28.4 | 258 304 | 161 |
| 553 | 0.3 | 4.0 | 0.3 | 2.7 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 757 | 0.3 | 4.4 | 0.3 | 3.0 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| 887 | 0.4 | 5.2 | 0.5 | 3.9 | 0.239 | 174 | 105 | 102 | 63.1 | 574 | 356 |
| 1048 | 0.5 | 5.7 | 0.5 | 4.4 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1439 | 0.8 | 6.5 7.1 | 0.8 | 5.8 | 0.147 | 241 282 | 196 | 140 | 102 | /88 927 | 576 |
| 1688 | 1.1 | 8.2 | 1.1 | 6.9 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 2142 | 0.7 1.9 | 8.9 10.8 | 0.8 1.9 | 7.6 9.5 | 0.116 0.0990 | 358 420 | 249 292 | 209 245 | 129 152 | 1173 1382 | 732 859 |
| 2510 | 2.9 | 13.7 | 2.9 | 12.4 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 3449 | 3.2 5.7 | 16.8 22.5 | 3.2 | 15.6 21.4 | 0.0720 | 577 676 | 401 469 | 337 395 | 209 245 | 1900 2227 | 1179 1379 |
| 4040 | 6.4 | 28.9 | 6.5 | 27.9 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 12.7 | 41.6 | 12.8 | 40.8 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 6002 | 0./ | 48.3 | 0.8 | 47.6 64.8 | 0.0415 | 11003 | 817 | 585 687 | 425 | 3864 | 2050 |
| 7033 | 19.9 | 85.2 | 20.2 | 85.0 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 7895 8920 | 13.0 | 98.2 100.0 | 13.2 | 98.2 100 0 | 0.0269 | 1548 1749 | 1075 | 904 1021 | 560 632 | 5091 5745 | 3162 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 1406 | 740 870 | 6727 7909 | 4185 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0113 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 27135 | 0.0 | 100.0 100.0 | 0.0 | 100.0 100.0 | 0.0085 | 4915 5321 | 3413 3695 | 2868 3105 | 1775 1922 | 16136 17473 | 10038 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 6749 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2438 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 0.0045 | 8547 9273 | 5935 6440 | 4989 5412 | 3088 3350 | 28073 30455 | 17456 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot
| /ell ample | Depth | | F 2 | ortescue 430 m | -2 | | | | | | |
|----------------|-------------|-----------------|------------|--------------------|----------------------|-----------------|-------------------------|------------------------|-----------------|---------------------|------------------------|
| lient | Geoscience | AVictoria | | Density (| Fradients (nsi/foot) | | Con | version Paramot | ers (dynes/em) |) | |
| /ell | Fortescue-2 | | | Density C | Typical | 1 | 01 | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| est Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| | | | | Gas: | 0.100 | Reservoir Theta | L | 0.0 | | 30.0 | 0.0 |
| mple | F2-2 | | | CO Density | 0.559 | Reservoir IFT | -Th -t- | 50.0 | 24.0 | 30.0 | 26.0 |
| ptn | 2430.00 m | | | CO_2 Density | 0.558 | Laboratory 1 co | 5 i ricia Thata | /2.0 | 24.0 | 42.0 | 12.0 |
| | | | | | Estimated Column | Fntry I | Pressure (psia) | 50.0 Displacement F | Pressure (nsia) | 20.0 Threshold P | 20.0 ressure (psia) |
| re radius (I | um) | 0.067 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv |
| | | | | A-Hg | na | 1585 | - | 2048 | - | 2587 | - |
| | | | | G-W | 635 | 311 | 216 | 402 | 279 | 508 | 352 |
| | | | | O-W | 1021 | 104 | 112 | 134 | 145 | 169 | 183 |
| | | | | CO ₂ -W | 587 | 311 | 112 | 402 | 145 | 508 | 183 |
| | | | | | | Emission | Initation Decomposition | Oil/Drin - | Oil/Daina | II.: ht Abarra | II |
| | Ray | 7 Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| | | | | • · | | | | · · | | | |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 1.8 | 1.8 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.75 | 0.7 | 2.4 | 0.0 | 0.0 | 66 7 | 0.54 | 0.43 | 0.31 | 0.19 | 2.05 | 1.09 |
| 3.73 | 0.4 | 3.2 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.25 | 2.40 | 1.49 |
| 4.38 | 0.2 | 3.4 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.3 | 3.8 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.3 | 4.1 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.3 | 4.4 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.3 | 4.7 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.3 | 5.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.2 | 5.4 5.4 | 0.0 | 0.0 | 18.3 | 2.25 | 1.30 | 1.52 | 0.82 | 1.43 8.66 | 4.39 |
| 15.5 | 0.2 | 5.6 | 0.0 | 0.0 | 13.7 | 2.03 | 2 11 | 1.54 | 1 10 | 10.0 | 6.21 |
| 18.5 | 0.2 | 5.8 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.2 | 6.0 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.1 | 6.1 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.2 | 6.4 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.0 | 6.4 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.1 | 6.5 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 50.0 66 3 | 0.1 | 0.0 | 0.0 | 0.0 | 3.75 | 11.1 | 9.03 | 0.48 | 4.01 | 50.5 47 7 | 22.7 |
| 80.4 | 0.1 | 67 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5 70 | 51.8 | 32.4 |
| 93.0 | 0.1 | 6.8 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.1 | 7.0 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.1 | 7.1 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.2 | 7.3 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 179 | 0.2 | 7.4 | 0.0 | 0.0 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 | 0.2 | 7.0 | 0.0 | 0.0 | 0.860 | 41.2 | 28.0 | 24.0 | 14.9 | 155 | 84.1 98.8 |
| 292 | 0.2 | 81 | 0.0 | 0.0 | 0.300 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 0.3 | 8.3 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 | 0.3 | 8.6 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 0.3 | 8.9 | 0.0 | 0.0 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.3 | 9.2 | 0.0 | 0.0 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 04/ 757 | 0.3 | 9.4 0.0 | 0.0 | 0.0 | 0.328 | 12/ | 88.2 | /4.0 | 45.8 | 416 | 202 |
| 887 | 0.5 | 9.8 10.2 | 0.0 | 0.0 | 0.280 | 148 | 105 | 102 | 55.0 63.1 | 40/ 574 | 305 |
| 1048 | 0.5 | 10.6 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 0.5 | 11.2 | 0.6 | 0.6 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 0.7 | 11.9 | 0.8 | 1.4 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 0.9 | 12.8 | 1.0 | 2.4 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 0.8 | 13.5 | 0.8 | 3.2 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 4.0 | 13.7 | 2.4 4 5 | 5.0 10.1 | 0.0990 | 420 | 342 | 243 | 152 | 1582 | 839 1006 |
| 2945 | 4 9 | 24.6 | 5.5 | 15.6 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3449 | 5.4 | 30.0 | 6.0 | 21.6 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4040 | 5.1 | 35.1 | 5.7 | 27.3 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 7.6 | 42.6 | 8.5 | 35.8 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 3.0 | 45.6 | 3.4 | 39.2 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 6.3 | 51.9 | 7.0 | 46.2 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7895 | 0.6 4.6 | 58.5 63.1 | 1.5 | 53.5 58 7 | 0.0301 | 15/9 | 958 1075 | 805 | 498 | 4527 | 2818 |
| 8920 | 4.0 | 67.9 | 53 | 64 1 | 0.0209 | 1740 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 3.0 | 70.9 | 3.3 | 67.4 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 3.1 | 74.0 | 3.5 | 70.9 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 5.6 | 79.6 | 6.3 | 77.2 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 3.9 | 83.5 | 4.4 | 81.5 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 3.9 | 87.4 | 4.4 | 85.9 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 2.9 | 90.3 | 3.2 | 89.1 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 1.7 | 92.0 | 1.9 | 91.1 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 25149 | 2.2 | 94.2 95.0 | 2.5 | 95.0 94.4 | 0.0092 | 4009 | 3132 | 2049 | 1040 | 14909 | 92/1 |
| 27135 | 12 | 96.2 | 14 | 95.8 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 | 0.6 | 96.9 | 0.7 | 96.5 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.9 | 97.8 | 1.1 | 97.6 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.7 | 98.5 | 0.7 | 98.3 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.7 | 99.2 | 0.8 | 99.1 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.6 | 99.8 | 0.7 | 99.8 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.2 | 99.9 | 0.2 | 99.9 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 1/456 |
| 4/291 51172 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0045 | 92/3 | 044U 6968 | 5856 | 3625 | 20422 | 18941 20404 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 7542 | 6339 | 3023 | 32933 | 20494 |
| 22201 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 22102 |



(B) Capillary Pressure Plot



ACS LABORATORIES

Well Sample Depth

Fortescue-3 2411.50 m



| Client | Geoscience Victoria | | | | | | Conversio | n Parameters | | | | | | | |
|-----------------|-----------------------------------|------------------------------|--------------------|--------------|------------------|-------------------------|--------------|--------------|-------------------|-------------------|--|--|--|--|--|
| Well | Fortescue-3 | | | | | | Conversio | air/water | air/oil | oil/water | | | | | |
| | | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 | | | | | |
| Test Method | Air/Mercury Capillary Pressure Dr | ainage | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 | | | | | |
| | | | | | Reservoir Theta | | | 0.0 | | 30.0 | | | | | |
| Sample | Fortescue-3 | Ambient Permeal | bility | | Reservoir IFT | The star | | 50.0 | 24.0 | 30.0 | | | | | |
| Deptn | 2411.30 III | Ambient Porosity | | | Reservoir TcosT | neta | | 50.0 | 24.0 | 42.0 | | | | | |
| pore radius (um | 2 | | | | D | ensity Gradients, psi/f | oot | 50.0 | | 20.0 | | | | | |
| 0.030 | Entry Pressure (psia) | Displacement Pressure (psia) | Threshold Pressure | e (psia) | | | Typical | 1 | | | | | | | |
| System | Lab Resv | Lab Resv | Lab | Resv | Water: | | 0.440 | T | | | | | | | |
| A-Hg | 3577 - | 4404 - | 5634 | - | Oil: | | 0.330 | | | | | | | | |
| G-W | 701.8 487.4 | 864.0 600.0 | 1105.3 | 767.6 | Gas: | | 0.100 | 1 | | | | | | | |
| 0-11 | 233.7 233.4 | 200.0 512.0 | 508.4 | 339.1 | 1 | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free | | | | | |
| Pressure | Intrusion | Saturation | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) | | | | | |
| (psia) | (percent) | (percent) | | (µm) | | | | | Oil-Water | Gas-Water | | | | | |
| | | | | | | | | | | | | | | | |
| 1.01 | 0.0 | 0.0 | | 210 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 | | | | | |
| 1.99 | 0.0 | 0.0 | | 107 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.07 | | | | | |
| 2.74 | 0.0 | 0.0 | | 77.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | | | | | |
| 3.19 | 0.0 | 0.0 | | 66.5 | 1.37 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 | | | | | |
| 4 38 | 0.0 | 0.0 | | 36.7 48.4 | 1.62 | 1.15 | 0.93 | 0.39 | 6.43 | 5.52 4.00 | | | | | |
| 5.18 | 0.0 | 0.0 | | 40.9 | 2.25 | 1.57 | 1.32 | 0.81 | 7.41 | 4.61 | | | | | |
| 5.98 | 0.0 | 0.0 | | 35.4 | 2.6 | 1.84 | 1.54 | 0.96 | 8.69 | 5.41 | | | | | |
| 6.98 | 0.0 | 0.0 | | 30.4 | 3.0 | 2.11 | 1.77 | 1.10 | 9.98 | 6.21 | | | | | |
| 8.28 | 0.0 | 0.0 | | 25.6 | 3.6 | 2.52 | 2.12 | 1.31 | 11.91 | 7.41 | | | | | |
| 9.98 | 0.0 | 0.0 | | 21.2 | 4.2 | 2.9 | 2.47 | 1.53 | 13.91 | 8.65 | | | | | |
| 13.5 | 0.0 | 0.0 | | 15.7 | 5.9 | 4.1 | 3.4 | 2.13 | 19.32 | 12.01 | | | | | |
| 15.5 | 0.0 | 0.0 | | 13.7 | 7.4 | 5.2 | 4.3 | 2.69 | 24.41 | 15.18 | | | | | |
| 18.5 | 0.0 | 0.0 | | 11.5 | 9.4 | 6.5 | 5.5 | 3.4 | 30.98 | 19.26 | | | | | |
| 21.6 | 0.0 | 0.0 | | 9.83 | 11.1 | 7.7 | 6.5 | 4.0 | 36.45 | 22.67 | | | | | |
| 25.3 | 0.0 | 0.0 | | 8.39 | 13.2 | 9.2 | 7.7 | 4.8 | 43.47 | 27.03 | | | | | |
| 37.9 | 0.0 | 0.0 | | 5.59 | 13.4 | 10.7 | 9.0 | 5.6 | 50.49 | 36.84 | | | | | |
| 48.1 | 0.0 | 0.0 | | 4.41 | 21.6 | 15.0 | 12.6 | 7.8 | 70.84 | 44.05 | | | | | |
| 56.6 | 0.0 | 0.0 | | 3.75 | 25.1 | 17.4 | 14.6 | 9.1 | 82.44 | 51.26 | | | | | |
| 67.5 | 0.0 | 0.0 | | 3.14 | 30 | 20.8 | 17.5 | 10.8 | 98.54 | 61.27 | | | | | |
| 78.4 | 0.0 | 0.0 | | 2.70 | 35 | 24.6 | 20.7 | 12.8 | 116.57 | 72.49 | | | | | |
| 92.0 | 0.0 | 0.0 | | 2.30 | 41 | 29 | 24.0 | 14.9 | 135.25 | 84.10 98.52 | | | | | |
| 128 | 0.0 | 0.0 | | 1.65 | 48 | 39 | 33 | 20.5 | 186.13 | 115.74 | | | | | |
| 153 | 0.0 | 0.0 | | 1.38 | 67 | 47 | 39 | 24.4 | 221.55 | 137.77 | | | | | |
| 181 | 0.0 | 0.0 | | 1.17 | 79 | 55 | 46 | 29 | 260.19 | 161.80 | | | | | |
| 210 | 0.0 | 0.0 | | 1.01 | 93 | 64 | 54 | 33 | 304.0 | 189.03 | | | | | |
| 246 | 0.0 | 0.0 | | 0.862 | 109 | /6 | 64 74 | 39 | 358.1 | 222.67 | | | | | |
| 344 | 0.0 | 0.0 | | 0.617 | 149 | 103 | 87 | 54 | 488.2 | 303.6 | | | | | |
| 404 | 0.0 | 0.0 | | 0.525 | 174 | 121 | 102 | 63 | 571.9 | 355.6 | | | | | |
| 472 | 0.0 | 0.0 | | 0.450 | 205 | 143 | 120 | 74 | 675.0 | 419.7 | | | | | |
| 556 | 0.0 | 0.0 | | 0.381 | 241 | 167 | 141 | 87 | 790.9 | 491.8 | | | | | |
| 64 / 758 | 0.0 | 0.0 | | 0.328 | 282 | 230 | 105 | 102 | 926.8 | 5/6.5 | | | | | |
| 888 | 0.0 | 0.0 | | 0.239 | 358 | 249 | 209 | 120 | 1176.0 | 731.3 | | | | | |
| 1048 | 0.0 | 0.0 | | 0.202 | 420 | 292 | 245 | 152 | 1378.9 | 857.4 | | | | | |
| 1228 | 0.0 | 0.0 | | 0.173 | 492 | 341 | 287 | 178 | 1614.6 | 1004.0 | | | | | |
| 1439 | 0.0 | 0.0 | | 0.147 | 577 | 401 | 337 | 208 | 1895.4 | 1178.6 | | | | | |
| 1826 | 0.0 | 0.0 | | 0.126 | 793 | 469 | 463 | 244 286 | 2220.0 | 1580.5 | | | | | |
| 2141 | 0.0 | 0.0 | | 0.0990 | 928 | 644 | 541 | 335 | 3047 | 1894.7 | | | | | |
| 2507 | 0.0 | 0.0 | | 0.0846 | 1003 | 697 | 586 | 363 | 3296 | 2049.3 | | | | | |
| 2943 | 0.0 | 0.0 | | 0.0720 | 1177 | 818 | 687 | 425 | 3867 | 2405 | | | | | |
| 3447 | 0.0 | 0.0 | | 0.0615 | 1379 | 958 | 805 | 498 | 4530 | 2817 | | | | | |
| 4042 | 1.7 | 7.2 | | 0.0324 | 1348 | 1075 | 1022 | 632 | 5749 | 3575 | | | | | |
| 5117 | 7.0 | 10.7 | | 0.0414 | 1895 | 1316 | 1106 | 685 | 6223 | 3870 | | | | | |
| 6005 | 11.0 | 21.6 | | 0.0353 | 2052 | 1425 | 1198 | 741 | 6739 | 4191 | | | | | |
| 7034 | 14.1 | 35.7 | | 0.0301 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 | | | | | |
| 7897 | 9.2 | 45.0 | | 0.0268 | 2813 | 1953 | 1642 | 1016 | 9239 | 5745 | | | | | |
| 8927 | 7.5 | 52.5 | | 0.0237 | 3214 | 2232 | 2117 | 1310 | 10558 | 6565 7408 | | | | | |
| 10464 | 4.2 | 62.2 | | 0.0203 | 4019 | 2791 | 2345 | 1452 | 13200 | 8208 | | | | | |
| 12296 | 7.5 | 69.7 | | 0.0172 | 4540 | 3153 | 2650 | 1640 | 14913 | 9274 | | | | | |
| 14346 | 4.8 | 74.4 | | 0.0148 | 4916 | 3414 | 2869 | 1776 | 16146 | 10040 | | | | | |
| 16393 | 5.0 | 79.4 | | 0.0129 | 5322 | 3696 | 3106 | 1923 | 17480 | 10870 | | | | | |
| 20495 | 2.8 | 82.2 | | 0.0115 | 6237 | 4001 | 3503 3640 | 2082 | 20485 | 12738 | | | | | |
| 23156 | 2.6 | 87.7 | | 0.0092 | 6750 | 4688 | 3940 | 2439 | 22172 | 13788 | | | | | |
| 25070 | 1.0 | 88.7 | | 0.0085 | 7293 | 5065 | 4257 | 2635 | 23955 | 14896 | | | | | |
| 27141 | 1.3 | 89.9 | | 0.0078 | 7911 | 5494 | 4617 | 2858 | 25984 | 16158 | | | | | |
| 29382 | 1.9 | 91.9 | | 0.0072 | 8548 | 5936 | 4989 | 3089 | 28078 | 17460 | | | | | |
| 34427 | 1.0 | 92.9 | | 0.0067 | 9274 10034 | 6968 | 5857 | 3625 | 32959 | 20495 | | | | | |
| 37194 | 0.6 | 95.2 | | 0.0057 | 10860 | 7541 | 6338 | 3924 | 35670 | 22181 | | | | | |
| 40345 | 0.6 | 95.8 | | 0.0053 | 11740 | 8153 | 6852 | 4242 | 38561 | 23979 | | | | | |
| 43596 | 1.2 | 97.0 | | 0.0049 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | |
| 4/297 | 1.1 | 98.1 | | 0.0045 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | |
| 55384 | 1.2 | 99.5 99.7 | | 0.0041 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | |
| 50974 | 0.2 | 100.0 | | 0.0025 | 0 | õ | 0 | 0 | 0 | ó | | | | | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



Well **Gippsland Frome Lakes-4** Sample Depth 503.5 m Geoscience AVictoria Density Gradients (psi/foot) Client Conversion Parameters (dynes/cm) Well oil/wate CO₂/wate Gippsland Frome Lakes-4 Typical r/wate air/oil Water 0 4 4 0 aboratory Theta 0.0 0.0 30.0 0.0 Air/Mercury Capillary Pressure 0.330 24.0 48.0 72.0 Test Method Oil: aboratory IFT 72.0 0.100 eservoir Theta 0.0 30.0 0.0 GFL4-1 Reservoir IFT 50.0 26.0 30.0 Sample CO2 Density 0.109 aboratory TcosTheta 72.0 24.0 42.0 72.0 Depth 503.50 m ervoir TcosTheta 50.0 26.0 26.0 Estimated Column Entry Pressure (psia) Displacemer ure (psia Threshold ure (psia) Pore radius (um) 0 743 Height (feet) Lab Res Cor Lab Resv Lah Resv A-Hg 143 185 na 166 28.1 9.36 19.5 10.1 32.6 10.9 22.6 25.2 13.1 G-W 57 36.3 o-w 11.8 12.1 92 CO₂-W 26 28.1 10.1 11.8 36.3 13.1 32.6 Equivalent Injection Pressures Oil/Brine Oil/Brine Height Above Height Above Pore Air/Brine Air/Brine Reservoir Free Water Free Water Raw Data Conformance Corrected Lab Conditions Oil-Water Gas-Water Pressure Intrusion Saturation Intrusion Saturation Diameter Lab Res Con Conditions (percent) (percent) (percent) (µm) (psi) (psi) (feet) (feet) (psia) (percent) (psi) (psi) 211 0.20 0.14 0.11 0.07 0.40 0.0 0.0 0.0 0.0 0.64 1.00 0.79 1.09 1.98 0.0 0.0 0.0 0.0 107 0.39 0.27 0.23 0.14 1.28 2.73 0.0 0.0 0.0 0.0 77.6 0.54 0.37 0.31 0.19 1.75 3.18 0.0 0.0 0.0 0.0 667 0.62 0.43 0.36 0.23 2.05 1 27 0.73 1.49 3.73 0.51 0.43 0.0 0.0 0.0 56.9 0.26 2.40 0.0 4.38 5.18 0.0 0.0 48.4 41.0 0.86 1.02 0.60 0.71 0.50 0.59 2.82 3.34 1.76 2.08 0.0 0.0 0.0 0.0 0.31 0.0 0.0 0.37 5.98 0.0 0.0 0.0 0.0 0.0 35.5 1.17 0.81 0.68 0.42 3.85 2 39 6.97 30.4 1.37 0.80 0.49 4.49 0.0 0.0 0.0 0.95 2.80 8.27 0.0 0.0 0.0 0.0 25.6 1.62 1.13 0.95 0.59 5.33 3.32 9.97 21.3 1.95 1.14 0.71 0.0 0.0 0.0 0.0 1.35 6.42 3.97 11.5 13.5 0.0 0.0 0.0 0.0 18 5 2 25 1 56 1 32 0.82 7 4 3 4 59 0.0 0.0 0.0 15.7 2.65 1.84 1.54 0.95 5.41 0.0 8.66 15.5 18.5 0.0 0.0 0.0 0.0 2.11 2.52 1.77 2.12 6.21 7.41 0.0 0.0 137 3.04 1.10 10.0 0.0 0.0 11.5 3.63 11.9 1.31 21.6 25.3 0.0 0.0 0.0 0.0 9.83 4 24 2.94 2.47 1.53 13.9 8.65 0.0 0.0 0.0 4.96 3.44 1.80 10.1 0.0 8.39 2.90 16.4 30.0 0.0 0.0 0.0 0.0 7.08 5.88 4.08 3.43 2.12 19.3 12.0 37.2 0.2 0.2 0.0 5.70 7.29 5.06 4.26 2.64 24.0 14.9 0.0 47.2 56.6 0.4 0.7 0.6 1.3 6.42 7.71 18.9 22.7 0.0 0.0 4 4 9 9 25 5 40 3 34 30.4 0.7 0.7 3.75 11.1 6.48 4.01 36.5 663 1.5 2.8 1.5 2.2 3 20 13.0 9.03 7 59 4.70 42.7 26.6 80.4 4.9 4.4 2.64 11.0 9.20 5.70 51.8 32.4 2.1 2.0 2.1 15.8 93.0 6.9 2.0 6.3 2.28 18.2 12.6 10.6 6.56 59.6 37.1 111 2.9 9.8 9.2 15.1 12.7 71.5 44.4 2.9 1.91 21.8 7.86 129 3.1 12.8 3.1 123 1.65 25.3 17.6 14.8 916 833 51.8 152 4.0 16.9 4.1 1.39 29.8 20.7 17.4 10.8 98.2 60.9 16.4 179 46 21.4 46 21.01 18 35.1 24.4 20.5 12.7 115 71.8 210 6.2 27.6 28.6 24.0 14.9 135 84.1 6.2 27.2 1.01 41.2 247 8.6 36.2 8.7 35.8 0.860 48.4 33.6 28.3 17.5 159 98.8 292 10.6 46.8 10.7 46.5 0.726 57.3 39.8 33.4 20.7 24.3 188 117 343 17.7 64.5 17.8 64.3 0.619 67.3 46.7 39.3 221 137 401 19.3 83.8 19.4 0.528 54.6 45.9 28.4 258 83.7 78.6 161 472 13.7 974 13.7 974 0 4 4 9 92.5 64.2 54.0 33.4 304 189 553 97.5 0.1 75.0 39.2 221 0.1 97.5 0.383 108 63.3 356 647 0.0 97.5 0.0 97.5 0.328 127 88.2 74.0 45.8 416 259 757 97.8 97.8 148 86.6 53.6 487 303 0.3 0.3 0.280 103 887 0.2 98.0 0.2 98.0 0.239 174 121 102 63.1 574 356 1048 0.5 98.5 0.5 98.5 0.202 205 142 120 74.3 675 418 1227 02 98 7 02 98 7 0 1 7 3 241 167 140 867 788 491 1439 0.2 98.9 0.2 98.9 0.147 282 196 165 102 927 576 0.2 1688 99.1 0.2 99.1 0.126 331 230 193 119 1082 676 99.3 99.4 732 859 1828 0.1 0.2 99.3 358 249 209 1173 0.1 0.1 0.116 129 0.0990 152 2142 99.4 420 292 245 1382 2510 0.1 99.6 0.1 99.5 0.0845 492 342 287 178 1618 1006 0.0720 577 337 1179 2945 0.2 99.7 0.2 99.7 401 209 1900 3449 0.1 99.8 0.1 99.8 0.0615 676 469 395 245 2227 1379 4040 0.0 99.8 0.0 99.8 0.0525 792 550 462 286 2600 1618 927 1003 541 585 4728 0.2 100.0 0.2 100.0 0.0448 644 335 3045 1894 5114 0.0 100.0 0.0 100.0 0.0415 697 362 3291 2050 6002 0.0 100.0 0.0 100.0 0.0353 1177 817 687 425 3864 2403 1379 498 4527 7033 0.0 100.0 0.0 100.0 0.0301 958 805 2818 7895 8920 0.0 100.0 0.0 100.0 0.0269 0.0238 1548 1749 1075 1215 904 1021 560 632 5091 5745 3162 3574 0.0 0.0 100.0 100.0 683 740 9649 0.0 100.0 0.0220 1892 1314 1104 6209 3865 0.0 100.0 10452 0.0 100.0 0.0 100.0 0.0203 2049 1423 1196 6727 4185 12283 0.0 100.0 0.0 100.0 0.0173 2408 1672 1406 870 7909 4918 2810 9227 14333 1951 1015 5738 0.0 100.0 0.0 100.0 0.0148 1640 0.0 0.0 16381 100.0 0.0 100.0 0.0129 3212 2231 1875 1161 10555 6562 11900 2517 18481 100.0 0.0 100.0 3624 2115 1309 7403 0.0115 20481 23149 0.0 0.0 100.0 0.0 100.0 100.0 0.0104 0.0092 4016 4539 2789 3152 2344 1451 13191 14909 8203 9271 100.0 0.0 2649 1640 25064 0.0 100.0 0.0 100.0 0.0085 4915 3413 2868 1775 16136 10038 27135 0.0 100.0 0.0 100.0 0.0078 5321 3695 3105 1922 17473 10868 29376 0.0 100.0 0.0 100.0 0.0072 5760 4000 3362 2081 18918 11765 6236 2253 0.0067 4331 20482 12738 31804 0.0 100.0 0.0 100.0 3640 34421 0.0 100.0 0.0 100.0 0.0062 6749 4687 3939 2438 22164 13785 0.0 37192 100.0 0.0 100.0 0.0057 7293 5065 4256 2635 23955 14897 0.0 0.0 7910 8547 40343 100.0 0.0 100.0 0.0053 5493 4617 2858 25982 16156 43591 0.0049 5935 4989 17456 100.0 100.0 28073 0.0 3088 47291 0.0 100.0 0.0 100.0 0.0045 9273 6440 5412 3350 30455 18941

51172

55387 59880

0.0

0.0

0.0

100.0 100.0 100.0 (A) Interpreted Capillary Pressure Chart

100.0

100.0

100.0

0.0

0.0

0.0

0.0041

0.0038

0.0035

10034

10860

11741

6968

7542

8153

3625

3924

4242

5856

6339

6853

32955

35673

38564

20494

22182

23979







(C) Pore Size Distribution plot

| Well Sample | Depth | | C 5 | Sippsland 106.6 m | l Frome Lake | es-4 | | | | | |
|----------------|------------------------------|-----------------|-----------|-------------------------|---------------------|----------------------------------|--------------------------|------------------|----------------|-------------|------------------------|
| Client | Geoscience / | Victoria | | Density (| radients (nsi/foot) | 1 | Con | version Paramete | ers (dynes/cm) | | |
| Well | Geoscience / Gippsland Fi | ome Lakes-4 | | Density C | Typical | | Con | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | GFI 4-2 | | | Gas: | 0.100 | Reservoir Theta Reservoir IFT | | 0.0 50.0 | | 30.0 | 0.0 26.0 |
| Depth | 506.60 m | | | CO ₂ Density | 0.110 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| | | | | | Estimated Column | Entry F | ressure (psia) | Displacement P | ressure (psia) | Threshold P | ressure (psia) |
| Pore radius (µ | .m) | 0.139 | | System A-Hg | Height (feet) | Lab 766 | Res Con | Lab 1120 | Resv | Lab 1228 | Resv |
| | | | | G-W | 307 | 150 | 104 | 220 | 153 | 241 | 167 |
| | | | | O-W | 493 | 50.1 | 54.3 | 73.3 | 79.4 | 80.3 | 87.0 |
| | | | | CO ₂ -W | 141 | 150 | 54.3 | 220 | 79.4 | 241 | 87.0 |
| | | | | | | Eminator | Initiation Decomposition | O:1/D=i== | O:1/D=i== | II | II.i.b. Ab |
| | Raw | Data | Conforma | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.7 | 0.7 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 0.3 | 1.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.1 | 1.1 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 5.73 4 38 | 0.1 | 1.2 | 0.0 | 0.0 | 48.4 | 0.73 | 0.51 | 0.45 | 0.20 | 2.40 | 1.49 |
| 5.18 | 0.1 | 1.6 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.1 | 1.7 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.1 | 1.9 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.1 | 2.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 11.5 | 0.1 | 2.1 | 0.0 | 0.0 | 18.5 | 2.25 | 1.55 | 1.14 | 0.71 | 7.43 | 4.59 |
| 13.5 | 0.2 | 2.4 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.1 | 2.5 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.1 | 2.6 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.1 | 2.7 | 0.0 | 0.0 | 9.85 | 4.24 | 3 44 | 2.47 | 1.55 | 15.9 | 8.65 10.1 |
| 30.0 | 0.1 | 3.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.0 | 3.1 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.1 | 3.2 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 56.6 | 0.1 | 3.2 | 0.1 | 0.1 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 80.4 | 0.2 | 3.5 | 0.2 | 0.4 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 0.2 | 3.7 | 0.2 | 0.5 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.2 | 3.9 | 0.2 | 0.7 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.2 | 4.1 | 0.2 | 0.9 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 132 | 0.2 | 4.5 | 0.2 | 1.2 | 1.59 | 29.8 | 20.7 | 20.5 | 10.8 | 98.2 | 60.9 71.8 |
| 210 | 0.3 | 4.8 | 0.3 | 1.7 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.3 | 5.1 | 0.3 | 2.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 0.3 | 5.4 | 0.3 | 2.3 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 401 | 0.4 | 5.9 | 0.4 | 2.8 | 0.619 | 67.3 78.6 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 472 | 0.7 | 7.1 | 0.7 | 4.1 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.8 | 7.9 | 0.9 | 4.9 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 | 1.1 | 9.1 | 1.2 | 6.1 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| /5/ | 1.6 | 10.6 | 1.6 | 7.7 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 1048 | 3.8 | 16.8 | 3.9 | 14.1 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 5.4 | 22.1 | 5.5 | 19.6 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 9.6 | 31.7 | 9.9 | 29.5 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 12.5 | 44.2 | 12.9 | 42.3 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 6/6 |
| 2142 | 17.3 | 71.3 | 17.9 | 70.4 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 17.7 | 89.0 | 18.3 | 88.6 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | 10.9 | 99.9 | 11.3 | 99.9 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3449 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0615 | 676 702 | 469 | 395 | 245 286 | 2227 | 1379 |
| 4728 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 8920 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14555 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 2231 | 1640 | 1015 | 9227 | 5758 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 2/135 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 5760 | 3095 | 3105 | 1922 2081 | 1/4/3 | 10868 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 804/ 9273 | 5935 6440 | 4989 | 3088 | 28073 | 1/450 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |

Gippsland Frome Lakes-4





(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

Well Sample Depth

Golden Beach West-1 667.68 m



| Client | Geoscience Victoria | | | | | Conversio | n Parameters | | | | | | | | |
|------------------|---|---------------------|-------------------------|------------------|--------------------------|-----------|--------------|-------------------|--------------------|--|--|--|--|--|--|
| Well | Golden Beach West-1 | | | | | | air/water | air/oil | oil/water | | | | | | |
| | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 | | | | | | |
| Test Method | Air/Mercury Capillary Pressure Drainage | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 | | | | | | |
| с I | | | | Reservoir Theta | | | 0.0 | | 30.0 | | | | | | |
| Sample | Golden Beach West-1 | Ambient Permeabil | ity | Laboratory Tcos | Thata | | 50.0 | 24.0 | 30.0 | | | | | | |
| Deptin | 007.00 | Ambient Forosity | | Reservoir TcosT | reta | | 50.0 | 24.0 | 26.0 | | | | | | |
| pore radius (µm) | | | | E | ensity Gradients, psi/fe | oot | | | | | | | | | |
| 0.585 | Entry Pressure (psia) Displacement | Pressure (psia) The | reshold Pressure (psia) | | | Typical | | | | | | | | | |
| System | Lab Resv Lab | Resv | Lab Resv | Water: | | 0.440 | | | | | | | | | |
| A-Hg | 181.9 - 849.1 | - | 1138 - | Oil: | | 0.330 | | | | | | | | | |
| G-W | 35.7 24.8 166.6 | 115.7 | 223.3 155.0 | Gas: | | 0.100 |] | | | | | | | | |
| 0-w | 11.7 12.7 55.5 | 00.2 | /4.4 80.0 | 1 | | | | | | | | | | | |
| | | | Dama | Envirolant | Initation Decouver | | | Haisht Abaus Fasa | Hainht Abassa Fran | | | | | | |
| Proceuro | Intrusion | Saturation | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) | | | | | | |
| (psia) | (percent) | (percent) | (µm) | A D Lao | ADRes | O/D Lab | 0/15 1463 | Oil-Water | Gas-Water | | | | | | |
| 4 | <i>a</i> · · · <i>y</i> | 4 | 4. 7 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| 1.01 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 | | | | | | |
| 1.98 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 | | | | | | |
| 3.18 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.31 | 0.13 | 2.05 | 1.09 | | | | | | |
| 3.73 | 0.0 | 0.0 | 56.8 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 | | | | | | |
| 4.38 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 | | | | | | |
| 5.18 | 0.0 | 0.0 | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.07 | | | | | | |
| 5.98 | 0.0 | 0.0 | 35.5 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | | | | | | |
| 6.97 | 0.0 | 0.0 | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.49 | 2.79 | | | | | | |
| 9.97 | 0.0 | 0.0 | 21.3 | 2.0 | 1.13 | 1 14 | 0.39 | 6.42 | 3.99 | | | | | | |
| 11.5 | 0.0 | 0.0 | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 | | | | | | |
| 13.5 | 0.0 | 0.0 | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 | | | | | | |
| 15.5 | 0.0 | 0.0 | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 | | | | | | |
| 18.5 | 0.0 | 0.0 | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 | | | | | | |
| 21.6 | 0.0 | 0.0 | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 | | | | | | |
| 30.0 | 0.0 | 0.0 | 7.08 | 5.9 | 41 | 3.4 | 2.1 | 19.32 | 12.01 | | | | | | |
| 38.7 | 0.0 | 0.0 | 5.48 | 7.6 | 5.3 | 4.4 | 2.7 | 24.92 | 15.50 | | | | | | |
| 49.8 | 0.0 | 0.0 | 4.26 | 9.8 | 6.8 | 5.7 | 3.5 | 32.07 | 19.94 | | | | | | |
| 56.9 | 0.0 | 0.0 | 3.73 | 11.2 | 7.7 | 6.5 | 4.0 | 36.65 | 22.79 | | | | | | |
| 68.7 | 0.0 | 0.0 | 3.09 | 13 | 9.4 | 7.9 | 4.9 | 44.25 | 27.51 | | | | | | |
| 81.7 | 0.0 | 0.0 | 2.59 | 16 | 11.1 | 9.5 | 5.8 | 52.62 | 32.72 | | | | | | |
| 111 | 0.0 | 0.0 | 1.90 | 22 | 15 | 13 | 7.9 | 71.49 | 44.45 | | | | | | |
| 131 | 0.0 | 0.0 | 1.62 | 26 | 18 | 15 | 9.3 | 84.37 | 52.46 | | | | | | |
| 153 | 0.0 | 0.0 | 1.39 | 30 | 21 | 18 | 10.8 | 98.54 | 61.27 | | | | | | |
| 182 | 0.0 | 0.0 | 1.17 | 36 | 25 | 21 | 13 | 117.22 | 72.89 | | | | | | |
| 213 | 1.0 | 1.0 | 0.994 | 42 | 29 | 24 | 15 | 137.2 | 85.30 | | | | | | |
| 249 | 1.1 | 3.8 | 0.832 | 49 | 54 40 | 28 | 21 | 188.7 | 99.72 | | | | | | |
| 345 | 1.6 | 5.4 | 0.614 | 68 | 40 | 39 | 24 | 222.2 | 138.2 | | | | | | |
| 404 | 2.6 | 8.0 | 0.524 | 79 | 55 | 46 | 29 | 260.2 | 161.8 | | | | | | |
| 474 | 2.3 | 10.3 | 0.448 | 93 | 65 | 54 | 34 | 305.3 | 189.8 | | | | | | |
| 555 | 2.8 | 13.1 | 0.382 | 109 | 76 | 64 | 39 | 357.4 | 222.3 | | | | | | |
| 648 | 3.1 | 10.2 | 0.327 | 127 | 88 | /4 | 40 | 417.3 | 259.5 | | | | | | |
| 890 | 3.7 | 23.0 | 0.238 | 175 | 121 | 102 | 63 | 573.2 | 356.4 | | | | | | |
| 1049 | 4.5 | 27.5 | 0.202 | 206 | 143 | 120 | 74 | 675.6 | 420.1 | | | | | | |
| 1228 | 5.5 | 33.1 | 0.173 | 241 | 167 | 141 | 87 | 790.9 | 491.8 | | | | | | |
| 1437 | 9.2 | 42.3 | 0.148 | 282 | 196 | 164 | 102 | 925.5 | 575.5 | | | | | | |
| 1689 | 17.8 | 60.1 77.1 | 0.126 | 351 | 230 | 200 | 120 | 1087.8 | 732.0 | | | | | | |
| 2144 | 12.9 | 90.0 | 0.0989 | 420 | 292 | 245 | 150 | 1381 | 858.6 | | | | | | |
| 2508 | 5.2 | 95.2 | 0.0845 | 492 | 342 | 287 | 178 | 1615 | 1004.4 | | | | | | |
| 2940 | 2.5 | 97.7 | 0.0721 | 576 | 400 | 336 | 208 | 1893 | 1177 | | | | | | |
| 3449 | 1.3 | 99.0 | 0.0615 | 676 | 470 | 395 | 244 | 2221 | 1381 | | | | | | |
| 4044 | 0.5 | 99.5 | 0.0524 | /93 | 551 | 463 | 286 | 2605 | 1620 | | | | | | |
| 5102 | 0.1 | 100.0 | 0.0415 | 1000 | 695 | 584 | 361 | 3286 | 2043 | | | | | | |
| 5993 | 0.0 | 100.0 | 0.0354 | 1175 | 816 | 686 | 425 | 3860 | 2400 | | | | | | |
| 7020 | 0.0 | 100.0 | 0.0302 | 1376 | 956 | 803 | 497 | 4521 | 2811 | | | | | | |
| 7884 | 0.0 | 100.0 | 0.0269 | 1546 | 1074 | 902 | 559 | 5078 | 3157 | | | | | | |
| 8914 | 0.0 | 100.0 | 0.0238 | 1/48 | 1214 | 1020 | 632 | 5/41 | 35/0 | | | | | | |
| 10448 | 0.0 | 100.0 | 0.0220 | 2049 | 1423 | 1196 | 740 | 6729 | 4184 | | | | | | |
| 12283 | 0.0 | 100.0 | 0.0173 | 2408 | 1673 | 1406 | 870 | 7911 | 4919 | | | | | | |
| 14329 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9228 | 5739 | | | | | | |
| 16379 | 0.0 | 100.0 | 0.0129 | 3212 | 2230 | 1874 | 1160 | 10549 | 6560 | | | | | | |
| 18478 | 0.0 | 100.0 | 0.0115 | 3623 | 2516 | 2115 | 1309 | 11901 | 7400 | | | | | | |
| 20480 | 0.0 | 100.0 | 0.0104 | 4016 | 2/89 | 2344 | 1451 | 13190 | 8202 | | | | | | |
| 25065 | 0.0 | 100.0 | 0.0092 | 4015 | 3413 | 2868 | 1776 | 16143 | 10038 | | | | | | |
| 27136 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17477 | 10868 | | | | | | |
| 29376 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18919 | 11765 | | | | | | |
| 31801 | 0.0 | 100.0 | 0.0067 | 6235 | 4330 | 3639 | 2253 | 20481 | 12736 | | | | | | |
| 34422 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2439 | 22169 | 13786 | | | | | | |
| 5/192 40330 | 0.0 | 100.0 | 0.0057 | 7010 | 5/03 | 4230 | 2033 | 23933 | 14695 | | | | | | |
| 43589 | 0.0 | 100.0 | 0.0033 | 8547 | 5935 | 4988 | 3088 | 28073 | 17457 | | | | | | |
| 47294 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3351 | 30459 | 18941 | | | | | | |
| 51169 | 0.0 | 100.0 | 0.0041 | 10033 | 6967 | 5856 | 3625 | 32955 | 20493 | | | | | | |
| 55385 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35670 | 22181 | | | | | | |



(B) Capillary Pressure Plot





| Well Sample | Depth | | 7 | Goon Nur 26.3 m | e-9 | | | | | | |
|----------------|-------------|-----------------|-----------|-------------------------|---------------------|----------------------------------|---------------------|-----------------|----------------|--------------|------------------------|
| Client | Gaoscianca | Victoria | | Doneity (| radiants (nsi/faat) | <u> </u> | Com | vorsion Paramat | ore (dynos/cm) | | |
| Well | Goon Nure-9 |) | | Density C | Typical | | Con | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | GN9 | | | Gas: | 0.100 | Reservoir Theta Reservoir IFT | l | 0.0 | | 30.0 30.0 | 0.0 26.0 |
| Depth | 726.30 m | | | CO ₂ Density | 0.230 | Laboratory Tco: | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| n 11 (| | | | | Estimated Column | Entry I | Pressure (psia) | Displacement I | ressure (psia) | Threshold Pi | ressure (psia) |
| Pore radius (p | ım) | 0.052 | | A-Hg | Height (feet) | Lab 2057 | Res Con | Lab 2515 | Resv | Lab 2686 | Resv |
| | | | | G-W | 824 | 404 | 280 | 493 | 343 | 527 | 366 |
| | | | | O-W | 1325 | 135 | 146 | 164 | 178 | 176 | 190 |
| | | | | CO ₂ -W | 437 | 404 | 146 | 493 | 178 | 527 | 190 |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| | Raw | Data | Conforma | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 1.3 | 1.3 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 3.18 | 0.3 | 2.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.13 | 2.05 | 1.09 |
| 3.73 | 0.4 | 2.7 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.4 | 3.1 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.4 | 3.5 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.3 | 5.8 4 3 | 0.0 | 0.0 | 55.5 30.4 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 4.49 | 2.39 |
| 8.27 | 0.5 | 4.8 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.5 | 5.3 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.4 | 5.7 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 15.5 | 0.8 | 6.9 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.54 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.5 | 7.4 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.4 | 7.7 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.4 | 8.1 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.4 | 8.6 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.12 | 24.0 | 14.9 |
| 47.2 | 0.1 | 8.6 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 56.6 | 0.1 | 8.7 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 | 0.1 | 8.9 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 93.0 | 0.2 | 9.1 | 0.0 | 0.0 | 2.04 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 32.4 |
| 111 | 0.2 | 9.5 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.2 | 9.7 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.3 | 9.9 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 71.8 |
| 210 | 0.2 | 10.2 | 0.0 | 0.0 | 1.01 | 41.2 | 28.6 | 20.5 | 14.9 | 135 | 84.1 |
| 247 | 0.3 | 10.8 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 0.3 | 11.1 | 0.0 | 0.0 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 0.4 | 11.5 | 0.0 | 0.0 | 0.619 | 67.3 78.6 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 472 | 0.4 | 12.0 | 0.5 | 0.5 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.5 | 12.9 | 0.5 | 1.0 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 | 0.6 | 13.5 | 0.7 | 1.7 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| 887 | 0.8 | 14.5 | 1.0 | 2.6 | 0.280 | 148 | 103 | 102 | 55.0 63.1 | 487 574 | 356 |
| 1048 | 1.2 | 16.3 | 1.4 | 5.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 1.3 | 17.6 | 1.5 | 6.5 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 1.6 | 19.3 | 1.8 | 8.3 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1828 | 1.3 | 21.4 | 1.5 | 12.2 | 0.120 | 358 | 230 | 209 | 129 | 1173 | 732 |
| 2142 | 2.9 | 25.6 | 3.3 | 15.5 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 4.3 | 30.0 | 4.9 | 20.4 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | /.9 | 37.9 49.4 | 9.0 | 29.5 42.6 | 0.0720 | 577 | 401 | 337 | 209 | 2227 | 1179 |
| 4040 | 24.0 | 73.4 | 27.3 | 69.8 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 25.3 | 98.7 | 28.7 | 98.5 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.3 | 99.0 | 0.4 | 98.9 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 7033 | 0.5 | 99.5 | 0.5 | 99.4 | 0.0353 | 11// | 817 | 687 805 | 425 | 3864 | 2403 |
| 7895 | 0.1 | 99.9 | 0.1 | 99.9 | 0.0269 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| 8920 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2408 | 1423 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6749 | 4331 4687 | 3640 3939 | 2253 | 20482 | 12/38 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 4/291 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |









(C) Pore Size Distribution plot

| Well | | | (| Groper-1 | | | | | | |
|----------------|----------------|-----------------|-----------|--------------------|----------------------|-----------------|---------------------|-----------------|-----------------|--------------|
| Sample | Depth | | 9 | 909.15 n | 1 | | | | | |
| Client | Geoscience A | AVictoria | | Density (| Gradients (psi/foot) | | Con | version Paramet | ers (dynes/cm) |) |
| Well | Groper-1 | | | | Typical | | | air/water | air/oil | oil/water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 |
| Test Method | Air/Mercurv | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 |
| | - | | | Gas: | 0.100 | Reservoir Theta | ı | 0.0 | | 30.0 |
| Sample | G1 | | | | | Reservoir IFT | | 50.0 | | 30.0 |
| Depth | Depth 909.15 m | | | | 0.235 | Laboratory Tco: | sTheta | 72.0 | 24.0 | 42.0 |
| | | | | 2 5 | | Reservoir Tcos | Theta | 50.0 | | 26.0 |
| | | | | | Estimated Column | Entry I | Pressure (psia) | Displacement | Pressure (psia) | Threshold |
| Pore radius (1 | um) | 0.045 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab |
| | | | | A-Hg | na | 2352 | - | 2628 | - | 2807 |
| | | | | G-W | 943 | 461 | 320 | 516 | 358 | 551 |
| | | | | O-W | 1515 | 154 | 167 | 172 | 186 | 184 |
| | | | | CO ₂ -W | 503 | 461 | 167 | 516 | 186 | 551 |
| | | | | | | | | | | |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above |
| | Raw | Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) |
| | | | | | | • • | | | <u> </u> | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 |
| 1.98 | 0.7 | 0.7 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 |
| 2.73 | 0.3 | 1.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 |
| 3.18 | 0.1 | 1.1 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 |
| 3.73 | 0.1 | 1.2 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 |
| 4.38 | 0.1 | 1.4 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 |
| 5.18 | 0.1 | 1.5 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 |
| 5.98 | 0.1 | 1.6 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 |
| 6.97 | 0.1 | 1.8 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 |
| 8.27 | 0.1 | 1.9 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 |
| 9.97 | 0.2 | 2.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 |
| 11.5 | 0.1 | 2.2 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 |
| 13.5 | 0.1 | 2.3 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 |
| 15.5 | 0.1 | 2.4 | 0.0 | 0.0 | 12.7 | 2.04 | 2.11 | 1 77 | 1.10 | 10.0 |

11.5

9.83

8.39

7.08

5.70 4.49

3.75 3.20

2.64

2.28

1.91

1.65

1.39

1.18

1.01

0.860

0.726

0.619

0.528

0 4 4 9

0.383

0.328

0.280

0 2 3 9

0.202

0.173

0.147

0.126

0.116 0.0990

0.0845 0.0720

0.0615 0.0525

0.0448

0.0415

0.0353

0.0301

0.0269

0.0238

0.0203 0.0173

0.0148

0.0129

0.0115

0.0104

0.0092

0.0085

0.0078

0.0072

0.0067

0.0062

0.0057

0.0053 0.0049

0.0045

0.0041

0.0038

0.0035

3.63

4.24

4.96 5.88

7.29 9.25

11.1 13.0

15.8 18.2

21.8

25.3

29.8

35.1

41.2

48.4 57.3

67.3 78.6

92.5

108

127

148

174

205

241

282 331

358 420

492 577

676 792

927

1003

1177

1379

1548

1749

1892

2049

2408

2810

3212

3624

4016

4539

4915

5321

5760

6236

6749

7293

7910 8547

9273

10034

10860

11741

2.52

2.94

3 44

4.08

5.06 6.42

7.71

9.03

11.0 12.6

15.1

17.6

20.7

24.4

28.6

33.6

39.8

46.7 54.6

64.2

75.0

88.2

103

121

142

167 196 230

249 292

342 401

469 550

644 697

817

958

1075

1215

1314

1423

1672

1951

2231

2517

2789

3152

3413

3695

4000

4331

4687

5065

5493 5935

6440

6968

7542

8153

2.12

2.47

2.90

3.43

4.26 5.40

6.48 7.59

9.20

10.6

127

14.8

174

20.5

24.0

28.3 33.4

39.3 45.9

54.0

63.3

74.0

86.6

102

120

140

165

193

209 245

287 337

395 462

541 585

687

805

904

1021

1104

1196

1406

1640

1875

2115 2344

2649 2868

3105

3362

3640

3939 4256

4617 4989

5412 5856

6339

6853



CO₂/water

0.0 72.0

0.0

26.0

72.0

26.0

e (psia)

382

199

Height Above

Free Water

Gas-Water (feet)

0.40

0.79

1.09

1.27

1.49

1.76 2.08

2.39 2.80

3.32

3.97 4.59

5.41 6.21 7.41

8.65 10.1

12.0

14.9 18.9

22.7 26.6

32.4 37.1

44.4 51.8

60.9 71.8 84.1

98.8 117

137

161

189

221

259

303

356

418

491

576

676

732 859

1006 1179

1379

1618

1894

2050

2403

2818

3162

3574

3865

4185

4918

5738

6562

7403

8203

9271

10038

10868

11765

12738

13785 14897

16156 17456

18941

20494

22182

23979

Resv

10.0

11.9

13.9

16.4

19.3

24.0

30.4

36.5 42.7

51.8

59.6

71.5

83.3

98.2 115 135

159 188

221 258

304

356

416

487

574

675

788

927

1082

1173 1382

1618 1900

2227

2600

3045

3291

3864

4527

5091

5745

6209

6727

7909

9227

10555

11900

13191

14909

16136

17473

18918

20482

22164

23955

25982

28073

30455 32955

35673

38564

1.31

1.53

1.80

2.12

2.64 3.34

4.01 4.70

5.70

6.56

7 86

9.16

10.8 12.7

14.9

17.5

20.7

24.3 28.4

33.4

39.2

45.8

53.6

63.1 74.3

86.7

102

119

129 152

178 209

245

286

335

362

425

498

560

632

683

740

870

1015

1161

1309

1451

1640

1775

1922

2081 2253

2438

2635

2858

3088

3350

3625

3924

4242

100.0 100.0 (A) Interpreted Capillary Pressure Chart

18.5

21.6

25.3

30.0

37.2 47.2

56.6 66.3

80.4 93.0

111

129

152 179 210

247 292

343 401

472

553

647

757

887

1048

1227

1439

1688

1828 2142

2510 2945

3449

4040

4728

5114

6002

7033

7895

8920

9649

10452 12283

14333

16381

18481

20481

23149

25064

27135

29376

31804

34421 37192

40343 43591

47291 51172

55387 59880

0.1

0.1

0.1

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0.2

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0.3

03

0.4

0.4

0.5

0.7

0.4

1.1

2.2 7.9

26.1 24.1

17.5

4.1

6.6

2.2 0.2

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2.6 2.7 2.8 2.9 3.0 3.0

3.1 3.2

3.2 3.3 3.4 3.5

3.6 3.7 3.8 3.9 4.1

4.2 4.3 4.5 4.7 5.0

5.0 5.2 5.5 5.9

6.3 6.9 7.5 8.0 9.1

11.3 19.2

45.3

69.3

86.9

91.0

97.6

99.8

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1.1

2.3 8.3

273

25.2

18.3 4.3

6.9 2.3 0.2

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0.0 0.0

0.2 0.4

0.6

0.9

1.2 1.6

2.1 2.6 3.3

3.8 4.9

7.2 15.5

42.8

68.0

863

90.6

97.5

99.8

100.0

100.0 100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0

100.0 100.0

100.0

100.0

100.0

100.0

100.0

100.0







ACS LABORATORIES PTY. LTD.

| Well | |
|--------------|---|
| Sample Depth | ı |

Groper-1 926.1 m



| Client | Geoscience Victo | oria | | | | | | | Conversi | on Parameters | | | | | | | | |
|-----------------|-------------------|------------------------|------------------|-------------------------|------------------|------------|------------------|-----------------------------------|----------------------|---------------|-------------------|-------------------|--|--|--|--|--|--|
| Well | Groper-1 | | | | | | | | | air/water | air/oil | oil/water | | | | | | |
| Test Mathad | Air/Mercury Con | illary Proceura Dr. | ainage | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 48.0 | | | | | | |
| i est methou | . in microury Cap | mary i ressure Die | | | | | Reservoir Theta | | | 0.0 | 24.0 | 30.0 | | | | | | |
| Sample | Groper-1 | | | Ambient Perme | ability | | Reservoir IFT | | | 50.0 | 1 | 30.0 | | | | | | |
| Depth | 926.10 | m | | Ambient Porosit | ty | | Laboratory TcosT | Theta | | 72.0 | 24.0 | 42.0 | | | | | | |
| pore radius (um |) | | | | | | Reservoir TcosTi | neta Density Gradients, psi/fa | oot | 50.0 | | 20.0 | | | | | | |
| 0.425 | Entry Pressure (p | sia) | Displacement Pre | essure (psia) | Threshold Pressu | ire (psia) | | , in an interest part | Typical | 1 | | | | | | | | |
| System | Lab | Resv | Lab | Resv | Lab | Resv | Water: | | 0.440 | | | | | | | | | |
| A-Hg C-W | 250.4 | - 34.1 | 293.5 | - 40.0 | 347.9 | - 47.4 | Oil: Gas: | | 0.330 | | | | | | | | | |
| o-w | 16.4 | 17.7 | 19.2 | 20.8 | 22.8 | 24.6 | 043. | | 0.100 | 4 | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free | | | | | | |
| Pressure | | Intrusion (percent) | | Saturation (paraant) | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) | | | | | | |
| (psia) | | (percent) | | (percent) | | (µIII) | | | | | Oil-Water | Gas-water | | | | | | |
| | | | | | | | | | | 0.05 | 0.65 | 0.40 | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 210 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 | | | | | | |
| 2.74 | | 0.0 | | 0.0 | | 77.5 | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.10 | | | | | | |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 | | | | | | |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 | | | | | | |
| 4.38 | | 0.0 | | 0.0 | | 48.4 | 1.02 | 0.80 | 0.59 | 0.31 | 3.34 | 2.07 | | | | | | |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | | | | | | |
| 6.98 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 | | | | | | |
| 8.28 | | 0.0 | | 0.0 | | 25.6 | 1.6 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 | | | | | | |
| 11.5 | | 0.0 | | 0.0 | | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 | | | | | | |
| 13.5 | | 0.0 | | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 | | | | | | |
| 15.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 | | | | | | |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 5.6 4.2 | 2.3 | 2.1 | 1.5 | 13.91 | 8.65 | | | | | | |
| 25.3 | | 0.0 | | 0.0 | | 8.39 | 5.0 | 3.4 | 2.9 | 1.8 | 16.29 | 10.13 | | | | | | |
| 30.0 | | 0.0 | | 0.0 | | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 | | | | | | |
| 37.7 | | 0.0 | | 0.0 | | 5.63 | 7.4 | 5.1 | 4.3 | 2.7 | 24.28 | 15.10 | | | | | | |
| 56.3 | | 0.0 | | 0.0 | | 3.76 | 11.0 | 7.7 | 6.4 | 4.0 | 36.26 | 22.55 | | | | | | |
| 67.2 | | 0.0 | | 0.0 | | 3.15 | 13 | 9.2 | 7.7 | 4.8 | 43.28 | 26.91 | | | | | | |
| 78.2 | | 0.0 | | 0.0 | | 2.71 | 15 | 10.6 | 8.9 | 5.5 | 50.36 | 31.32 | | | | | | |
| 110 | | 0.0 | | 0.0 | | 1.94 | 22 | 12 | 10.5 | 7.8 | 70.84 | 44.05 | | | | | | |
| 128 | | 0.0 | | 0.0 | | 1.66 | 25 | 17 | 15 | 9.1 | 82.44 | 51.26 | | | | | | |
| 153 | | 0.0 | | 0.0 | | 1.39 | 30 | 21 | 18 | 10.8 | 98.54 | 61.27 | | | | | | |
| 210 | | 0.0 | | 0.0 | | 1.18 | 35 41 | 25 | 21 | 15 | 115.93 | 72.09 | | | | | | |
| 246 | | 0.0 | | 0.0 | | 0.863 | 48 | 33 | 28 | 17 | 158.4 | 98.52 | | | | | | |
| 289 | | 1.2 | | 1.2 | | 0.733 | 57 | 39 | 33 | 20 | 186.1 | 115.74 | | | | | | |
| 343 | | 1.8 | | 3.0 | | 0.617 | 67 79 | 47 | 39 | 24 | 220.9 | 137.4 | | | | | | |
| 405 | | 3.2 | | 8.6 | | 0.450 | 92 | 64 | 54 | 33 | 303.3 | 188.6 | | | | | | |
| 555 | | 3.9 | | 12.5 | | 0.382 | 109 | 76 | 64 | 39 | 357.4 | 222.3 | | | | | | |
| 646 | | 4.0 | | 16.5 | | 0.328 | 127 | 88 | 74 | 46 | 416.1 | 258.7 | | | | | | |
| 887 | | 3.0 | | 22.7 | | 0.230 | 148 | 121 | 102 | 63 | 571.3 | 355.2 | | | | | | |
| 1047 | | 3.0 | | 25.7 | | 0.203 | 205 | 143 | 120 | 74 | 674.3 | 419.3 | | | | | | |
| 1227 | | 2.9 | | 28.6 | | 0.173 | 241 | 167 | 140 | 87 | 790.2 | 491.4 | | | | | | |
| 1686 | | 3.2 | | 34.7 | | 0.147 | 331 | 230 | 193 | 119 | 1085.9 | 675.2 | | | | | | |
| 1825 | | 2.8 | | 36.3 | | 0.116 | 358 | 249 | 209 | 129 | 1175 | 730.9 | | | | | | |
| 2140 | | 3.6 | | 39.9 | | 0.0991 | 420 | 291 | 245 | 152 | 1378 | 857.0 | | | | | | |
| 2941 | | 4.4 | | 48.2 | | 0.0340 | 577 | 400 | 337 | 208 | 1894 | 1178 | | | | | | |
| 3445 | | 4.7 | | 52.9 | | 0.0615 | 675 | 469 | 394 | 244 | 2219 | 1380 | | | | | | |
| 4040 | | 5.2 | | 58.1 | | 0.0525 | 792 | 550 | 462 | 286 | 2602 | 1618 | | | | | | |
| 5115 | | 4.8 | | 67.1 | | 0.0448 | 1003 | 696 | 585 | 362 | 3294 | 2048 | | | | | | |
| 6002 | | 4.5 | | 71.5 | | 0.0353 | 1177 | 817 | 687 | 425 | 3866 | 2404 | | | | | | |
| 7032 | | 3.9 | | 75.4 | | 0.0301 | 1379 | 958 | 805 | 498 | 4529 | 2816 | | | | | | |
| 7895 | | 2.6 | | /8.0 | | 0.0269 | 1548 | 10/5 | 904 | 559 | 5085 | 3162 | | | | | | |
| 9661 | | 1.9 | | 82.4 | | 0.0219 | 1894 | 1315 | 1106 | 684 | 6222 | 3869 | | | | | | |
| 10463 | | 1.6 | | 83.9 | | 0.0203 | 2052 | 1425 | 1197 | 741 | 6739 | 4190 | | | | | | |
| 12295 | | 2.9 | | 86.8 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 | | | | | | |
| 16392 | | 2.0 | | 91.0 | | 0.0148 | 3214 | 2232 | 1876 | 1161 | 10557 | 6565 | | | | | | |
| 18495 | | 1.3 | | 92.3 | | 0.0115 | 3626 | 2518 | 2117 | 1310 | 11912 | 7407 | | | | | | |
| 20493 | | 1.3 | | 93.6 | | 0.0103 | 4018 | 2790 | 2345 | 1452 | 13198 | 8207 | | | | | | |
| 23154 | | 1.2 | | 94.8 | | 0.0092 | 4540 | 3153 | 2650 | 1640 | 14912 | 9273 | | | | | | |
| 27139 | | 0.6 | | 95.9 | | 0.0078 | 5321 | 3695 | 3106 | 1923 | 17479 | 10869 | | | | | | |
| 29380 | | 0.8 | | 96.7 | | 0.0072 | 5761 | 4001 | 3362 | 2081 | 18922 | 11766 | | | | | | |
| 31806 | | 0.5 | | 97.2 | | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20484 | 12738 | | | | | | |
| 34426 | | 0.7 | | 97.9 | | 0.0062 | 7293 | 4088 | 3940 4256 | 2439 | 22172 | 13/8/ 14895 | | | | | | |
| 40344 | | 0.4 | | 98.5 | | 0.0053 | 7911 | 5493 | 4617 | 2858 | 25983 | 16157 | | | | | | |
| 43594 | | 0.5 | | 99.0 | | 0.0049 | 8548 | 5936 | 4989 | 3088 | 28076 | 17459 | | | | | | |
| 4/295 | | 0.4 | | 99.4 99.7 | | 0.0045 | 9274 10034 | 0440 6968 | 541 <i>3</i> 5856 | 3351 | 30460 | 18941 | | | | | | |
| 55383 | | 0.1 | | 99.9 | | 0.0038 | 10859 | 7541 | 6338 | 3924 | 35669 | 22180 | | | | | | |
| 59872 | | 0.1 | | 100.0 | | 0.0035 | 11740 | 8153 | 6852 | 4242 | 38560 | 23978 | | | | | | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



| Well | |
|--------------|--|
| Sample Depth | |

Groper-1 932.00 m



| Client | Geoscience Victoria | | | 1 | | Conversio | on Parameters | | | | | | | | |
|-----------------|-----------------------------------|------------------------------|------------------|-----------|--------------------|---------------------------------------|---------------|-----------|--------------------|-------------------|--|--|--|--|--|
| Well | Groper-1 | | | | | | Conversio | air/water | air/oil | oil/water | | | | | |
| | | | | | Laboratory Theta | ı | | 0.0 | 0.0 | 30.0 | | | | | |
| Test Method | Air/Mercury Capillary Pressure Dr | rainage | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 | | | | | |
| | | | | | Reservoir Theta | | | 0.0 | | 30.0 | | | | | |
| Sample | Groper-1 A | Ambient Perme | ability | | Reservoir IFT | T1 (| | 50.0 | 24.0 | 30.0 | | | | | |
| Deptn | 932.00 m | Ambient Porosi | ty | | Laboratory I cos I | I neta | | 72.0 | 24.0 | 42.0 | | | | | |
| pore radius (un | 0 | | | | Reservoir reos ri | Density Gradients, psi/f | òot | 50.0 | | 20.0 | | | | | |
| 0.680 | Entry Pressure (psia) | Displacement Pressure (psia) | Threshold Pressu | re (psia) | | · · · · · · · · · · · · · · · · · · · | Typical | | | | | | | | |
| System | Lab Resv | Lab Resv | Lab | Resv | Water: | [| 0.440 | | | | | | | | |
| A-Hg | 156.5 - | 151.3 - | 285.0 | - | Oil: | | 0.330 | | | | | | | | |
| G-W | 30.7 21.3 | 29.7 20.6 | 55.9 | 38.8 | Gas: | | 0.100 | 1 | | | | | | | |
| 0-w | 10.2 11.1 | 9.9 10.7 | 18.0 | 20.2 | 1 | | | | | | | | | | |
| | | | | Dama | Emission | Inite time Deservation | | | Haisht Abassa Fara | Hainht Abaus Ener | | | | | |
| Proseturo | Intrusion | Saturation | | Diameter | A/B Lab | A/B Ree | O/B Lab | O/B Res | Water (feet) | Water (feet) | | | | | |
| (nsia) | (percent) | (nercent) | | (um) | A/D Lab | A D KC3 | O/D Lab | 0/10 1403 | Oil-Water | Gas-Water | | | | | |
| (1.0.11) | () | (F1111) | | 4- / | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| 1.01 | 0.0 | 0.0 | | 210 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 | | | | | |
| 1.99 | 0.0 | 0.0 | | 10/ | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.80 | | | | | |
| 3 19 | 0.0 | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.10 | | | | | |
| 3.74 | 0.0 | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 | | | | | |
| 4.38 | 0.0 | 0.0 | | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 | | | | | |
| 5.18 | 0.0 | 0.0 | | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.07 | | | | | |
| 5.98 | 0.0 | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | | | | | |
| 6.98 | 0.0 | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 | | | | | |
| 9.98 | 0.0 | 0.0 | | 21.2 | 2.0 | 1.15 | 1.14 | 0.71 | 6.43 | 4.00 | | | | | |
| 11.5 | 0.0 | 0.0 | | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 | | | | | |
| 13.5 | 0.0 | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 | | | | | |
| 15.5 | 0.0 | 0.0 | | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 | | | | | |
| 18.5 | 0.0 | 0.0 | | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 | | | | | |
| 21.0 | 0.0 | 0.0 | | 9.85 | 4.2 | 2.9 | 2.3 | 1.5 | 15.91 | 8.05 | | | | | |
| 30.0 | 0.0 | 0.0 | | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 | | | | | |
| 40.1 | 0.0 | 0.0 | | 5.29 | 7.9 | 5.5 | 4.6 | 2.8 | 25.83 | 16.06 | | | | | |
| 49.6 | 0.0 | 0.0 | | 4.27 | 9.7 | 6.8 | 5.7 | 3.5 | 31.94 | 19.86 | | | | | |
| 58.2 | 0.0 | 0.0 | | 3.64 | 11.4 | 7.9 | 6.7 | 4.1 | 37.48 | 23.31 | | | | | |
| 68.4 81.4 | 0.0 | 0.0 | | 3.10 | 13 | 9.5 | /.8 | 4.8 | 44.05 | 27.39 | | | | | |
| 94.3 | 0.0 | 0.0 | | 2.25 | 18 | 13 | 10.8 | 6.7 | 60.73 | 37.77 | | | | | |
| 112 | 0.0 | 0.0 | | 1.90 | 22 | 15 | 13 | 7.9 | 72.13 | 44.85 | | | | | |
| 130 | 0.0 | 0.0 | | 1.63 | 25 | 18 | 15 | 9.2 | 83.73 | 52.06 | | | | | |
| 154 | 0.0 | 0.0 | | 1.38 | 30 | 21 | 18 | 10.9 | 99.18 | 61.67 | | | | | |
| 182 | 1.4 | 1.4 | | 1.17 | 36 | 25 | 21 | 13 | 117.22 | 72.89 | | | | | |
| 213 | 2.2 | 5.4 | | 0.855 | 42 | 34 | 24 | 18 | 159.7 | 99.32 | | | | | |
| 292 | 2.4 | 7.8 | | 0.725 | 57 | 40 | 33 | 21 | 188.1 | 116.94 | | | | | |
| 344 | 2.0 | 9.8 | | 0.616 | 67 | 47 | 39 | 24 | 221.6 | 137.8 | | | | | |
| 403 | 1.7 | 11.5 | | 0.526 | 79 | 55 | 46 | 29 | 259.5 | 161.4 | | | | | |
| 4/3 | 1.5 | 13.0 | | 0.448 | 93 | 64 76 | 54 | 34 | 304.6 | 189.4 | | | | | |
| 648 | 1.4 | 14.4 | | 0.382 | 109 | 76 88 | 74 | 39 46 | 417.3 | 222.5 | | | | | |
| 759 | 1.3 | 17.0 | | 0.279 | 149 | 103 | 87 | 54 | 488.8 | 304.0 | | | | | |
| 888 | 1.3 | 18.3 | | 0.239 | 174 | 121 | 102 | 63 | 571.9 | 355.6 | | | | | |
| 1048 | 1.3 | 19.6 | | 0.202 | 205 | 143 | 120 | 74 | 675.0 | 419.7 | | | | | |
| 1230 | 1.3 | 20.8 | | 0.172 | 241 | 167 | 141 | 8/ | 792.2 | 492.6 | | | | | |
| 1437 | 1.2 | 22.1 | | 0.148 | 331 | 230 | 193 | 102 | 925.5 | 676.4 | | | | | |
| 1829 | 1.1 | 23.9 | | 0.116 | 359 | 249 | 209 | 130 | 1178 | 732.5 | | | | | |
| 2143 | 1.3 | 25.2 | | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 | | | | | |
| 2510 | 1.3 | 26.6 | | 0.0845 | 492 | 342 | 287 | 178 | 1617 | 1005.2 | | | | | |
| 2944 | 1.4 | 28.0 | | 0.0720 | 577 | 401 | 337 | 209 | 2221 | 1381 | | | | | |
| 4043 | 1.4 | 31.0 | | 0.0524 | 793 | 551 | 463 | 244 | 2604 | 1619 | | | | | |
| 4732 | 2.3 | 33.4 | | 0.0448 | 928 | 644 | 542 | 335 | 3048 | 1895 | | | | | |
| 5116 | 1.8 | 34.3 | | 0.0414 | 1003 | 697 | 585 | 362 | 3295 | 2049 | | | | | |
| 6004 | 2.0 | 36.4 | | 0.0353 | 1177 | 818 | 687 | 425 | 3867 | 2405 | | | | | |
| 7032 | 2.4 | 38.7 | | 0.0301 | 13/9 | 958 | 805 | 498 | 4529 | 2816 | | | | | |
| 8926 | 3.2 | 40.9 | | 0.0208 | 1750 | 1215 | 1022 | 632 | 5749 | 3575 | | | | | |
| 9663 | 2.9 | 47.1 | | 0.0219 | 1895 | 1316 | 1106 | 685 | 6223 | 3870 | | | | | |
| 10465 | 3.7 | 50.8 | | 0.0203 | 2052 | 1425 | 1198 | 741 | 6740 | 4191 | | | | | |
| 12296 | 9.9 | 60.6 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 | | | | | |
| 1434/ | 10.2 | 70.9 | | 0.0148 | 2813 | 1954 | 1642 | 1016 | 9240 | 5/46 | | | | | |
| 18496 | 5.8 | 84.6 | | 0.0129 | 3627 | 2519 | 2117 | 1310 | 11912 | 7407 | | | | | |
| 20495 | 4.6 | 89.2 | | 0.0103 | 4019 | 2791 | 2345 | 1452 | 13200 | 8208 | | | | | |
| 23155 | 4.3 | 93.5 | | 0.0092 | 4540 | 3153 | 2650 | 1640 | 14913 | 9273 | | | | | |
| 25069 | 2.4 | 95.9 | | 0.0085 | 4915 | 3414 | 2869 | 1776 | 16146 | 10040 | | | | | |
| 27139 | 2.0 | 97.9 | | 0.0078 | 5321 | 3695 | 5106 | 1923 | 1/479 | 10869 | | | | | |
| 31807 | 1.2 | 99.1 99.7 | | 0.0072 | 6237 | 4331 | 3640 | 2253 | 20485 | 12738 | | | | | |
| 34425 | 0.3 | 99.9 | | 0.0062 | 6750 | 4688 | 3940 | 2439 | 22171 | 13787 | | | | | |
| 37194 | 0.1 | 100.0 | | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14896 | | | | | |
| 40342 | 0.0 | 100.0 | | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 | | | | | |
| 43593 | 0.0 | 100.0 | | 0.0049 | 8548 | 5936 | 4989 | 3088 | 28076 | 17458 | | | | | |
| 51166 | 0.0 | 100.0 | | 0.0045 | 10033 | 6967 | 5856 | 3625 | 32953 | 20491 | | | | | |
| 55381 | 0.0 | 100.0 | | 0.0038 | 10859 | 7541 | 6338 | 3923 | 35668 | 22179 | | | | | |
| 59876 | 0.0 | 100.0 | | 0.0035 | 11740 | 8153 | 6852 | 4242 | 38563 | 23980 | | | | | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well | | |
|--------|-------|--|
| Sample | Depth | |

Groper-2 747.86 m



| Client | Geoscience Vic | toria | | | | | | Conversion Parameters | | | | | | |
|---------------------|----------------|----------------------|-----------------|------------------|------------------|-----------|--------------------|--------------------------|---------|-----------|-------------------|-------------------|--|--|
| Well | Groper_? | | | | | | | | | air/water | air/oil | oil/water | | |
| | 5.0pm - | | | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 | | |
| Test Method | Air/Mercury Cs | millary Pressure Dr | ainana | | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 | | |
| i cat intenioù | in mereary ee | ipinary riessare isi | uniuge | | | | Reservoir Theta | | | 0.0 | 21.0 | 30.0 | | |
| Sample | Groper-2 | | | Ambiant Barmas | hilite | | Reservoir IFT | | | 50.0 | | 30.0 | | |
| Donth | 747.86 | | | Ambient Permea | binty | | Laboratory Taoal | Thata | | 72.0 | 24.0 | 42.0 | | |
| Deptii | /4/.00 | | | Ambient i orosit | y | | Databolatory TCOST | neta | | 72.0 | 24.0 | 42.0 | | |
| a sea and is a form | 7 | | | | | | Reservoir TCOSTI | ieta | 4 | 30.0 | | 20.0 | | |
| pore radius (µm | | (| In: 1 (n | 6.15 | 71 1 115 | | L | ensity Gradients, psi/io | | + | | | | |
| 2.330 | Entry Pressure | (psia) | Displacement Pl | essure (psia) | Threshold Pressu | re (psia) | W7 / | ŀ | Typical | ł | | | | |
| System | Lab 41.7 | Resv | Lab 54.7 | Resv | 151 | Resv | water. | | 0.440 | | | | | |
| A-lig C W | 41.7 | 5.7 | 10.7 | 7.6 | 20.6 | 20.6 | C | | 0.550 | | | | | |
| 0-W | 0.2 | 3.7 | 2.6 | 2.0 | 29.0 | 20.0 | Gas. | | 0.100 | 1 | | | | |
| 0-11 | 2.7 | 5.0 | 5.0 | 3.9 | 7.7 | 10.7 | 1 | | | | | | | |
| | | | | | | | | | | | | | | |
| | | | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free | | |
| Pressure | | Intrusion | | Saturation | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) | | |
| (psia) | | (percent) | | (percent) | | (µm) | | | | | Oil-Water | Gas-Water | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 209 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 | | |
| 1.99 | | 0.0 | | 0.0 | | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.80 | | |
| 2.74 | | 0.0 | | 0.0 | | 77.4 | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.10 | | |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 | | |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 | | |
| 4.39 | | 0.0 | | 0.0 | | 48.3 | 0.86 | 0.60 | 0.50 | 0.31 | 2.83 | 1.76 | | |
| 5.19 | | 0.0 | | 0.0 | | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 | | |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.08 | 0.42 | 5.85 | 2.39 | | |
| 0.98 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.60 | 0.49 | 4.50 | 2.80 | | |
| 0.28 | | 0.0 | | 0.0 | | 23.0 | 1.0 | 1.15 | 0.95 | 0.59 | 5.55 | 3.32 | | |
| 9.98 | | 0.0 | | 0.0 | | 21.2 | 2.0 | 1.4 | 1.14 | 0.71 | 7.41 | 4.00 | | |
| 11.5 | | 0.0 | | 0.0 | | 16.5 | 2.5 | 1.0 | 1.3 | 0.06 | 2.41 | +.01 | | |
| 15.5 | | 0.0 | | 0.0 | | 13./ | 2.0 | 1.0 | 1.5 | 1.10 | 0.09 | 6.21 | | |
| 13.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 1.0 | 1.10 | 9.98 | 0.21 | | |
| 18.3 | | 0.0 | | 0.0 | | 11.5 | 3.0 | 2.3 | 2.1 | 1.5 | 12.01 | 2.41 | | |
| 21.0 | | 0.0 | | 0.0 | | 9.03 | 4.2 | 2.9 | 2.5 | 1.5 | 16.20 | 10.12 | | |
| 30.0 | | 0.0 | | 0.0 | | 7.08 | 5.0 | 4.1 | 3.4 | 2.1 | 10.29 | 12.01 | | |
| 30.5 | | 0.0 | | 0.0 | | 5 37 | 77 | 5.4 | 4.5 | 2.1 | 25.44 | 15.82 | | |
| 49.5 | | 0.3 | | 0.0 | | 4 29 | 97 | 67 | 57 | 3.5 | 31.88 | 19.82 | | |
| 59.4 | | 1.2 | | 2.2 | | 3.57 | 11.6 | 81 | 6.8 | 4.2 | 38.26 | 23.79 | | |
| 69.2 | | 2.5 | | 47 | | 3.07 | 14 | 9.4 | 79 | 4.9 | 44 57 | 27.71 | | |
| 80.8 | | 3.4 | | 8.1 | | 2.62 | 16 | 11.0 | 9.2 | 5.7 | 52.04 | 32.36 | | |
| 94.7 | | 3.0 | | 11.1 | | 2.24 | 19 | 13 | 10.8 | 6.7 | 60.99 | 37.93 | | |
| 113 | | 4.0 | | 15.1 | | 1.87 | 22 | 15 | 13 | 8.0 | 72.78 | 45.26 | | |
| 132 | | 3.5 | | 18.6 | | 1.61 | 26 | 18 | 15 | 9.4 | 85.01 | 52.86 | | |
| 156 | | 3.7 | | 22.3 | | 1.36 | 31 | 21 | 18 | 11.1 | 100.47 | 62.48 | | |
| 183 | | 3.4 | | 25.7 | | 1.16 | 36 | 25 | 21 | 13 | 117.86 | 73.29 | | |
| 212 | | 2.9 | | 28.6 | | 0.999 | 42 | 29 | 24 | 15 | 136.5 | 84.90 | | |
| 246 | | 2.6 | | 31.2 | | 0.861 | 48 | 33 | 28 | 17 | 158.4 | 98.52 | | |
| 293 | | 2.8 | | 34.0 | | 0.723 | 57 | 40 | 34 | 21 | 188.7 | 117.34 | | |
| 345 | | 2.3 | | 36.3 | | 0.615 | 68 | 4/ | 39 | 24 | 222.2 | 138.2 | | |
| 403 | | 1.8 | | 38.1 | | 0.527 | /9 | 55 | 46 | 29 | 259.5 | 161.4 | | |
| 473 | | 2.1 | | 40.2 | | 0.448 | 100 | 76 | 54 | 34 | 259 1 | 222.7 | | |
| 649 | | 1.8 | | 43.0 | | 0.327 | 107 | 88 | 74 | 16 | 418.0 | 250.0 | | |
| 758 | | 1.8 | | 45.7 | | 0.280 | 149 | 103 | 87 | 54 | 488.2 | 303.6 | | |
| 888 | | 1.8 | | 47.5 | | 0.239 | 174 | 121 | 102 | 63 | 571.9 | 355.6 | | |
| 1048 | | 1.8 | | 49.3 | | 0.202 | 205 | 143 | 120 | 74 | 675.0 | 419.7 | | |
| 1228 | | 1.7 | | 51.0 | | 0.173 | 241 | 167 | 141 | 87 | 790.9 | 491.8 | | |
| 1437 | | 1.7 | | 52.7 | | 0.148 | 282 | 196 | 164 | 102 | 925.5 | 575.5 | | |
| 1688 | | 1.9 | | 54.6 | | 0.126 | 331 | 230 | 193 | 120 | 1087.1 | 676.0 | | |
| 1827 | | 1.5 | | 55.5 | | 0.116 | 358 | 249 | 209 | 129 | 1177 | 731.7 | | |
| 2143 | | 1.8 | | 57.4 | | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 | | |
| 2508 | | 1.9 | | 59.2 | | 0.0845 | 492 | 342 | 287 | 178 | 1615 | 1004.4 | | |
| 2943 | | 2.0 | | 61.2 | | 0.0720 | 5// | 401 | 33/ | 208 | 1895 | 11/9 | | |
| 5449 4042 | | 1.9 | | 63.1 | | 0.0015 | 702 | 4/0 | 393 | 244 | 2221 | 1561 | | |
| 4045 | | 2.8 | | 67.7 | | 0.0524 | 928 | 645 | 542 | 200 | 3049 | 1896 | | |
| 5117 | | 1.8 | | 68.7 | | 0.0414 | 1003 | 697 | 586 | 363 | 3296 | 2049 | | |
| 6002 | | 1.7 | | 70.4 | | 0.0353 | 1177 | 817 | 687 | 425 | 3866 | 2404 | | |
| 7032 | | 2.5 | | 72.9 | | 0.0301 | 1379 | 958 | 805 | 498 | 4529 | 2816 | | |
| 7896 | | 2.3 | | 75.2 | | 0.0268 | 1548 | 1075 | 904 | 559 | 5085 | 3162 | | |
| 8927 | | 2.4 | | 77.6 | | 0.0237 | 1750 | 1216 | 1022 | 632 | 5749 | 3575 | | |
| 9662 | | 1.5 | | 79.2 | | 0.0219 | 1895 | 1316 | 1106 | 685 | 6223 | 3870 | | |
| 10465 | | 1.8 | | 80.9 | | 0.0203 | 2052 | 1425 | 1198 | 741 | 6740 | 4191 | | |
| 12296 | | 3.3 | | 84.2 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 | | |
| 14346 | | 2.5 | | 86.7 | | 0.0148 | 2813 | 1953 | 1642 | 1016 | 9239 | 5745 | | |
| 16396 | | 1.8 | | 88.5 | | 0.0129 | 3215 | 2233 | 1876 | 1162 | 10560 | 6566 | | |
| 18495 | | 1.2 | | 89.7 | | 0.0115 | 3626 | 2518 | 2117 | 1310 | 11912 | 7407 | | |
| 20497 | | 1.7 | | 91.4 | | 0.0103 | 4019 | 2791 | 2346 | 1452 | 13201 | 8209 | | |
| 23154 | | 0.8 | | 92.2 | | 0.0092 | 4540 | 3153 | 2650 | 1640 | 14912 | 9273 | | |
| 25069 | | 1.0 | | 93.2 | | 0.0085 | 4915 | 3414 | 2869 | 1776 | 16146 | 10040 | | |
| 27137 | | 1.0 | | 94.2 | | 0.0078 | 5321 | 3695 | 3106 | 1923 | 17477 | 10868 | | |
| 29382 | | 1.0 | | 95.3 | | 0.0072 | 5761 | 4001 | 3363 | 2082 | 18923 | 11767 | | |
| 31806 | | 0.7 | | 96.0 | | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20484 | 12/38 | | |
| 34427 | | 1.1 | | 97.1 | | 0.0062 | 0/50 | 4088 | 3940 | 2439 | 22172 | 13/88 | | |
| 3/195 | | 0.4 | | 97.4 | | 0.0057 | /293 | 5065 | 4257 | 2635 | 23955 | 14896 | | |
| 40346 | | 1.0 | | 98.5 | | 0.0053 | /911 | 5026 | 401/ | 2838 | 23985 | 10138 | | |
| 43393 | | 0.7 | | 99.1 | | 0.0049 | 9274 | 6440 | 4789 | 3351 | 20077 | 1/439 | | |
| 51173 | | 0.3 | | 99.8 | | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32958 | 20494 | | |
| 55384 | | 0.2 | | 99.9 | | 0.0038 | 10860 | 7541 | 6338 | 3924 | 35670 | 22181 | | |
| 59893 | | 0.1 | | 100.0 | | 0.0035 | 11744 | 8155 | 6854 | 4243 | 38574 | 23986 | | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

WellHSample Depth3



Hunters Lane-1 377.00 m

| Well | Hunters Lane-1 | na | | | | | | | Conversion | air/water | air/oil | oil/water |
|--------------------|--------------------|------------------------|----------------|-------------------------|-------------|--------------------------|-----------------------|--------------------------------|--------------|--------------|--|--|
| Test Method | Air/Mercury Con | llary Procence De | inana | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 |
| r cor method | An / wiercury Capi | y r ressure Dra | | | | | Reservoir Theta | | | 0.0 | 24.0 | 48.0 |
| Sample Depth | Hunters Lane -1 | m | | Ambient Permea | bility | | Reservoir IFT | heta | | 50.0 | 24.0 | 30.0 |
| hun | 5,1,00 | | | oren rorosit | , | | Reservoir TcosTh | eta | | 50.0 | 24.0 | 26.0 |
| pore radius (µm) | Entry Process | sia) | Displacement P | ssure (poin) | Threehold D | e (nsia) | D | ensity Gradients, psi/f | Tunia-1 | | | |
| 2.000 System | Lab | Resv | Lab | Resv | Lab | Resv | Water: | ŀ | 0.440 | | | |
| A-Hg G-W | 58.2 | - 7 2 | 142.6 | - 17 9 | 182.1 | 22.7 | Oil: Gas: | | 0.330 | | | |
| 0-W | 3.5 | 3.8 | 8.5 | 9.2 | 10.9 | 11.8 | Gdð. | | 0.100 | l | | |
| | | | | | | | | | | | | |
| Pressure (psia) | | Intrusion (percent) | | Saturation (percent) | | Pore Diameter (µm) | Equivalent A/B Lab | Injection Pressures A/B Res | O/B Lab | O/B Res | Height Above Free Water (feet) Oil-Water | Height Above Free Water (feet) Gas-Water |
| | | | | | | | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 209 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 |
| 1.99 | | 0.0 | | 0.0 | | 107 77 4 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.80 |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 |
| 4.39 | | 0.0 | | 0.0 | | 48.5 40.9 | 1.02 | 0.71 | 0.50 | 0.31 | 2.83 | 2.08 |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.98 8.28 | | 0.0 | | 0.0 | | 30.4 25.6 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 5.33 | 2.80 |
| 9.98 | | 0.0 | | 0.0 | | 21.2 | 2.0 | 1.13 | 1.14 | 0.71 | 6.43 | 4.00 |
| 11.5 | | 0.0 | | 0.0 | | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 |
| 13.5 | | 0.0 | | 0.0 | | 15.7 13.7 | 2.6 3.0 | 1.8 2.1 | 1.5 1.8 | 0.96 1.10 | 8.69 9.98 | 5.41 6.21 |
| 18.5 | | 0.0 | | 0.0 | | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 |
| 25.3 30.0 | | 0.0 | | 0.0 | | 8.39 | 5.0 | 5.4 4.1 | 2.9 3.4 | 2.1 | 19.32 | 12.01 |
| 39.7 | | 0.0 | | 0.0 | | 5.34 | 7.8 | 5.4 | 4.5 | 2.8 | 25.57 | 15.90 |
| 49.7 59.6 | | 0.0 | | 0.0 | | 4.27 | 9.7 11.7 | 6.8 8.1 | 5.7 6.8 | 3.5 4.2 | 32.01 38.38 | 19.90 23.87 |
| 69.5 | | 1.2 | | 1.9 | | 3.05 | 14 | 9.5 | 8.0 | 4.9 | 44.76 | 27.83 |
| 81.2 | | 1.5 | | 3.4 | | 2.61 | 16 | 11.1 | 9.3 | 5.8 | 52.30 | 32.52 |
| 95.0 | | 2.0 | | 4.8 | | 2.23 | 22 | 15 | 13 | 8.1 | 73.42 | 45.66 |
| 132 | | 1.8 | | 8.6 | | 1.60 | 26 | 18 | 15 | 9.4 | 85.01 | 52.86 |
| 156 | | 2.3 | | 11.0 | | 1.35 | 31 | 21 | 18 | 11.1 | 100.47 | 62.48 73.29 |
| 213 | | 3.3 | | 17.0 | | 0.997 | 42 | 29 | 24 | 15 | 137.2 | 85.30 |
| 247 | | 4.3 | | 21.4 | | 0.860 | 48 | 34 | 28 | 17 | 159.1 | 98.92 |
| 294 345 | | 6.2 | | 33.7 | | 0.722 | 58 68 | 40 47 | 34 39 | 21 | 222.2 | 117.74 138.2 |
| 403 | | 5.3 | | 39.0 | | 0.527 | 79 | 55 | 46 | 29 | 259.5 | 161.4 |
| 473 | | 6.9 7 2 | | 46.0 53.1 | | 0.449 | 93 109 | 64 76 | 54 64 | 34 39 | 304.6 357.4 | 189.4 |
| 648 | | 6.9 | | 60.1 | | 0.327 | 127 | 88 | 74 | 46 | 417.3 | 259.5 |
| 757 | | 7.5 | | 67.6 | | 0.280 | 148 | 103 | 87 | 54 | 487.5 | 303.2 |
| 887 | | 7.6 7.6 | | /5.2 82.8 | | 0.239 | 205 | 121 143 | 102 | 63 74 | 571.3 | 355.2 419.3 |
| 1227 | | 6.7 | | 89.5 | | 0.173 | 241 | 167 | 140 | 87 | 790.2 | 491.4 |
| 1435 | | 6.0 | | 95.5 | | 0.148 | 281 | 195 | 164 | 102 | 924.2 | 574.7 675.2 |
| 1825 | | 1.6 | | 99.1 | | 0.120 | 358 | 249 | 209 | 129 | 1175 | 730.9 |
| 2141 | | 0.4 | | 99.5 | | 0.0990 | 420 | 292 | 245 | 152 | 1379 | 857.4 |
| 2506 | | 0.3 | | 99.7 100.0 | | 0.0846 | 491 577 | 400 | 28/ 337 | 208 | 1894 | 1178 |
| 3447 | | 0.0 | | 100.0 | | 0.0615 | 676 | 469 | 394 | 244 | 2220 | 1380 |
| 4041 4732 | | 0.0 | | 100.0 | | 0.0525 | 792 928 | 550 644 | 462 542 | 286 | 2603 3048 | 1618 1895 |
| 5115 | | 0.0 | | 100.0 | | 0.0414 | 1003 | 696 | 585 | 362 | 3294 | 2048 |
| 6000 | | 0.0 | | 100.0 | | 0.0353 | 1176 | 817 | 687 805 | 425 | 3864 | 2403 |
| 7895 | | 0.0 | | 100.0 | | 0.0302 | 1579 | 1075 | 904 | 559 | 4328 | 3162 |
| 8926 | | 0.0 | | 100.0 | | 0.0238 | 1750 | 1215 | 1022 | 632 | 5749 | 3575 |
| 9661 10463 | | 0.0 | | 100.0 | | 0.0219 | 1894 2052 | 1315 | 1106 | 684 741 | 6222 | 3869 4190 |
| 12295 | | 0.0 | | 100.0 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 |
| 14345 | | 0.0 | | 100.0 | | 0.0148 | 2813 | 1953 | 1642 | 1016 | 9239 | 5745 |
| 18494 | | 0.0 | | 100.0 | | 0.0129 | 3626 | 2518 | 2116 | 1310 | 11911 | 7407 |
| 20496 | | 0.0 | | 100.0 | | 0.0103 | 4019 | 2791 | 2346 | 1452 | 13200 | 8208 |
| 23153 25068 | | 0.0 | | 100.0 | | 0.0092 | 4540 4915 | 3153 3413 | 2650 2869 | 1640 1776 | 14912 | 9272 10039 |
| 27136 | | 0.0 | | 100.0 | | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17477 | 10868 |
| 29381 | | 0.0 | | 100.0 | | 0.0072 | 5761 | 4001 | 3362 | 2081 | 18923 | 11767 |
| 31805 | | 0.0 | | 100.0 | | 0.0067 | 6750 | 4551 4688 | 3940 | 2439 | 20484 22172 | 12/3/ 13787 |
| 37195 | | 0.0 | | 100.0 | | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14896 |
| 40346 | | 0.0 | | 100.0 | | 0.0053 | 7911 | 5494 5936 | 4617 4989 | 2858 | 25985 | 16158 |
| 47295 | | 0.0 | | 100.0 | | 0.0049 | 9274 | 6440 | 5413 | 3351 | 30460 | 18941 |
| 51172 | | 0.0 | | 100.0 | | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32957 | 20494 |
| 55384 59893 | | 0.0 | | 100.0 | | 0.0038 | 10860 | /541 8155 | 6338 6854 | 3924 4243 | 356/0 38574 | 22181 23986 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well | |
|--------|-------|
| Sample | Depth |

Kingfish-3 2143.05 m



| Client | Geoscience Victo | ria | | | | | | | Conversio | on Parameters | | |
|------------------|--------------------|------------------|------------------|-----------------|------------------|-----------|------------------|---------------------------------|--------------|---------------|-------------------|-------------------|
| Well | Kingfish-3 | | | | | | | | | air/water | air/oil | oil/water |
| T | Air/Marrie C | llan Dra | ainaga | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 |
| i est Method | An/mercury Capi | naty riessure Dr | amage | | | | Reservoir Theta | | | 0.0 | 24.0 | 48.0 |
| Sample | Kingfish-3 | | | Ambient Perme | ability | | Reservoir IFT | | | 50.0 | | 30.0 |
| Depth | 2143.05 | m | | Ambient Porosit | y . | | Laboratory TcosT | Theta | | 72.0 | 24.0 | 42.0 |
| nore radius (um) | 7 | | | | | | Reservoir TcosTh | ieta Iensity Gradiante pri/f | not | 50.0 | 1 | 26.0 |
| 0.063 | Entry Pressure (ps | sia) | Displacement Pro | essure (psia) | Threshold Pressu | re (psia) | | cusity Gradients, psi/i | Typical | 4 | | |
| System | Lab | Resv | Lab | Resv | Lab | Resv | Water: | | 0.440 | 1 | | |
| A-Hg | 1703 | - | 2866 | - 200 5 | 3730 | - | Oil: | | 0.330 | | | |
| O-W | 111.4 | 120.6 | 187.4 | 203.0 | 243.9 | 264.3 | Gas. | | 0.100 | 4 | | |
| | | | | | | | • | | | | | |
| | | | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free |
| Pressure | | Intrusion | | Saturation | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) |
| (psia) | | (percent) | | (percent) | | (µ11) | | | | | Oil-water | Gas-water |
| | | | | | | | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 209 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 |
| 2.74 | | 0.0 | | 0.0 | | 77.4 | 0.54 | 0.37 | 0.31 | 0.19 | 1.26 | 1.10 |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 |
| 5.19 | | 0.0 | | 0.0 | | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.98 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 |
| 9.98 | | 0.0 | | 0.0 | | 23.6 | 2.0 | 1.13 | 1.14 | 0.39 | 6.43 | 4.00 |
| 11.5 | | 0.0 | | 0.0 | | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 |
| 13.5 | | 0.0 | | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 |
| 15.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 2.1 | 1.10 | 9.98 | 6.21 7.41 |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 |
| 25.3 | | 0.0 | | 0.0 | | 8.39 | 5.0 | 3.4 | 2.9 | 1.8 | 16.29 | 10.13 |
| 30.0 | | 0.0 | | 0.0 | | 7.08 | 5.9 | 4.1 | 3.4 4.3 | 2.1 | 24.41 | 12.01 |
| 46.6 | | 0.0 | | 0.0 | | 4.55 | 9.1 | 6.3 | 5.3 | 3.3 | 30.01 | 18.66 |
| 57.6 | | 0.0 | | 0.0 | | 3.68 | 11.3 | 7.8 | 6.6 | 4.1 | 37.10 | 23.07 |
| 67.2 | | 0.0 | | 0.0 | | 3.15 | 13 | 9.2 | 7.7 | 4.8 | 43.28 | 26.91 |
| 92.2 | | 0.0 | | 0.0 | | 2.30 | 18 | 13 | 10.6 | 6.5 | 59.38 | 36.92 |
| 110 | | 0.0 | | 0.0 | | 1.93 | 22 | 15 | 13 | 7.8 | 70.84 | 44.05 |
| 128 | | 0.0 | | 0.0 | | 1.65 | 25 | 21 | 15 | 9.1 | 82.44 | 51.26 |
| 178 | | 0.0 | | 0.0 | | 1.19 | 35 | 24 | 20 | 13 | 114.64 | 71.29 |
| 210 | | 0.0 | | 0.0 | | 1.01 | 41 | 29 | 24 | 15 | 135.2 | 84.10 |
| 246 | | 0.0 | | 0.0 | | 0.861 | 48 | 33 | 28 | 17 | 158.4 | 98.52 116.14 |
| 343 | | 0.0 | | 0.0 | | 0.617 | 67 | 47 | 39 | 24 | 220.9 | 137.4 |
| 401 | | 0.0 | | 0.0 | | 0.529 | 79 | 55 | 46 | 28 | 258.3 | 160.6 |
| 472 | | 0.0 | | 0.0 | | 0.449 | 93 109 | 64 75 | 54 | 33 | 304.0 356.8 | 189.0 |
| 648 | | 0.0 | | 0.0 | | 0.327 | 127 | 88 | 74 | 46 | 417.3 | 259.5 |
| 757 | | 0.0 | | 0.0 | | 0.280 | 148 | 103 | 87 | 54 | 487.5 | 303.2 |
| 887 1048 | | 0.0 | | 0.0 | | 0.239 | 205 | 121 | 102 | 63 74 | 571.5 | 355.2 419.7 |
| 1227 | | 0.0 | | 0.0 | | 0.173 | 241 | 167 | 140 | 87 | 790.2 | 491.4 |
| 1438 | | 0.0 | | 0.0 | | 0.147 | 282 | 196 | 165 | 102 | 926.1 | 575.9 |
| 1828 | | 0.0 | | 0.0 | | 0.126 | 358 | 230 | 209 | 120 | 1177 | 732.1 |
| 2143 | | 1.6 | | 1.6 | | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 |
| 2509 | | 2.2 | | 3.7 | | 0.0845 | 492 | 342 | 287 | 178 | 1616 | 1004.8 |
| 3448 | | 3.6 | | 10.4 | | 0.0615 | 676 | 469 | 395 | 209 | 2221 | 1381 |
| 4043 | | 6.6 | | 16.9 | | 0.0524 | 793 | 551 | 463 | 286 | 2604 | 1619 |
| 4731 | | 8.0 | | 24.9 | | 0.0448 | 928 | 644 | 541 | 335 | 3047 | 1895 |
| 6004 | | 9.7 | | 41.8 | | 0.0353 | 1177 | 818 | 687 | 425 | 3867 | 2405 |
| 7032 | | 11.0 | | 52.9 | | 0.0301 | 1379 | 958 | 805 | 498 | 4529 | 2816 |
| 7897 | | 6.0 | | 58.9 | | 0.0268 | 1548 | 1075 | 904 | 559 | 5086 | 3163 |
| 9662 | | 3.6 | | 69.0 | | 0.0237 | 1895 | 1316 | 11022 | 685 | 6223 | 3870 |
| 10464 | | 3.6 | | 72.6 | | 0.0203 | 2052 | 1425 | 1198 | 741 | 6739 | 4191 |
| 12296 | | 5.8 | | 78.5 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 |
| 16397 | | 3.2 | | 86.6 | | 0.0148 | 3215 | 2233 | 1876 | 1162 | 10560 | 6567 |
| 18494 | | 3.1 | | 89.7 | | 0.0115 | 3626 | 2518 | 2116 | 1310 | 11911 | 7407 |
| 20497 | | 2.6 | | 92.3 | | 0.0103 | 4019 | 2791 | 2346 | 1452 | 13201 | 8209 |
| 23152 | | 1.4 | | 93.8 95.1 | | 0.0092 | 4540 | 3153 | 2650 | 1640 | 14911 | 9272 |
| 27136 | | 1.0 | | 96.2 | | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17477 | 10868 |
| 29380 | | 0.8 | | 96.9 | | 0.0072 | 5761 | 4001 | 3362 | 2081 | 18922 | 11766 |
| 31806 | | 0.8 | | 97.8 98.2 | | 0.0067 | 6751 | 4331 4688 | 3640 3940 | 2253 2439 | 20484 22174 | 12/38 13788 |
| 37197 | | 0.4 | | 98.6 | | 0.0057 | 7294 | 5065 | 4257 | 2635 | 23956 | 14897 |
| 40347 | | 0.4 | | 99.0 | | 0.0053 | 7911 | 5494 | 4617 | 2858 | 25985 | 16158 |
| 43595 47293 | | 0.3 | | 99.5 99.6 | | 0.0049 | 6548 9273 | 5936 6440 | 4989 | 3350 | 26077 | 17459 |
| 51174 | | 0.3 | | 99.9 | | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32958 | 20495 |
| 55386 | | 0.0 | | 99.9 | | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35671 | 22181 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



| Well Sample | Depth | | N 7 | /errlieu-/ 22.00 m | 4 1 | | | | | | |
|----------------|------------------------|-------------------------|------------------------|-------------------------|----------------------|----------------------------------|---------------------|-----------------|---------------------|----------------|------------------------|
| Client | Geoscience . | AVictoria | | Density C | Gradients (psi/foot) | | Con | version Paramet | ers (dynes/cm) |) | |
| Well | Meerlieu-4 | | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| Test Method | Air/Mercury | Canillary Press | ire | Water: Oil: | 0.440 | Laboratory The Laboratory IFT | a | 0.0 72.0 | 0.0 24.0 | 30.0 48.0 | 0.0 |
| rest witchiou | 7 til/ Wiereury | Capital y 1 10350 | iii c | Gas: | 0.100 | Reservoir Theta | | 0.0 | 24.0 | 30.0 | 0.0 |
| Sample | M4-1 | | | CO Density | 0.102 | Reservoir IFT | T1 (| 50.0 | 24.0 | 30.0 | 26.0 |
| Depth | 722.00 m | | | CO ₂ Density | 0.183 | Laboratory Tcos | s I heta Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | Estimated Column | Entry I | Pressure (psia) | Displacement I | Pressure (psia) | Threshold P | ressure (psia) |
| Pore radius (µ | ım) | 0.058 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv |
| | | | | G-W | 731 | 358 | 249 | 392 | 272 | 418 | 290 |
| | | | | O-W | 1176 | 119 | 129 | 131 | 141 | 139 | 151 |
| | | | | CO ₂ -W | 365 | 358 | 129 | 392 | 141 | 418 | 151 |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| | Rav | v Data | Conforma | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion (percent) | Saturation (paraant) | Intrusion (norcont) | Saturation | Diameter | Lab | Res Con | Conditions | Conditions (noi) | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (ieei) | (leet) |
| | | | | | | | | | 0.05 | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2.73 | 0.0 | 0.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.0 | 0.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.0 | 0.0 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.58 | 0.0 | 0.0 | 0.0 | 0.0 | 40.4 | 1.02 | 0.00 | 0.50 | 0.31 | 2.82 | 2.08 |
| 5.98 | 0.0 | 0.0 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.0 | 0.0 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.0 | 0.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 6.42 | 3.32 3.97 |
| 11.5 | 0.0 | 0.0 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.0 | 0.0 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.0 | 0.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 21.6 | 0.0 | 0.0 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.0 | 0.0 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 47.2 | 0.2 | 0.2 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 4.20 5.40 | 3.34 | 30.4 | 14.9 |
| 56.6 | 0.3 | 0.8 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 | 0.4 | 1.2 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 93.0 | 0.5 | 1.6 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 111 | 0.5 | 2.5 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.5 | 3.0 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.5 | 3.4 | 0.0 | 0.0 | 1.39 | 29.8 35.1 | 20.7 | 17.4 20.5 | 10.8 | 98.2 115 | 60.9 71.8 |
| 210 | 0.5 | 4.5 | 0.0 | 0.0 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.6 | 5.1 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 0.6 | 5.7 | 0.0 | 0.0 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 401 | 1.0 | 7.7 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 24.5 | 258 | 161 |
| 472 | 1.3 | 9.0 | 0.0 | 0.0 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 647 | 1.4 | 10.4 | 0.0 | 0.0 | 0.383 | 108 | 75.0 | 63.3 74.0 | 39.2 45.8 | 356 | 221 |
| 757 | 1.5 | 13.7 | 0.0 | 0.0 | 0.280 | 148 | 103 | 86.6 | 53.6 | 410 | 303 |
| 887 | 2.0 | 15.7 | 0.0 | 0.0 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 2.4 | 18.1 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1439 | 3.1 | 20.8 | 0.0 | 0.0 | 0.147 | 282 | 196 | 140 | 102 | 927 | 576 |
| 1688 | 4.2 | 28.1 | 5.5 | 5.5 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 2.8 | 30.9 | 3.7 | 9.2 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2510 | 10.8 | 49.4 | 14.2 | 33.5 | 0.0845 | 420 | 342 | 245 | 178 | 1618 | 1006 |
| 2945 | 10.9 | 60.3 | 14.3 | 47.8 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3449 | 31.7 | 92.0 | 41.7 | 89.5 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4728 | 0.1 | 98.8 | 0.1 | 98.4 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.3 | 99.1 | 0.4 | 98.8 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 0.4 | 99.4 | 0.5 | 99.3 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 0.3 | 99.7 99.9 | 0.4 | 99.0 99.9 | 0.0301 | 1548 | 1075 | 803 904 | 498 560 | 4327 5091 | 3162 |
| 8920 | 0.1 | 100.0 | 0.1 | 99.9 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1406 | 740 870 | 7909 | 4185 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 2344 | 1309 | 11900 | 7403 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29576 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 6236 | 4000 | 3562 3640 | 2081 | 20482 | 11765 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 5935 | 4617 4989 | 2858 | 25982 28073 | 16156 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | /542 8153 | 6339 6853 | 3924 4242 | 356/3 38564 | 22182 |









(C) Pore Size Distribution plot

ACS LABORATORES PTY. LTD.

| Well Sample | Depth | | 1 | Merrlieu- 769.00 n | 4 n | | | | | | |
|----------------|---------------|-----------------|-----------|-----------------------|---------------------|----------------------------------|----------------|-----------------|----------------|--------------|------------------------|
| Client | Geoscience | Victoria | | Density (| radients (nsi/foot) | | Com | version Paramet | ers (dynes/cm |) | |
| Well | Meerlieu-4 | victoria | | Density C | Typical | | Conv | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | sure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | 2 | | | Gas: | 0.100 | Reservoir Theta Reservoir IET | | 0.0 50.0 | | 30.0 30.0 | 0.0 26.0 |
| Depth | 2 769.00 m | | | CO2 Density | 0.215 | Laboratory Tco: | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| Ambient Pern | neability | | | | Estimated Column | Entry P | ressure (psia) | Displacement F | ressure (psia) | Threshold P | ressure (psia) |
| Ambient Poro | sity m) | 0.039 | | System A-Hg | Height (feet) | Lab 2709 | Res Con | Lab 3340 | Resv | Lab 3602 | Resv |
| pore rautus (µ |) | 0.057 | | G-W | 1086 | 532 | 369 | 655 | 455 | 707 | 491 |
| | | | | O-W | 1745 | 177 | 192 | 218 | 237 | 236 | 255 |
| | | | | CO ₂ -W | 565 | 532 | 192 | 655 | 237 | 707 | 255 |
| | | | | | | E 1 1 4 | L' C D | 0.1/D . | 0'1/D : | 11 - 1 - 41 | TT : 1 / 41 |
| | Raw | / Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1.01 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.41 |
| 1.98 | 0.7 | 0.7 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 0.3 | 1.1 | 0.0 | 0.0 | 77.7 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.1 | 1.2 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.2 | 1.4 | 0.0 | 0.0 | 56.9 48.4 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 5.18 | 0.2 | 1.5 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.50 | 0.37 | 3.34 | 2.08 |
| 5.97 | 0.1 | 1.8 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.2 | 2.0 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.2 | 2.2 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.2 | 2.4 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 7.42 | 3.97 |
| 13.5 | 0.2 | 3.5 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.52 | 0.82 | 8.66 | 5.41 |
| 15.5 | 0.3 | 3.7 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.3 | 4.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.3 | 4.3 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.3 | 4.6 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 39.7 | 0.4 | 5.0 | 0.0 | 0.0 | 5.34 | 7.78 | 5.40 | 4.54 | 2.12 | 25.5 | 15.9 |
| 49.5 | 0.1 | 5.1 | 0.0 | 0.0 | 4.28 | 9.71 | 6.74 | 5.66 | 3.50 | 31.8 | 19.8 |
| 57.3 | 0.0 | 5.1 | 0.0 | 0.0 | 3.70 | 11.2 | 7.78 | 6.56 | 4.06 | 36.9 | 22.9 |
| 67.8 | 0.1 | 5.3 | 0.0 | 0.0 | 3.13 | 13.3 | 9.24 | 7.76 | 4.80 | 43.6 | 27.2 |
| 80.3 | 0.1 | 5.4 | 0.0 | 0.0 | 2.64 | 15.7 | 10.9 | 9.19 | 5.69 | 51.7 | 32.1 |
| 111 | 0.1 | 5.6 | 0.0 | 0.0 | 1.92 | 21.8 | 12.8 | 12.7 | 7.86 | 71.5 | 44.4 |
| 130 | 0.1 | 5.7 | 0.0 | 0.0 | 1.63 | 25.5 | 17.7 | 14.9 | 9.22 | 83.8 | 52.1 |
| 155 | 0.1 | 5.8 | 0.0 | 0.0 | 1.37 | 30.4 | 21.1 | 17.7 | 11.0 | 100 | 62.1 |
| 181 | 0.1 | 5.9 | 0.0 | 0.0 | 1.17 | 35.5 | 24.7 | 20.7 | 12.8 | 116 | 72.6 |
| 211 248 | 0.1 | 6.0 | 0.0 | 0.0 | 0.853 | 41.4 | 28.8 | 24.1 | 14.9 | 135 | 84.7 99.4 |
| 294 | 0.1 | 6.3 | 0.1 | 0.1 | 0.722 | 57.6 | 40.0 | 33.6 | 20.8 | 189 | 118 |
| 345 | 0.2 | 6.4 | 0.2 | 0.3 | 0.615 | 67.6 | 46.9 | 39.5 | 24.5 | 223 | 138 |
| 405 | 0.2 | 6.6 | 0.2 | 0.5 | 0.523 | 79.4 | 55.1 | 46.3 | 28.7 | 261 | 162 |
| 475 | 0.2 | 6.8 7.1 | 0.2 | 0.7 | 0.447 | 93.1 | 64.7 75.7 | 54.4 | 33.7 | 306 | 190 |
| 650 | 0.3 | 7.4 | 0.3 | 1.3 | 0.326 | 109 | 88.2 | 74.4 | 46.1 | 419 | 259 |
| 760 | 0.4 | 7.8 | 0.4 | 1.7 | 0.279 | 149 | 103 | 87.0 | 53.9 | 490 | 303 |
| 890 | 0.5 | 8.2 | 0.5 | 2.3 | 0.238 | 175 | 122 | 102 | 63.1 | 574 | 359 |
| 1049 | 0.6 | 8.9 | 0.7 | 2.9 | 0.202 | 206 | 143 | 120 | 74.3 | 675 | 421 |
| 1230 | 0.8 | 9.6 | 0.8 | 3.7 4.7 | 0.172 | 241 | 107 | 141 | 87.5 102 | 927 | 491 576 |
| 1692 | 1.2 | 11.7 | 1.3 | 6.0 | 0.125 | 332 | 231 | 194 | 120 | 1091 | 679 |
| 1831 | 0.7 | 12.4 | 0.8 | 6.7 | 0.116 | 359 | 249 | 210 | 130 | 1182 | 732 |
| 2146 | 1.7 | 14.1 | 1.8 | 8.5 | 0.0988 | 421 | 292 | 246 | 152 | 1382 | 859 |
| 2511 | 1.7 | 15.8 | 1.8 | 10.4 | 0.0844 | 492 577 | 342 401 | 287 | 1/8 | 1018 | 1006 |
| 3449 | 4.8 | 23.7 | 5.1 | 18.7 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4042 | 7.4 | 31.1 | 7.9 | 26.6 | 0.0524 | 793 | 551 | 463 | 287 | 2609 | 1621 |
| 4728 | 17.6 | 48.7 | 18.8 | 45.4 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5106 | 9.6 10 4 | 58.3 77 7 | 10.2 | 55.6 | 0.0415 | 1001 | 695 | 584 | 362 | 3291 | 2044 |
| 7022 | 22.1 | 99.8 | 20.7 | 70.5 99.8 | 0.0354 | 1377 | 956 | 804 | 423 | 4527 | 2400 |
| 7886 | 0.0 | 99.8 | 0.0 | 99.8 | 0.0269 | 1546 | 1074 | 902 | 558 | 5073 | 3159 |
| 8916 | 0.1 | 99.9 | 0.1 | 99.9 | 0.0238 | 1748 | 1214 | 1020 | 631 | 5736 | 3571 |
| 9648 | 0.1 | 99.9 | 0.1 | 99.9 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10432 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1406 | 740 870 | 7909 | 4185 4921 |
| 14331 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18479 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3623 | 2516 | 2115 | 1309 | 11900 | 7400 |
| 20480 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 25148 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3413 | 2049 2868 | 1040 | 14909 | 9271 10038 |
| 27137 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3106 | 1923 | 17482 | 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31803 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34423 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6750 | 4688 | 3939 | 2438 | 22164 | 13788 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 5493 | 4256 | 2635 | 23955 | 14897 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47294 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55385 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35673 | 22182 |
| 37860 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11/41 | 8133 | 0805 | 4242 | 38304 | 23719 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well Sample | Depth | | N 6 | Aeerlieu 599.9 m | 15001 | | | | | | |
|--|--|---|--|---|---|---|---|---|--|---|--|
| Client Well | Geoscience A Meerlieu-150 | AVIctoria 001 | | Density Water: | Gradients (psi/foot) Typical 0.440 | Laboratory Thet | Cor | air/water | ters (dynes/cm air/oil 0.0 | oil/water 30.0 | CO ₂ /water 0.0 |
| Test Method Sample Depth | Air/Mercury M15001 699.90 m | Capillary Pressu | ire | Oil: Gas: CO ₂ Density | 0.330 0.100 | Laboratory IFT Reservoir Theta Reservoir IFT Laboratory Tcos | Theta | 72.0 0.0 50.0 72.0 | 24.0 24.0 | 48.0 30.0 30.0 42.0 | 72.0 0.0 26.0 72.0 |
| Pore radius (µ | m) | 0.176 | | System A-Hg G-W O-W | Estimated Column Height (feet) na 242 390 | Keservoir 1 cos1 Entry P Lab 605 119 39.6 | ressure (psia) Res Con - 82.4 42.9 | 50.0 Displacement F Lab 932 183 60.9 | Pressure (psia) Resv - 127 66.0 | 26.0 Threshold I Lab 1033 203 67.6 | 26.0 Pressure (psia) Resv - 141 73.2 |
| | | | | CO ₂ -W | 118 | 119 Equivalent | 42.9 Injection Pressures | 183 Oil/Brine | 66.0 Oil/Brine | 203 Height Above | 73.2 Height Above |
| Pressure (psia) | Raw Intrusion (percent) | Data Saturation (percent) | Conforma Intrusion (percent) | Saturation (percent) | Pore Diameter (μm) | Air/Brine Lab (psi) | Air/Brine Res Con (psi) | Lab Conditions (psi) | Reservoir Conditions (psi) | Free Water Oil-Water (feet) | Free Water Gas-Water (feet) |
| (psia) 1.00 1.98 2.73 3.18 3.73 4.38 5.98 6.97 8.27 9.97 9.97 9.97 9.97 9.97 11.5 13.5 15.5 18.5 21.6 25.3 30.0 37.2 47.2 56.6 66.3 80.4 93.0 111 129 152 179 210 247 292 343 401 472 553 647 757 887 1048 1227 1439 1688 1828 2142 2510 | (percent) 0.0 0.8 0.3 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 | (percent) 0.0 0.8 1.1 1.3 1.5 1.7 1.9 2.0 2.2 2.4 2.5 2.6 2.9 3.0 3.3 3.6 3.9 4.2 4.2 4.3 4.4 4.5 5.5 5.8 6.3 6.8 7.4 7.9 8.6 9.4 10.3 11.5 1.7 1.9 8.6 9.4 10.3 11.5 1.7 1.9 1.7 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.5 1.7 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.9 1.7 1.7 1.9 1.7 1.7 1.9 1.7 1.7 1.9 1.7 1.7 1.7 1.7 1.9 1.5 1.3 1.5 1.5 1.3 1.5 1.5 1.3 1.5 1.5 1.3 1.5 1.5 1.3 1.5 1.5 1.5 1.5 1.3 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 | (percent) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0. | (percent) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0. | (µm) 211 107 77.6 66.7 56.9 48.4 41.0 35.5 30.4 25.6 21.3 18.5 15.7 13.7 11.5 9.83 8.39 7.08 5.70 4.49 3.75 3.20 2.64 2.28 1.91 1.65 1.39 1.18 1.01 0.860 0.726 0.619 0.528 0.483 0.383 0.328 0.239 0.202 0.173 0.147 0.126 0.116 0.0990 0.0845 | (psi) 0.20 0.39 0.54 0.62 0.73 0.86 1.02 1.17 1.37 1.62 2.55 2.65 3.04 3.63 4.24 4.96 5.88 7.29 9.25 11.1 13.0 15.8 18.2 21.8 25.3 29.8 35.1 41.2 48.4 57.3 78.6 92.5 108 127 148 174 205 241 255 241 255 265 265 265 265 265 265 265 | (psi) 0.14 0.27 0.37 0.43 0.51 0.60 0.71 0.81 0.95 1.13 1.35 1.56 1.84 2.11 2.52 2.94 3.44 4.08 5.06 6.42 7.71 9.03 11.0 12.6 15.1 17.6 20.7 24.4 28.6 33.6 39.8 46.7 54.6 64.2 75.0 88.2 103 121 142 167 196 230 249 249 242 242 244 211 211 211 211 211 | (psi) 0.11 0.23 0.31 0.36 0.43 0.50 0.59 0.68 0.80 0.95 1.14 1.32 1.54 1.54 1.54 1.54 1.77 2.12 2.47 2.90 3.43 4.26 5.40 6.48 7.59 9.20 10.6 12.7 14.8 17.4 20.5 24.0 28.3 33.4 39.3 35.4 0.68 17.4 28.3 33.4 39.3 35.4 0.68 17.4 28.3 33.4 39.3 35.4 0.68 17.4 28.5 24.0 28.3 33.4 39.3 35.4 0.68 17.4 28.3 33.4 39.3 35.4 0.68 17.4 28.3 33.4 39.3 35.4 0.68 17.5 24.0 28.3 33.4 39.3 35.4 0.68 17.5 24.0 28.3 33.4 39.3 35.4 0.68 17.5 24.0 28.3 33.4 39.3 35.4 0.68 17.5 24.0 28.3 33.4 39.3 35.4 0.65 10.2 10.6 10.2 10.6 10.2 10.6 10.5 24.0 28.3 33.4 39.3 35.4 10.6 10.2 10.6 10.2 10.6 10.6 10.2 10.6 10.6 10.2 10.6 10.6 10.2 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.7 10.6 10.2 10.6 10.6 10.2 10.0 10.6 10.2 10.0 10.6 10.2 10.0 | (psi) 0.07 0.14 0.19 0.23 0.26 0.31 0.37 0.42 0.49 0.59 0.71 0.82 0.95 1.10 1.31 1.53 1.80 2.12 2.64 3.34 4.01 4.70 6.56 7.86 9.16 10.8 12.7 2.64 3.34 4.01 4.70 6.57 7.86 9.16 10.8 12.7 2.64 3.34 4.01 4.70 6.56 7.86 6.56 7.86 9.16 10.8 12.7 2.64 3.34 4.01 4.70 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.50 7.86 6.56 7.86 6.50 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.56 7.86 6.50 7.85 0.71 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1. | (feet) 0.64 1.28 1.75 2.05 2.40 2.82 3.34 3.85 4.49 5.33 6.42 7.43 8.66 10.0 11.9 13.9 16.4 19.3 24.0 30.4 36.5 42.7 51.8 59.6 71.5 8.33 98.2 115 135 159 188 221 258 304 416 487 574 675 788 927 1082 1173 1382 1618 | (feet) 0.40 0.79 1.09 1.27 1.49 1.76 2.08 2.39 2.80 3.32 3.97 4.59 5.41 6.21 7.41 8.65 10.1 12.0 14.9 18.9 22.7 26.6 32.4 37.1 44.4 51.8 60.9 71.8 84.1 98.8 117 137 161 189 221 259 303 356 418 491 576 676 732 859 1006 |
| 2945 3449 4040 4728 5114 6002 7033 7895 8920 9649 10452 12283 14333 16381 | $\begin{array}{c} 0.6\\ 0.1\\ 0.1\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$ | 99.7 99.8 99.9 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.7 0.1 0.0 | 99.7 99.8 99.9 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.0720 0.0615 0.0525 0.0448 0.0415 0.0353 0.0301 0.0269 0.0238 0.0220 0.0203 0.0173 0.0148 0.0129 | 577 676 792 927 1003 1177 1379 1548 1749 1892 2049 2408 2810 3212 | 401 469 550 644 697 817 958 1075 1215 1314 1423 1672 1951 2231 | 337 395 462 541 585 687 805 904 1021 1104 1196 1406 1640 1875 | 209 245 286 335 362 425 498 560 632 683 740 870 1015 | 1900 2227 2600 3045 3291 3864 4527 5091 5745 6209 6727 7909 9227 10555 | 1179 1379 1618 1894 2050 2403 2818 3162 3574 3865 4185 4918 5738 6562 |
| 18481 20481 23149 25064 27135 29376 31804 34421 37192 40343 40343 40343 40343 43591 47291 51172 55387 59880 | 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | $\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$ | 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.0115 0.0104 0.0092 0.0085 0.0078 0.0072 0.0067 0.0062 0.0053 0.0049 0.0045 0.0041 0.0038 0.0038 | 3624 4016 4539 4915 5321 5760 6236 6749 7293 7910 8547 9273 10034 10860 11741 | 2517 2789 3152 3413 3695 4000 4331 4687 5065 5493 5935 6440 6968 7542 8153 | 2115 2344 2649 2868 3105 3362 3640 3939 4256 4617 4989 5412 5856 6339 6853 | 1309 1451 1640 1775 1922 2081 2253 2438 2635 2858 3088 3350 3625 3924 4242 | 11900 13191 14909 16136 17473 18918 20482 22164 23955 25982 28073 30455 32955 35673 38564 | 7403 8203 9271 10038 10868 11765 12738 13785 14897 16156 17456 18941 20494 22182 23979 |

598800.0100.00.0100.0(A) Interpreted Capillary Pressure Chart



⁽B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Vell ample | Depth | | N B | /ullungd 863.00 m | ung-7 เ | | | | | | |
|---------------------|------------------------|---------------------------|------------------------|---------------------------------|---------------------------|---|--------------------------|--------------------------|------------------------|---------------------------|---------------------------------------|
| lient | Geoscience | AVictoria | | Density (| Gradients (psi/foot) | | Co | nversion Parame | ters (dynes/cn |) | |
| √ell `est Method | Mullungdun | g-7 Capillary Pressure | e | Water: Oil: | Typical 0.440 0.330 | Laboratory Thet Laboratory IFT | a | air/water 0.0 72.0 | air/oil 0.0 24.0 | oil/water 30.0 48.0 | CO ₂ /water 0.0 72.0 |
| ample epth | M7 363.00 m | | | Gas: CO ₂ Density | 0.100 | Reservoir Theta Reservoir IFT Laboratory Tcos | Theta | 0.0 50.0 72.0 | 24.0 | 30.0 30.0 42.0 | 0.0 26.0 72.0 |
| | | | | | Estimated Column | Reservoir Tcos Entry F | Theta Pressure (psia) | 50.0 Displacement F | Pressure (psia) | 26.0 Threshold F | 26.0 Pressure (psia) |
| əre radius (µ | ım) | 2.34 | | System A-Hg | Height (feet) na | Lab 45.5 | Res Con | Lab 98.3 | Resv - | Lab 126 | Resv - |
| | | | | O-W CO ₂ -W | 29 8 | 8.92 2.97 8.92 | 3.22 3.22 | 6.43 19.3 | 6.96 6.96 | 8.27 24.8 | 8.96 8.96 |
| | Pau | 7 Data | Conform | unce Corrected | Dore | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine Reservoir | Height Above | Height Above |
| Pressure (psia) | Intrusion (percent) | Saturation (percent) | Intrusion (percent) | Saturation (percent) | Diameter (µm) | Lab (psi) | Res Con (psi) | Conditions (psi) | Conditions (psi) | Oil-Water (feet) | Gas-Water (feet) |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2.73 | 1.0 | 3.3 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 3.73 | 0.4 | 5.7 4.3 | 0.0 | 0.0 | 56.9 | 0.62 | 0.43 | 0.36 | 0.23 0.26 | 2.05 2.40 | 1.27 |
| 4.38 | 0.6 | 4.8 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 5.98 | 0.7 | 5.5 6.1 | 0.0 | 0.0 | 41.0 35.5 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 3.85 | 2.08 |
| 6.97 | 0.7 | 6.8 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 9.97 | 0.6 | 8.2 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 6.42 | 3.32 3.97 |
| 11.5 | 0.6 | 8.7 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 15.5 | 0.8 0.6 | 9.5 10.1 | 0.0 0.0 | 0.0 0.0 | 15.7 13.7 | 2.65 3.04 | 1.84 2.11 | 1.54 1.77 | 0.95 | 8.66 10.0 | 5.41 6.21 |
| 18.5 | 0.6 | 10.6 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.6 | 11.2 12.0 | 0.0 | 0.0 | 9.83 8.39 | 4.24 4.96 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 10.1 |
| 30.0 | 0.6 | 12.6 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 47.2 | 0.4 | 12.9 | 0.0 | 0.0 | 5.70 4.49 | 7.29 | 5.06 | 4.26 5.40 | 2.64 | 24.0 30.4 | 14.9 18.9 |
| 56.6 | 1.2 | 14.8 | 1.4 | 1.4 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 80.4 | 1.4 | 16.2 18.4 | 1.6 | 3.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 32.4 |
| 93.0 | 2.6 | 21.0 | 3.0 | 8.6 | 2.04 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 3.4 | 24.4 | 3.9 | 12.5 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 3.6 | 31.5 | 4.2 | 20.7 | 1.65 | 25.5 | 20.7 | 14.8 | 9.16 | 83.5 98.2 | 60.9 |
| 179 | 3.8 | 35.3 | 4.4 | 25.1 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 247 | 4.1 | 39.4 44.0 | 4.7 5.4 | 29.8 35.2 | 1.01 | 41.2 | 28.6 | 24.0 28.3 | 14.9 17.5 | 135 | 84.1 98.8 |
| 292 | 4.7 | 48.7 | 5.4 | 40.6 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 401 | 6.0 5.8 | 54.7 60.5 | 6.9 6.7 | 47.5 54.2 | 0.619 | 67.3 78.6 | 46.7 54.6 | 39.3 | 24.3 | 221 | 137 |
| 472 | 7.3 | 67.8 | 8.5 | 62.7 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 7.9 | 75.7 | 9.2 | 71.9 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 757 | 8.9 | 84.6 95.9 | 10.3 | 82.2 95.3 | 0.328 | 127 | 88.2 103 | /4.0 86.6 | 45.8 53.6 | 416 487 | 259 303 |
| 887 | 2.1 | 98.0 | 2.5 | 97.7 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 1227 | 0.3 | 98.4 98 7 | 0.4 | 98.1 98.4 | 0.202 | 205 241 | 142 167 | 120 140 | 74.3 86 7 | 675 788 | 418 491 |
| 1439 | 0.3 | 99.0 | 0.4 | 98.8 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 0.4 | 99.4 99.5 | 0.4 | 99.3 99.4 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 732 |
| 2142 | 0.2 | 99.7 | 0.2 | 99.4 99.6 | 0.0990 | 420 | 292 | 245 | 129 | 1382 | 859 |
| 2510 | 0.1 | 99.8 | 0.1 | 99.7 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 3449 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0720 | 676 | 469 | 395 | 209 | 2227 | 1379 |
| 4040 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 5114 | 0.0 0.0 | 100.0 100.0 | 0.0 | 100.0 100.0 | 0.0448 0.0415 | 927 1003 | 644 697 | 541 585 | 335 362 | 3045 3291 | 1894 2050 |
| 6002 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 7895 | 0.0 | 100.0 100.0 | 0.0 | 100.0 100.0 | 0.0301 | 1379 1548 | 958 1075 | 805 904 | 498 560 | 4527 5091 | 2818 3162 |
| 8920 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 9649 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 740 | 6209 6727 | 3865 4185 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 0.0115 | 3212 3624 | 2231 2517 | 2115 | 1309 | 10555 | 6562 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 25064 | 0.0 0 0 | 100.0 100.0 | 0.0 | 100.0 100 0 | 0.0092 0.0085 | 4539 4915 | 3152 3413 | 2649 2868 | 1640 1775 | 14909 16136 | 9271 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 20482 22164 | 12/38 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 43591 | 0.0 | 100.0 100.0 | 0.0 | 100.0 100.0 | 0.0053 0.0049 | 7910 8547 | 5493 5935 | 4617 4989 | 2858 3088 | 25982 28073 | 16156 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 | 5856 | 3625 | 32955 | 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | /542 | 6339 | 3924 | 35673 | 22182 |



(B) Capillary Pressure Plot



ACS LABORATORIES PTY. LTD.

WellSale-13Sample Depth748.1 m



| Client | Cassaianaa | Viatoria | | Donaity (| readiants (nsi/foot) | Conversion Parameters (dynes/cm) | | | | | | | |
|----------------|-----------------------|------------------|--------------|---------------|----------------------|----------------------------------|---------------------|----------------|-----------------|--------------|-----------------|--|--|
| Well | Sala 12 | A VICTOLIA | | Density | Typical | | Con | air/water | air/oil | oil/water | CO./water | | |
| wen | Sule-15 | | | Water: | 0.440 | Laboratory Thet | я | 0.0 | 0.0 | 30.0 | 0.0 | | |
| Test Method | Air/Mercury | Capillary Pressu | re | Oil: | 0.330 | Laboratory IFT | u | 72.0 | 24.0 | 48.0 | 72.0 | | |
| | | | | Gas: | 0.100 | Reservoir Theta | | 0.0 | | 30.0 | 0.0 | | |
| Sample | S13-1 | | | | | Reservoir IFT | Reservoir IFT | | | 30.0 | 26.0 | | |
| Depth | 748.10 m | | | CO2 Density | 0.180 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 | | |
| | | | | | | Reservoir TcosT | heta | 50.0 | | 26.0 | 26.0 | | |
| D |) | 0.0/1 | | Contant | Estimated Column | Entry P | ressure (psia) | Displacement P | Pressure (psia) | Threshold I | Pressure (psia) | | |
| rore radius (µ | ore radius (μm) 0.061 | | | | neight (leet) | 1749 | Kes Con | 1811 | Resv | 1922 | Resv | | |
| | | | | G-W | 701 | 343 | 238 | 355 | 247 | 377 | 262 | | |
| | | | | O-W | 1126 | 114 | 124 | 118 | 128 | 126 | 136 | | |
| | | | | CO2-W | 349 | 343 | 124 | 355 | 128 | 377 | 136 | | |
| | | | | | | | | | | | | | |
| | _ | _ | | | _ | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above | | |
| Dessentes | Raw | v Data | Conforma | nce Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water | | |
| (nsia) | (percent) | (nercent) | (nercent) | (nercent) | (um) | (nsi) | (nsi) | (nsi) | (nsi) | (feet) | (feet) | | |
| (point) | (percent) | (percent) | (percent) | (percent) | (J) | (551) | (1997) | (psi) | (151) | (1001) | (1001) | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 | | |
| 2 73 | 0.4 | 1.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.27 | 0.25 | 0.14 | 1.20 | 1.09 | | |
| 3.18 | 0.2 | 1.6 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 | | |
| 3.73 | 0.2 | 1.8 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 | | |
| 4.38 | 0.2 | 2.0 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 | | |
| 5.18 | 0.2 | 2.2 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 | | |
| 5.98 | 0.2 | 2.4 | 0.0 | 0.0 | 35.5 30.4 | 1.1/ | 0.81 | 0.08 | 0.42 | 5.85 1 10 | 2.39 | | |
| 8.27 | 0.2 | 2.8 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.49 | 5.33 | 3.32 | | |
| 9.97 | 0.3 | 3.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 | | |
| 11.5 | 0.2 | 3.2 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 | | |
| 13.5 | 0.2 | 3.4 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 | | |
| 15.5 | 0.2 | 3.6 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 | | |
| 21.6 | 0.2 | 3.8 4.0 | 0.0 | 0.0 | 9.83 | 3.03 4.24 | 2.52 | 2.12 | 1.51 | 11.9 | 7.41 | | |
| 25.3 | 0.2 | 4.2 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 | | |
| 30.0 | 0.3 | 4.5 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 | | |
| 37.2 | 0.1 | 4.5 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 | | |
| 47.2 | 0.1 | 4.6 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 | | |
| 56.6 | 0.1 | 4.7 | 0.1 | 0.1 | 3.75 | 11.1 | 7.71 | 6.48 7.50 | 4.01 | 36.5 | 22.7 | | |
| 80.4 | 0.1 | 4.8 | 0.1 | 0.2 | 2.64 | 15.0 | 9.03 | 9.20 | 5 70 | 51.8 | 32.4 | | |
| 93.0 | 0.1 | 5.0 | 0.1 | 0.4 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 | | |
| 111 | 0.1 | 5.1 | 0.2 | 0.6 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 | | |
| 129 | 0.1 | 5.3 | 0.1 | 0.7 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 | | |
| 152 | 0.2 | 5.4 | 0.2 | 0.9 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 | | |
| 210 | 0.2 | 5.6 | 0.2 | 1.1 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 | | |
| 247 | 0.2 | 6.0 | 0.2 | 1.4 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 | | |
| 292 | 0.2 | 6.2 | 0.2 | 1.6 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 | | |
| 343 | 0.2 | 6.4 | 0.2 | 1.9 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 | | |
| 401 | 0.3 | 6.7 | 0.3 | 2.1 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 | | |
| 4/2 | 0.3 | 6.9 7.2 | 0.3 | 2.4 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 | | |
| 647 | 0.3 | 7.5 | 0.3 | 3.1 | 0.328 | 103 | 88.2 | 74.0 | 45.8 | 416 | 259 | | |
| 757 | 0.4 | 7.9 | 0.4 | 3.5 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 | | |
| 887 | 0.5 | 8.4 | 0.5 | 4.0 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 | | |
| 1048 | 0.6 | 9.0 | 0.6 | 4.6 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 | | |
| 1/22/ | 0.8 | 9.8 | 0.8 | 5.4 | 0.1/3 | 241 | 16/ | 140 | 86./ | /88 | 491 | | |
| 1688 | 2.0 | 12.9 | 2.1 | 8.7 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 | | |
| 1828 | 2.1 | 15.0 | 2.2 | 10.9 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 | | |
| 2142 | 10.1 | 25.1 | 10.6 | 21.4 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 | | |
| 2510 | 25.2 | 50.2 | 26.4 | 47.8 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 | | |
| 2945 | 36.3 | 86.5 | 38.0 13.6 | 85.8 99.4 | 0.0720 | 577 | 401 | 337 | 209 | 2227 | 11/9 | | |
| 4040 | 0.0 | 99.5 | 0.0 | 99.4 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 | | |
| 4728 | 0.2 | 99.7 | 0.2 | 99.6 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 | | |
| 5114 | 0.2 | 99.9 | 0.2 | 99.9 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 | | |
| 6002 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 | | |
| 7033 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 | | |
| 8920 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 | | |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 | | |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 | | |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 | | |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5/38 6562 | | |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 | | |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 | | |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 | | |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 | | |
| 2/135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 | | |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 6236 | 4331 | 3640 | 2081 | 20482 | 12738 | | |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 | | |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 | | |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 | | |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 | | |
| 47291 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 10034 | 0440 6968 | 5856 | 3625 | 30455 | 204941 | | |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 | | |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 | | |







(C) Pore Size Distribution plot



| Client | Geoscience | A Victoria | | Density G | radients (psi/foot) | Conversion Parameters (dynes/cm) | | | | | | | |
|----------------|-------------------|----------------------|------------|--------------------------|---------------------|----------------------------------|----------------------|----------------|----------------|-------------------------|-------------------------|--|--|
| Well | Sale-13 | | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water | | |
| | | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 | | |
| Test Method | Air/Mercury | Capillary Pressu | ire | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 | | |
| с I | 612.2 | | | Gas: | 0.100 | Reservoir Theta | | 0.0 | | 30.0 | 0.0 | | |
| Sample | 513-2 705.60 m | | | CO Density | 0.205 | Laboratory Teor | Thata | 72.0 | 24.0 | 30.0 | 20.0 | | |
| Deptii | 795.00 III | | | CO ₂ Delisity | 0.205 | Reservoir Tcos | Theta | 50.0 | 24.0 | 26.0 | 26.0 | | |
| | | | | | Estimated Column | Entry P | ressure (psia) | Displacement P | ressure (psia) | Threshold P | ressure (psia) | | |
| Pore radius (µ | ι m) | 0.075 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv | | |
| | | | | A-Hg | na 570 | 1421 | - | 1682 | - | 1962 | - | | |
| | | | | 0-W | 915 | 92.9 | 194 | 110 | 119 | 128 | 139 | | |
| | | | | CO ₂ -W | 293 | 279 | 101 | 330 | 119 | 385 | 139 | | |
| | | | | , | | | ÷ | | | | | | |
| | _ | _ | | | _ | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above | | |
| Pressure | Intrusion | / Data Saturation | Conforma | nce Corrected | Pore | Air/Brine | Air/Brine Res Con | Lab | Conditions | Free Water Oil Water | Free Water Gas Water | | |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) | | |
| | _ | | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 | | |
| 1.98 | 0.3 | 0.3 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 | | |
| 2.73 | 0.1 | 0.5 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 | | |
| 3.18 | 0.1 | 0.5 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 | | |
| 5.75 4.38 | 0.1 | 0.6 | 0.0 | 0.0 | 56.9 48.4 | 0.75 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 | | |
| 5.18 | 0.1 | 0.7 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 | | |
| 5.98 | 0.2 | 0.9 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 | | |
| 6.97 | 0.1 | 1.0 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 | | |
| 8.27 | 0.1 | 1.1 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 | | |
| 9.97 | 0.1 | 1.2 | 0.0 | 0.0 | 21.3 18 5 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 7.43 | 3.97 4.59 | | |
| 13.5 | 0.1 | 1.4 | 0.0 | 0.0 | 15.7 | 2.25 | 1.84 | 1.54 | 0.82 | 8.66 | 5.41 | | |
| 15.5 | 0.1 | 1.6 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 | | |
| 18.5 | 0.1 | 1.7 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 | | |
| 21.6 | 0.1 | 1.8 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 | | |
| 25.5 | 0.1 | 2.0 | 0.0 | 0.0 | 8.39 7.08 | 4.90 | 5.44 4.08 | 2.90 | 2.12 | 10.4 | 10.1 | | |
| 37.2 | 0.0 | 2.6 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 | | |
| 47.2 | 0.0 | 2.6 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 | | |
| 56.6 | 0.0 | 2.6 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 | | |
| 66.3 | 0.0 | 2.7 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 | | |
| 80.4 93.0 | 0.1 | 2.8 | 0.0 | 0.0 | 2.64 | 15.8 | 12.6 | 9.20 | 5.70 | 59.6 | 32.4 | | |
| 111 | 0.2 | 3.0 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 | | |
| 129 | 0.2 | 3.3 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 | | |
| 152 | 0.3 | 3.6 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 | | |
| 210 | 0.3 | 3.8 4.1 | 0.0 | 0.0 | 1.18 | 35.1 41.2 | 24.4 | 20.5 | 12.7 | 115 | 71.8 | | |
| 247 | 0.3 | 4.4 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 | | |
| 292 | 0.4 | 4.7 | 0.0 | 0.0 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 | | |
| 343 | 0.4 | 5.1 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 | | |
| 401 | 0.5 | 5.7 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 | | |
| 553 | 0.5 | 6.7 | 0.0 | 0.0 | 0.383 | 92.5 108 | 75.0 | 63.3 | 39.2 | 356 | 221 | | |
| 647 | 0.7 | 7.4 | 0.0 | 0.0 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 | | |
| 757 | 0.8 | 8.2 | 0.0 | 0.0 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 | | |
| 887 | 1.0 | 9.2 | 0.0 | 0.0 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 | | |
| 1048 | 1.2 | 10.4 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 788 | 418 | | |
| 1439 | 1.9 | 13.8 | 2.1 | 2.1 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 | | |
| 1688 | 2.6 | 16.4 | 2.9 | 5.1 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 | | |
| 1828 | 2.1 | 18.5 | 2.4 | 7.5 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 | | |
| 2142 | 6.2 | 24.7 | 7.0 | 14.5 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 | | |
| 2945 | 10.9 | 44.3 | 12.4 | 36.7 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 | | |
| 3449 | 8.0 | 52.3 | 9.1 | 45.8 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 | | |
| 4040 | 10.6 | 62.9 | 12.0 | 57.9 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 | | |
| 4728 | 14.1 | 77.0 | 16.0 | 73.9 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 | | |
| 6002 | 4.5 | 01.5 88.2 | 5.1 7.6 | 79.0 86.6 | 0.0415 | 1005 | 817 | 585 687 | 425 | 3864 | 2403 | | |
| 7033 | 5.2 | 93.5 | 6.0 | 92.6 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 | | |
| 7895 | 3.3 | 96.8 | 3.8 | 96.3 | 0.0269 | 1548 | 1075 | 904 | 560 | 5091 | 3162 | | |
| 8920 | 2.5 | 99.3 | 2.8 | 99.2 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 | | |
| 9649 | 0.6 | 99.9 100.0 | 0.7 | 99.8 100 0 | 0.0220 | 1892 | 1314 | 1104 | 683 740 | 6209 | 3803 4185 | | |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 | | |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 | | |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 | | |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 | | |
| 20481 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 3152 | 2544 2649 | 1451 | 14909 | 8203 9271 | | |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 | | |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 | | |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 | | |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 | | |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2438 | 23955 | 13/83 | | |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 | | |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 | | |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 | | |
| 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 6968 7542 | 5856 | 3625 | 32955 35673 | 20494 | | |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 | | |
| | | | _ | | | | | | - | | | | |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot
| Well | Sale-15 |
|--------------|---------|
| Sample Depth | 628.6 m |
| | |



| Client | Geoscience | AVictoria | | Density G | radients (psi/foot) | | Conv | version Paramete | ers (dynes/cm) | | |
|-----------------|-------------|------------------|-----------|-------------------------|-----------------------------------|-----------------|---------------------|-------------------------|----------------|----------------|------------------------|
| Well | Sale-15 | | | · · · · | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Pressu | ire | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| | | | | Gas: | 0.100 | Reservoir Theta | | 0.0 | | 30.0 | 0.0 |
| Sample | S15 | | | | | Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 628.60 m | | | CO ₂ Density | 0.166 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | E-thread Column | Reservoir Tcos | Theta | 50.0 Dianta ann an t | | 26.0 | 26.0 |
| Poro radius (u | m) | 0.229 | | System | Estimated Column Height (feet) | Entry P | Res Con | Lab | Resv | I hreshold P | Resv |
| i ore rautus (µ | m) | 0.22) | | A-Hg | na | 465 | - | 586 | - | 620 | - |
| | | | | G-W | 186 | 91.2 | 63.4 | 115 | 79.9 | 122 | 84.5 |
| | | | | O-W | 299 | 30.4 | 32.9 | 38.3 | 41.5 | 40.6 | 43.9 |
| | | | | CO ₂ -W | 91 | 91.2 | 32.9 | 115 | 41.5 | 122 | 43.9 |
| | | | | | | | | | | | |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| | Raw | v Data | Conforma | nce Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (ps1) | (psi) | (psi) | (psi) | (reet) | (reet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.0 | 0.0 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 0.0 | 0.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.0 | 0.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 | 0.0 | 0.0 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.0 | 0.0 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.0 | 0.0 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 6.97 | 0.0 | 0.0 | 0.0 | 0.0 | 30.4 | 1.17 | 0.95 | 0.08 | 0.42 | 4 49 | 2.59 |
| 8.27 | 0.0 | 0.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.0 | 0.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.0 | 0.0 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.0 | 0.0 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.0 | 0.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.0 | 0.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.0 | 0.0 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.5 | 0.0 | 0.0 | 0.0 | 0.0 | 8.39 7.08 | 4.90 | 5.44 4.08 | 2.90 | 2.12 | 10.4 | 10.1 |
| 37.2 | 0.0 | 0.0 | 0.0 | 0.0 | 5 70 | 7 29 | 5.06 | 4 26 | 2.12 | 24.0 | 14.9 |
| 47.2 | 0.2 | 0.3 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 56.6 | 0.3 | 0.5 | 0.0 | 0.0 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 | 0.4 | 0.9 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 | 1.0 | 1.9 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 1.0 | 2.9 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 1.1 | 4.0 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 1.1 | 5.1 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 132 | 1.2 | 7.5 | 0.0 | 0.0 | 1.39 | 29.0 | 20.7 | 20.5 | 10.8 | 96.2 | 71.8 |
| 210 | 1.2 | 87 | 0.0 | 0.0 | 1.10 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.0 | 8.7 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 1.1 | 9.8 | 0.0 | 0.0 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 1.5 | 11.3 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 | 1.6 | 12.9 | 1.8 | 1.8 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 2.2 | 15.1 | 2.5 | 4.3 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 3.2 | 18.3 | 3.6 | 8.0 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 757 | 24.8 | 20.7 | 27.9 | 45.3 | 0.528 | 127 | 103 | 74.0 86.6 | 43.8 | 410 | 303 |
| 887 | 24.0 | 76.3 | 28.0 | 73.3 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 20.9 | 97.2 | 23.5 | 96.8 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 1.4 | 98.6 | 1.6 | 98.5 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 0.0 | 98.6 | 0.0 | 98.5 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 0.1 | 98.8 | 0.1 | 98.6 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 0.2 | 98.9 | 0.2 | 98.8 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 0.1 | 99.1 | 0.2 | 99.0 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2945 | 0.1 | 99.2 | 0.1 | 99.1 | 0.0345 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3449 | 0.2 | 99.4 | 0.2 | 99.3 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4040 | 0.1 | 99.5 | 0.1 | 99.4 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 0.1 | 99.6 | 0.1 | 99.5 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.1 | 99.6 | 0.1 | 99.6 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 0.1 | 99.8 | 0.1 | 99.7 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 0.0 | 99.8 | 0.1 | 99.8 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 8920 | 0.0 | 99.8 | 0.0 | 99.8 | 0.0209 | 1348 | 1075 | 1021 | 632 | 5745 | 3102 |
| 9649 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0238 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 25149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3132 | 2049 | 1040 | 14909 | 9271 |
| 23004 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4713 | 3695 | 2008 | 1022 | 17473 | 10058 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 511/2 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 0908 7542 | 2820 | 3023 | 32933 35672 | 20494 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |
| | | | | | | | | · · · · • | .= | | 1.1.1.2 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Orac Concernes Verter is produce Concernes | Well Sample | Depth | | | Seacomb 947.60 n | e-7 n | | | | | | |
|---|--------------------------------|-------------|--------------------|------------|------------------------------|----------------------|------------------|----------------------|-------------------|-------------------------|-------------------------|-------------------------|
| Math Jigual Jigual </th <th>Client</th> <th>Geoscience</th> <th>Victoria</th> <th></th> <th>Density C</th> <th>Fradients (psi/foot)</th> <th></th> <th>Conv</th> <th>ersion Paramet</th> <th>ers (dynes/cm)</th> <th>)</th> <th></th> | Client | Geoscience | Victoria | | Density C | Fradients (psi/foot) | | Conv | ersion Paramet | ers (dynes/cm) |) | |
| Ta Mada AbAbesy Cynling Paswer Parker 1997 97.0 340 49.0 193 Sorge 17.0 200 199 199 199 199 199 199 199 199 199 1 | Well | Seacombe-7 | | | Watan | Typical | I ab and any The | | air/water | air/oil | oil/water | CO ₂ /water |
| Image Unit Unit Unit Description 0000 200 200 200 200 | Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | la. | 72.0 | 24.0 | 48.0 | 72.0 |
| Martie Provensities Attice Provensities< | | | | | Gas: | 0.100 | Reservoir Theta | ı | 0.0 | | 30.0 | 0.0 |
| | Sample Denth | 947 60 m | | | CO ₂ Density | 0.246 | Reservoir IFT | sTheta | 50.0 72.0 | 24.0 | 30.0 42.0 | 26.0 |
| Atheno Provestigner Output Temperature junt Tempe | Depth | 947.00 m | | | e og Bensky | 0.240 | Reservoir Tcos | Theta | 50.0 | 24.0 | 26.0 | 26.0 |
| Ambed Property and Pr | Ambient Pern | neability | | | | Estimated Column | Entry P | ressure (psia) | Displacement F | Pressure (psia) | Threshold P | ressure (psia) |
| | Ambient Poro pore radius (u | sity m) | 0.034 | | A-Hg | na | Lab 3091 | Res Con | Lab 3284 | Resv | Lab 3520 | Resv |
| Und 190 200 210 211 213 210 214 230 216 Pessen (max) Implies (max) Concent (max) Concent (max) Pessen (max) Concent (max) Concent (max) <t< th=""><th>F</th><th>)</th><th></th><th></th><th>G-W</th><th>1238</th><th>606</th><th>421</th><th>644</th><th>447</th><th>691</th><th>480</th></t<> | F |) | | | G-W | 1238 | 606 | 421 | 644 | 447 | 691 | 480 |
| L L <thl< th=""> L <thl< th=""> <thl< th=""></thl<></thl<></thl<> | | | | | O-W COs-W | 1991 671 | 202 | 219 | 215 | 233 | 230 | 249 |
| Jac Juli Calibative Control Person Description Injustational Control Description Injustational Control Oillibre Description Control Description Descriptio | | | | | | | | | | | | |
| present List Jik. Control (preced) Present Antities Antities Antities Control (preced) Present Present 101 000 | | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| (prov) (prov)< | Pressure | Intrusion | Data Saturation | Intrusion | ance Corrected Saturation | Pore Diameter | Air/Brine Lab | Air/Brine Res Con | Lab Conditions | Reservoir Conditions | Free Water Oil-Water | Free Water Gas-Water |
| | (psia) | (percent) | (percent) | (percent) | (percent) | (μm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1 0.0 0.0 0.0 211 C.2 0.14 0.12 0.05 0.45 1.94 0.0 0.0 0.0 7.7 0.45 0.37 0.31 0.19 1.75 1.07 1.35 0.0 0.0 0.0 64.7 0.45 0.31 0.01 0.25 2.32 1.15 1.35 0.0 0.0 0.0 0.44 0.66 0.64 0.50 0.31 2.32 1.15 3.18 0.0 | | | | | | | | | | | | |
| 1 8 0.0 | 1.01 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.41 |
| 123 0.0 0.0 0.0 777 0.54 0.37 0.01 0.0< | 1.98 | 0.0 | 0.0 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 1.97 0.0 <td>2.73</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>77.7</td> <td>0.54</td> <td>0.37</td> <td>0.31</td> <td>0.19</td> <td>1.75</td> <td>1.09</td> | 2.73 | 0.0 | 0.0 | 0.0 | 0.0 | 77.7 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 4.8.8 0.0 0.0 0.0 0.0 4.4.4 0.86 0.60 0.59 0.31 2.22 1.76 5.18 0.0 0.0 0.0 0.0 0.0 0.00 | 3.18 | 0.0 | 0.0 | 0.0 | 0.0 | 56.9 | 0.02 | 0.43 | 0.30 | 0.23 | 2.03 | 1.27 |
| 5.18 0.0 0.0 0.0 4.10 1.02 0.71 0.57 0.37 1.34 2.08 5.97 0.0 0.0 0.0 0.25 1.12 0.13 0.06 0.40 0.33 3.32 9.97 0.0 0.0 0.0 0.0 1.55 1.55 1.14 0.71 6.42 3.32 1.15 0.0 0.0 0.0 0.0 1.55 1.55 1.35 0.82 7.44 4.59 1.15 0.0 0.0 0.0 0.0 1.15 3.43 2.22 1.14 1.13 1.19 8.44 1.15 0.0 0.0 0.0 9.33 4.44 2.94 1.41 1.10 1.13 1.13 1.13 1.14 1.14 1.15 1.13 1.13 1.14 1.14 1.14 1.15 1.14 1.15 1.14 1.15 1.14 1.15 1.14 1.15 1.14 1.15 1.15 1.14 | 4.38 | 0.0 | 0.0 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 6.97 0.0 0.0 0.0 204 1.17 0.05 0.00 0.00 4.60 2.33 9.77 0.0 0.0 0.0 0.0 21.3 1.95 1.13 0.14 0.71 6.4 3.32 9.77 0.0 0.0 0.0 0.0 1.57 2.34 1.54 1.03 1.14 1.04 6.74 1.45 1.15 0.0 0.0 0.0 1.57 2.34 2.24 2.47 1.53 1.19 7.41 1.15 0.0 0.0 0.0 0.0 8.39 4.64 2.47 1.53 1.39 8.65 2.53 0.0 0.0 0.0 0.0 3.71 1.12 7.78 6.53 3.32 4.64 3.67 2.29 6.62 0.0 0.0 0.0 3.71 1.12 7.78 6.54 3.32 5.46 9.46 3.64 3.64 3.64 3.64 3.64 3.64 | 5.18 | 0.0 | 0.0 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 8.27 0.0 0.0 0.0 256 1.62 1.13 0.95 3.3 3.3 3.3 9.97 0.0 0.0 0.0 0.0 185 2.23 1.56 1.32 0.08 7.4 4.59 135 0.0 0.0 0.0 1.57 2.6 1.84 1.54 0.08 7.6 4.54 135 0.0 0.0 0.0 9.83 2.44 2.44 2.47 1.53 1.19 7.84 216 0.0 0.0 0.0 9.83 4.46 3.44 2.40 2.13 1.19 7.84 210 0.0 0.0 0.0 7.38 4.08 3.44 2.44 2.44 2.44 1.64 8.63 4.64 3.64 3.64 4.64 8.63 4.64 3.65 3.64 4.64 3.65 3.64 3.65 3.64 3.65 3.64 3.65 3.64 3.64 3.65 3.64 3.65 3 | 6.97 | 0.0 | 0.0 | 0.0 | 0.0 | 30.4 | 1.17 | 0.95 | 0.80 | 0.42 | 4.49 | 2.80 |
| 9.97 0.0 0.0 0.0 12.3 1.95 1.14 0.15 1.42 0.87 7.46 4.29 3.47 115 0.0 0.0 0.0 0.0 1.37 2.36 2.11 1.37 1.14 0.87 7.46 4.24 125 0.0 0.0 0.0 0.0 1.37 2.36 2.212 1.31 1.19 7.47 126 0.0 0.0 0.0 9.33 4.44 2.94 2.47 1.53 1.53 1.54 1.13 1.54 1.53 1.54 1.54 1.54 1.55 1.54 1.00 1.54 1.55 1.54 1.54 1.55 1.54 1.55 1.54 1.55 1.54 1.55 1.54 1.55 1.55 1.54 1.55 1.54 1.55 1.55 1.56 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55 1. | 8.27 | 0.0 | 0.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 113 00 00 00 137 243 134 124 0.09 5.60 5.60 5.60 6.60 6.61 155 00 00 00 00 115 3.63 252 2.12 1.31 11.9 7.41 216 00 00 00 9.33 4.44 2.44 1.44 1.64 1.61 305 00 0.0 0.0 0.0 8.59 4.48 3.44 2.30 1.30 1.64 1.61 305 0.0 0.0 0.0 0.0 4.53 9.18 6.33 4.40 3.42 9.22 1.53 46.2 0.0 0.0 0.0 0.0 3.30 13.0 9.33 7.75 5.65 3.12 9.22 1.54 12.0 1.04 6.44 2.5 2.56 3.15 3.15 1.15 1.15 1.15 3.15 1.15 3.15 1.15 1.15 1.15 1.15 | 9.97 | 0.0 | 0.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 155 0.0 0.0 0.0 13.7 3.04 2.11 1.77 1.10 10.0 6.21 18.5 0.0 0.0 0.0 9.33 4.24 2.24 2.27 1.53 10.9 8.64 21.3 0.0 0.0 0.0 7.68 7.55 5.10 2.20 1.81 1.41 1.10 1.01 0.01 0.01 0.01 0.01 1.01 | 11.5 | 0.0 | 0.0 | 0.0 | 0.0 | 18.5 | 2.25 | 1.84 | 1.52 | 0.82 | 8.66 | 4.39 5.41 |
| 18.5 0.0 0.0 0.0 1.15 3.63 2.52 2.17 1.31 1.19 7.41 21.6 0.0 0.0 0.0 0.0 0.0 1.03 1.19 7.48 32.0 0.0 0.0 0.0 0.0 7.58 5.58 4.46 3.12 1.03 1.12 7.5 0.0 0.0 0.0 4.53 9.18 6.53 4.04 3.52 2.65 6.2 0.0 0.0 0.0 0.0 3.30 1.13 9.03 7.75 4.04 3.55 102 0.0 0.0 0.0 0.0 1.33 1.14 1.04 1.04 3.64 3.55 102 0.0 0.0 0.0 1.44 2.55 1.16 1.14 8.92 60.9 112 0.1 0.2 0.0 0.0 1.14 2.55 1.16 1.16 1.16 1.16 1.17 133 1.14 | 15.5 | 0.0 | 0.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 12.3 0.0 0.0 0.0 8.39 4.66 5.44 2.30 1.60 1.64 1.00 30.0 0.0 0.0 0.0 0.0 2.12 1.93 1.20 37.5 0.0 0.0 0.0 0.0 5.66 7.35 5.10 4.29 2.66 2.42 1.50 64.2 0.0 0.0 0.0 3.31 1.12 7.78 6.53 4.44 3.67 2.23 64.2 0.0 0.0 0.0 0.33 1.14 1.01 1.44 3.64 3.46 4.64 2.64 2.64 7.0 7.00 0.0 0.0 1.33 2.16 1.16 1.64 3.65 3.18 3.18 3.18 3.16 1.16 8.53 3.18 1.16 1.53 1.45 3.14 9.16 8.3.3 3.18 1.16 1.53 1.45 1.16 1.16 1.16 1.16 1.16 1.16 1.16 1.16 | 18.5 | 0.0 | 0.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 300 0.0 0.0 0.0 7.68 5.88 4.08 0.423 2.26 2.24 1.50 46.8 0.0 0.0 0.0 4.33 9.18 6.33 5.35 3.32 3.02 18.83 57.1 0.0 0.0 0.0 3.30 13.4 9.03 7.53 4.69 4.26 2.26 2.45 15.3 91.0 0.0 0.0 0.0 2.33 17.9 1.16 1.44 2.53 17.6 1.48 9.16 8.3 1.51 120 0.1 0.0 0.0 1.44 2.53 17.6 1.48 9.16 8.3 1.51 1210 0.1 0.0 0.0 1.44 2.53 17.5 1.60 9.41 1.61 9.23 1.50 1.28 1.16 7.14 1.08 9.24 1.60 9.41 1212 0.1 0.3 0.0 0.0 1.00 1.00 1.00 1.00 < | 21.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.39 | 4.24 | 3.44 | 2.47 | 1.55 | 16.4 | 10.1 |
| 375 0.0 0.0 0.0 0.0 0.0 3.11 1.13 7.38 5.10 4.29 2.66 3.22 1.85 57.1 0.0 0.0 0.0 0.0 3.71 1.13 7.78 6.53 4.44 3.67 2.29 6.55 4.64 3.67 2.29 6.55 4.64 3.67 2.29 6.55 4.64 3.67 2.29 6.55 4.64 3.67 2.29 6.55 4.64 3.65 3.55 1.6 1.64 2.55 3.55 6.55 3.65 1.64 1.64 2.53 1.76 1.44 9.16 8.3.3 5.18 1.65 8.50 1.88 5.18 1.66 7.21 1.22 0.1 0.0 0.0 0.0 1.44 2.53 2.64 1.76 1.68 8.50 1.88 2.43 1.76 1.68 8.50 1.68 8.50 1.68 8.50 1.68 8.50 1.68 8.50 1.68 8.51 1.61 1.75 3.33 2.54 1.76 1.61 8.55 1.61 8.55 | 30.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| s71 00 00 00 00 112 078 6.53 4.44 36.7 129 66.2 00 0.0 0.0 0.0 0.0 2.70 15.4 10.7 9.00 5.57 50.6 31.5 91.2 0.0 0.0 0.0 0.0 1.33 21.6 15.0 12.4 10.4 6.44 8.55 35.5 110 0.0 0.0 1.44 25.3 17.6 14.8 9.16 8.33 51.8 132 0.1 0.2 0.0 0.0 1.44 25.3 17.6 14.8 9.16 8.33 51.8 132 0.1 0.4 0.0 0.0 1.44 25.3 17.6 33.3 20.6 10.7 16.7 17.4 10.8 9.82 20.7 13.3 20.6 10.7 16.7 17.7 3.3 20.6 10.7 17.7 13.4 20.4 22.9 18.4 11.7 11.7 </td <td>37.5</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>5.66</td> <td>7.35</td> <td>5.10</td> <td>4.29</td> <td>2.66</td> <td>24.2</td> <td>15.0</td> | 37.5 | 0.0 | 0.0 | 0.0 | 0.0 | 5.66 | 7.35 | 5.10 | 4.29 | 2.66 | 24.2 | 15.0 |
| 66.2 0.0 0.0 0.0 0.2 0.1 1.10 9.0 7.58 4.69 4.2.6 3.5.5 91.2 0.0 0.0 0.0 0.0 2.33 1.16 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.6 1.5.0 1.2.0 1.0.0 </td <td>57.1</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>3.71</td> <td>11.2</td> <td>7.78</td> <td>6.53</td> <td>4.04</td> <td>36.7</td> <td>22.9</td> | 57.1 | 0.0 | 0.0 | 0.0 | 0.0 | 3.71 | 11.2 | 7.78 | 6.53 | 4.04 | 36.7 | 22.9 |
| 78.6 0.0 0.0 0.0 0.0 0.2 17.9 12.4 10.4 6.44 88.5 3.6.5 110 0.0 0.1 0.0 0.0 1.93 21.6 15.6 14.4 81.6 88.3 3.6.3 112 0.1 0.3 0.0 0.0 1.140 23.8 17.6 14.4 81.6 83.3 3.1.8 112 0.1 0.3 0.0 0.0 1.140 23.8 20.6 12.8 91.6 6.9 212 0.1 0.4 0.0 0.0 0.544 48.6 33.8 28.4 17.6 160 99.4 221 0.1 0.5 0.1 0.1 0.617 67.5 46.9 39.4 24.4 222 18.8 402 0.1 0.7 0.3 0.447 92.9 64.5 54.2 33.6 30.5 123.5 442 0.1 0.4 0.3 0.447 92.9 <td>66.2</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>3.20</td> <td>13.0</td> <td>9.03</td> <td>7.58</td> <td>4.69</td> <td>42.6</td> <td>26.6</td> | 66.2 | 0.0 | 0.0 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.58 | 4.69 | 42.6 | 26.6 |
| 10 00 00 1-33 116 150 128 930 780 741 129 0.1 0.2 0.0 0.0 1.40 298 20.7 174 10.8 98.2 60.9 180 0.1 0.3 0.0 0.0 1.40 29.8 20.7 174 10.8 98.2 60.9 212 0.1 0.4 0.0 0.0 4.46 28.9 24.3 15.0 13.6 85.0 218 0.1 0.5 0.1 0.1 0.729 77.1 39.7 33.3 20.6 187 117 344 0.1 0.5 0.1 0.1 0.647 29.9 64.3 54.2 33.6 30.5 190 35.5 0.1 0.8 0.1 0.4 0.322 197 78.0 3.5 33.3 37.7 22.9 74.1 55.9 40.0 303 38.8 1.1 1.0 0.4 0.32.9 | 78.6 | 0.0 | 0.0 | 0.0 | 0.0 | 2.70 | 15.4 | 10.7 | 9.00 | 5.57 | 50.6 | 31.5 |
| 129 0.1 0.0 0.0 1.64 253 1.76 1.48 9.16 83.3 51.8 152 0.1 0.3 0.0 0.0 1.17 35.3 24.5 20.6 12.8 11.6 72.1 212 0.1 0.5 0.1 0.0 0.854 48.6 33.8 28.4 17.6 16.0 19.7 344 0.1 0.5 0.1 0.1 0.617 77.5 46.9 39.4 24.4 22.2 138 402 0.1 0.5 0.1 0.3 0.477 72.9 64.5 54.2 33.6 355 190 555 0.1 0.8 0.1 0.4 0.322 11.9 81.2 1.5 33.3 357 229 643 0.1 0.4 0.477 14.8 13.4 10.0 71.4 45.9 401 259 644 0.1 0.1 0.6 0.279 14.8 | 110 | 0.0 | 0.0 | 0.0 | 0.0 | 1.93 | 21.6 | 15.0 | 12.6 | 7.80 | 70.9 | 44.1 |
| 152 0.1 0.2 0.0 0.0 1.40 29.83 20.7 17.4 10.8 98.2 60.9 180 0.1 0.3 0.0 0.0 1.00 41.6 23.9 24.3 15.0 13.6 85.0 248 0.1 0.4 0.0 0.0854 44.6 23.3 22.44 17.6 160 97.4 241 0.1 0.5 0.1 0.1 0.627 73.8 54.7 46.0 22.5 25.9 161 442 0.1 0.6 0.1 0.2 0.527 78.8 54.7 46.0 22.5 25.9 161 55 0.1 0.8 0.1 0.4 0.327 197 85.2 47.5 45.9 490 90.9 33.3 37.7 22.9 648 0.1 0.1 0.4 0.202 1.4 16.7 141 87.3 784 491 128 0.2 1.5 0.2 1.4 0.173 241 167 141 87.3 794 491 </td <td>129</td> <td>0.1</td> <td>0.1</td> <td>0.0</td> <td>0.0</td> <td>1.64</td> <td>25.3</td> <td>17.6</td> <td>14.8</td> <td>9.16</td> <td>83.3</td> <td>51.8</td> | 129 | 0.1 | 0.1 | 0.0 | 0.0 | 1.64 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 121 0.0 0.0 1.00 1.46 229 2.43 1.50 1.85 85.0 248 0.1 0.5 0.1 0.1 0.729 57.1 337 33.3 2.06 187 117 344 0.1 0.5 0.1 0.1 0.6 77.5 46.9 39.4 2.44 222 13 402 0.1 0.6 0.1 0.2 0.527 78.8 54.7 46.0 2.85 2.36 305 161 474 0.1 0.7 0.1 0.3 0.44 0.322 17.8 54.4 1.42 54.2 3.36 305 190 555 0.1 0.8 0.1 0.6 0.279 149 103 87.1 53.9 33.3 357 223 648 0.1 1.0 0.1 0.6 0.279 149 103 17.3 474 421 1228 0.1 0.1 0.17 | 152 | 0.1 | 0.2 | 0.0 | 0.0 | 1.40 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 72.1 |
| 248 0.1 0.4 0.0 0.84 446 338 284 176 100 99.4 291 0.1 0.5 0.1 0.1 0.617 67.5 469 39.4 24.4 222 138 442 0.1 0.6 0.1 0.2 0.527 78.8 54.7 46.0 28.5 259 161 444 0.1 0.7 0.1 0.3 0.447 92.9 64.5 54.2 33.6 305 1990 555 0.1 0.8 0.1 0.4 0.3327 127 88.2 74.2 45.9 417 259 761 0.1 1.0 0.1 0.7 0.292 206 143 102 7.3 675 421 128 0.2 1.4 0.173 241 167 141 87.3 794 491 1489 0.2 2.2 0.2 1.8 0.16 358 249 | 212 | 0.1 | 0.3 | 0.0 | 0.0 | 1.00 | 41.6 | 24.5 | 24.3 | 15.0 | 136 | 85.0 |
| 291 0.1 0.5 0.1 0.1 0.729 57.1 39.7 33.3 20.6 187 117 344 0.1 0.6 0.1 0.2 0.527 78.8 54.7 46.0 28.5 259 161 474 0.1 0.7 0.1 0.3 0.477 97.7 65.5 39.3 357 223 648 0.1 0.9 0.1 0.6 0.372 129 78.2 74.2 45.9 417 229 761 0.1 1.0 0.1 0.6 0.279 149 103 87.1 53.9 490 303 888 0.1 1.1 0.1 0.6 0.22 206 143 120 74.3 675 421 1228 0.2 1.8 0.147 282 196 165 102 92 757 57 1428 0.2 0.2 0.1 1.0 137 230 | 248 | 0.1 | 0.4 | 0.0 | 0.0 | 0.854 | 48.6 | 33.8 | 28.4 | 17.6 | 160 | 99.4 |
| | 291 344 | 0.1 | 0.5 | 0.1 | 0.1 | 0.729 | 57.1 67.5 | 39.7 | 33.3 39.4 | 20.6 24.4 | 187 | 117 |
| 474 0.1 0.7 0.1 0.3 0.447 92.9 64.5 54.2 33.6 305 190 555 0.1 0.8 0.1 0.5 0.327 127 88.2 74.2 45.9 41.7 229 648 0.1 1.0 0.1 0.6 0.27 127 88.2 74.2 45.9 44.9 303 888 0.1 1.1 0.1 0.7 0.239 174 121 102 63.1 574 436 1049 0.2 1.5 0.2 1.1 0.173 241 167 141 87.3 794 491 1439 0.2 1.5 0.2 1.4 0.173 241 167 141 87.3 794 491 1439 0.2 1.4 0.17 126 331 230 193 119 1082 676 1828 0.2 0.2 0.3 1.7 0.126 331 337 209 1090 1179 2444 1.4 3. | 402 | 0.1 | 0.6 | 0.1 | 0.2 | 0.527 | 78.8 | 54.7 | 46.0 | 28.5 | 259 | 161 |
| 5530.10.80.10.40.82109 (5.7) 63.399.33571236480.11.00.10.60.27914910387.153.944033610490.21.30.20.90.20220614312074.367542112280.21.50.21.10.17324116714187.379449114390.21.80.21.40.14728219616510292757616870.32.00.31.70.126331230193119108267618280.22.20.21.80.116358249209129117373221420.42.70.42.30.0990420292245152188285925080.63.20.62.90.08454423423471618100629441.14.31.14.00.07205774013372091900117934482.87.12.86.80.06156.764693952452227137940452.3.130.22.5.75.5.70.044410046975863633000205040449.170.89.270.70.0331.77187676425336 <td< td=""><td>474</td><td>0.1</td><td>0.7</td><td>0.1</td><td>0.3</td><td>0.447</td><td>92.9</td><td>64.5</td><td>54.2</td><td>33.6</td><td>305</td><td>190</td></td<> | 474 | 0.1 | 0.7 | 0.1 | 0.3 | 0.447 | 92.9 | 64.5 | 54.2 | 33.6 | 305 | 190 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 555 648 | 0.1 | 0.8 | 0.1 | 0.4 | 0.382 | 109 | 75.7 88.2 | 63.5 74.2 | 39.3 45.9 | 357 417 | 223 |
| 888 0.1 1.1 0.1 0.7 0.239 174 121 102 63.1 574 356 1049 0.2 1.3 0.2 0.4 0.173 241 167 141 87.3 794 491 1439 0.2 1.8 0.2 1.4 0.147 282 196 165 102 927 576 1687 0.3 2.0 0.3 1.7 0.126 331 230 193 119 1082 676 1888 0.2 2.2 0.2 1.8 0.116 358 249 209 129 1173 752 2142 0.4 2.7 0.4 2.3 00990 420 242 287 178 1618 1006 2244 1.1 1.3 1.1 4.0 0.0720 577 401 337 209 100 1179 3448 2.8 7.1 2.8 6.8 0.64 542 336 3055 1894 512 5.5 0.0524< | 761 | 0.1 | 1.0 | 0.1 | 0.6 | 0.279 | 149 | 103 | 87.1 | 53.9 | 490 | 303 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 888 | 0.1 | 1.1 | 0.1 | 0.7 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | 1228 | 0.2 | 1.5 | 0.2 | 1.1 | 0.173 | 200 | 143 | 120 | 87.3 | 794 | 421 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 1439 | 0.2 | 1.8 | 0.2 | 1.4 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 1687 | 0.3 | 2.0 | 0.3 | 1.7 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 722 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 2142 | 0.2 | 2.2 | 0.2 | 2.3 | 0.0990 | 420 | 249 292 | 209 | 129 | 1382 | 859 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 2508 | 0.6 | 3.2 | 0.6 | 2.9 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 4045 23.1 30.2 23.2 29.9 0.0524 793 551 463 287 2609 1621 4734 25.6 55.8 25.7 55.7 0.0448 928 644 542 336 3055 1894 5122 5.9 61.7 75.86 3300 2055 1894 6004 9.1 70.8 9.2 70.7 0.0353 1177 817 687 425 3864 2403 7033 6.7 77.5 6.7 77.4 0.0301 1379 958 805 498 4527 2818 7897 3.9 81.4 4.0 84.7 0.0237 1750 1215 1022 633 5755 3574 9662 2.0 86.5 1.7 88.5 0.0233 2052 1425 1198 742 6745 4191 10465 1.7 88.5 1.7 0.0172 2411 1674 407 871 7918 4924 14346 2.6 94.3 0.0148 2813 1953 1642 1016 9236 5744 16397 2.1 96.4 2.1 96.4 0.0129 3215 2233 1876 1161 10555 6568 18446 1.6 98.0 1.6 98.6 0.0015 3627 2519 2117 1311 11918 7499 20495 0.6 99.5 0.0092 4540 | 2944 3448 | 1.1 | 4.3 | 1.1 | 4.0 | 0.0720 | 577 | 401 | 337 | 209 | 1900 2227 | 1179 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 4045 | 23.1 | 30.2 | 23.2 | 29.9 | 0.0524 | 793 | 551 | 463 | 287 | 2609 | 1621 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 4734 | 25.6 | 55.8 | 25.7 | 55.7 | 0.0448 | 928 | 644 | 542 | 336 | 3055 | 1894 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 6004 | 5.9 9.1 | 70.8 | 5.9 9.2 | 61.5 70.7 | 0.0414 | 1004 | 817 | 586 687 | 363 425 | 3300 | 2050 |
| 7897 3.9 81.4 4.0 81.4 0.0268 1548 1075 904 560 5091 31674 8927 3.4 84.8 3.4 84.7 0.0237 1750 1215 1022 633 5755 3574 9662 2.0 86.8 2.0 86.7 0.0219 1895 1316 1106 685 6227 8711 10465 1.7 88.5 1.7 88.5 0.0203 2052 1425 1198 742 6745 41911 12296 3.2 91.7 3.2 91.7 0.0172 2411 1674 1407 871 7918 4924 14346 2.6 94.3 0.0148 2813 1953 1642 1016 9236 5744 16397 2.1 96.4 0.0129 3215 2233 1876 1161 10555 6568 18496 1.6 98.0 0.0115 3627 2519 2117 1311 11918 7409 20495 0.8 98.8 0.0092 4540 3153 2650 1640 14909 9274 25069 0.2 99.7 0.0078 5322 3966 3106 1923 17482 10871 29174 0.2 99.7 0.0077 5761 4001 3362 2081 18918 11768 31806 0.0 100.0 0.0077 7576 4688 3940 2233 | 7033 | 6.7 | 77.5 | 6.7 | 77.4 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 892/ 3.4 84.8 3.4 84.7 0.023 17.50 1215 1022 633 5753 3574 9662 2.0 86.8 2.0 86.7 0.0219 1895 1316 1106 685 6227 3871 10465 1.7 88.5 1.7 88.5 0.0203 2052 1425 1198 742 6745 4191 12266 3.2 91.7 3.2 91.7 0.0172 2411 1674 1407 871 7918 4924 16397 2.1 96.4 0.0129 3215 2233 1876 1161 10555 6568 18496 1.6 98.0 0.013 4019 2791 2345 1452 13200 8209 20495 0.8 98.8 0.0003 4019 2791 2345 1452 13200 8209 23155 0.6 99.5 0.6 99.5 0.0092 4540 3153 | 7897 | 3.9 | 81.4 | 4.0 | 81.4 | 0.0268 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 8927 9662 | 2.0 | 84.8 86.8 | 3.4 2.0 | 84.7 86.7 | 0.0237 | 1/50 | 1215 | 11022 | 685 | 6227 | 3871 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 10465 | 1.7 | 88.5 | 1.7 | 88.5 | 0.0203 | 2052 | 1425 | 1198 | 742 | 6745 | 4191 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 12296 | 3.2 | 91.7 | 3.2 | 91.7 | 0.0172 | 2411 | 1674 | 1407 | 871 | 7918 | 4924 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 16397 | 2.6 | 94.5 96.4 | 2.6 | 94.3 96.4 | 0.0148 | 3215 | 2233 | 1842 | 1161 | 10555 | 5744 6568 |
| 20495 0.8 98.8 0.8 98.8 0.0092 4540 3153 2650 1452 13200 8209 23155 0.6 99.5 0.6 99.5 0.0092 4540 3153 2650 1640 14909 9274 25069 0.2 99.7 0.2 99.7 0.0085 4915 31413 2869 1776 16145 10038 27141 0.2 99.9 0.2 99.9 0.0072 5761 4001 3362 2081 18918 11768 31806 0.0 100.0 0.0 0.0067 6236 4331 3640 2253 20482 12738 34424 0.0 100.0 0.0062 6750 4688 3940 2439 22173 13788 37194 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0040 0.0049 8548 | 18496 | 1.6 | 98.0 | 1.6 | 98.0 | 0.0115 | 3627 | 2519 | 2117 | 1311 | 11918 | 7409 |
| 2102 0.0 27.3 0.00 27.3 0.002 49.40 5153 2650 1640 14909 92/2 2506 0.2 99.7 0.2 99.7 0.0085 4915 3413 2869 1776 16145 10038 27141 0.2 99.9 0.2 99.9 0.0078 5322 3696 3106 1923 17482 10871 29379 0.1 100.0 0.1 100.0 0.0072 5761 4001 3362 2081 18918 11768 31806 0.0 100.0 0.0 0.0067 6236 4331 3640 2253 20482 12738 34424 0.0 100.0 0.0062 6750 4688 3940 2439 22173 13788 37194 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 0.0049 8548 | 20495 | 0.8 | 98.8 | 0.8 | 98.8 | 0.0103 | 4019 | 2791 | 2345 | 1452 | 13200 | 8209 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 25155 | 0.6 | 99.5 99.7 | 0.6 | 99.5 99.7 | 0.0092 | 4540 | 3413 | 2850 | 1040 | 14909 | 9274 10038 |
| 29379 0.1 100.0 0.1 100.0 0.0072 5761 4001 3362 2081 18918 11768 31806 0.0 100.0 0.0 100.0 0.0067 6236 4331 3640 2253 20482 12738 34424 0.0 100.0 0.0062 6750 4688 3940 2439 22173 13788 37194 0.0 100.0 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 0.0049 8548 5936 4989 3088 28073 17459 47294 0.0 100.0 0.0045 9273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0041 10033 6967 5856< | 27141 | 0.2 | 99.9 | 0.2 | 99.9 | 0.0078 | 5322 | 3696 | 3106 | 1923 | 17482 | 10871 |
| 5 1000 0.0 100.0 0.0 100.0 0.00 62.50 43.51 3640 2253 20482 127.88 34424 0.0 100.0 0.0 100.0 0.0062 6750 4688 3940 2439 22173 13788 37194 0.0 100.0 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 43346 0.0 100.0 0.0 0.0049 8548 5936 4989 3088 28073 17459 47294 0.0 100.0 0.0 0.0045 9273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0041 10033 6967 5856 3625 32955 20491 55385 0.0 100.0 0.0035 117 | 29379 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0072 | 5761 | 4001 | 3362 | 2081 | 18918 | 11768 |
| 37194 0.0 100.0 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 100.0 0.0057 7293 5065 4257 2635 23955 14897 40344 0.0 100.0 0.0 100.0 0.0053 7911 5494 4617 2858 25982 16159 43596 0.0 100.0 0.0 0.0049 8548 5936 4989 3088 28073 17459 47294 0.0 100.0 0.0 0.0045 9273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0041 10033 6967 5856 3625 32955 20491 55385 0.0 100.0 0.0035 11740 8153 6852 4742 38564 23975 2182 59876 0.0 100.0 0.0035 11740 815 | 34424 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6750 | 4551 4688 | 3040 3940 | 2233 | 20482 22173 | 12758 |
| 40344 0.0 100.0 0.0 100.0 0.0053 7911 5494 4617 2858 25982 16159 43596 0.0 100.0 0.0 100.0 0.0049 8548 5936 4989 3088 28073 17459 47294 0.0 100.0 0.0 100.0 0.0045 9273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0 0.0041 10033 6967 5856 3625 32955 20491 55385 0.0 100.0 0.0 100.0 0.0035 11740 8153 6852 4742 38543 23854 59876 0.0 100.0 0.0035 11740 8153 6852 4742 38543 23854 | 37194 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14897 |
| 47294 0.0 100.0 0.0 100.0 0.0045 \$273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0 0.0045 \$273 6440 5412 3350 30455 18941 51169 0.0 100.0 0.0 0.0041 10033 6967 5856 3625 32955 20491 55385 0.0 100.0 0.0 0.0035 11740 8153 6852 4742 38564 23975 2182 | 40344 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7911 | 5494 | 4617 | 2858 | 25982 | 16159 |
| 51169 0.0 100.0 0.0041 10033 6967 5856 3625 32955 20491 55385 0.0 100.0 0.0 100.0 0.0038 10860 7542 6338 3924 35673 22182 59876 0.0 100.0 0.0035 11740 8153 6852 4242 38564 23979 | 45596 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8548 9273 | 5936 6440 | 4989 5412 | 3088 | 28073 | 17459 |
| 55385 0.0 100.0 0.0038 10860 7542 6338 3924 35673 22182 59876 0.0 100.0 0.0035 11740 8153 6852 4242 38564 23979 | 51169 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10033 | 6967 | 5856 | 3625 | 32955 | 20491 |
| | 55385 59876 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 11740 | 7542 | 6338 6852 | 3924 4242 | 35673 38564 | 22182 |

 55385
 0.0
 100.0
 0.0
 100.0

 59876
 0.0
 100.0
 0.0
 100.0

 (A) Interpreted Capillary Pressure Chart



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

WellSole-1Sample Depth805.9 m



| Client Geoscience AVictoria Density Gradients (psi/foot) Conversion Parameters (dynes/cm) Well Sole-1 Typical air/water air/oil oil/wa | | | | | | | | | | | |
|--|-------------|------------------|------------|--------------------|------------------|-----------------|---------------------|----------------|----------------|--------------|------------------------|
| Well | Sole-1 | in victoria | | Density G | Typical | | Conv | air/water | air/oil | oil/water | CO ₂ /water |
| en | 5010 1 | | | Water: | 0.440 | Laboratory Thet | a | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Pressu | ire | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| | | | | Gas: | 0.100 | Reservoir Theta | | 0.0 | | 30.0 | 0.0 |
| Sample | S1 | | | | | Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 805.90 m | | | CO2 Density | 0.259 | Laboratory Tcos | Theta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir TcosT | heta | 50.0 | | 26.0 | 26.0 |
| | , | 0.405 | | | Estimated Column | Entry P | ressure (psia) | Displacement F | ressure (psia) | Threshold P | ressure (psia) |
| Pore radius (µ | .m) | 0.405 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv |
| | | | | C W | 105 | 203 | - 25.8 | 102 | - 70.8 | 131 | - 8 00 |
| | | | | 0-W | 169 | 17.2 | 18.6 | 34.0 | 36.8 | 43.6 | 47.2 |
| | | | | CO ₂ -W | 58 | 51.6 | 18.6 | 102 | 36.8 | 131 | 47.2 |
| | | | | | •• | | | | | | |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| | Rav | v Data | Conforma | ince Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 2.7 | 2.7 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 1.3 | 4.1 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.6 | 4.0 | 0.0 | 0.0 | 56.0 | 0.62 | 0.43 | 0.30 | 0.23 | 2.03 | 1.27 |
| 4 38 | 0.7 | 61 | 0.0 | 0.0 | 48.4 | 0.86 | 0.51 | 0.45 | 0.20 | 2.40 | 1.49 |
| 5.18 | 0.7 | 6.7 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.6 | 7.3 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.8 | 8.1 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.9 | 9.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.8 | 9.8 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.5 | 10.3 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.8 | 11.1 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 18.5 | 0.0 | 12.5 | 0.0 | 0.0 | 11.7 | 3.63 | 2.11 | 2.12 | 1.10 | 11.9 | 7.41 |
| 21.6 | 0.8 | 13.3 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.6 | 13.8 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.4 | 14.3 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.1 | 14.4 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.2 | 14.5 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 56.6 | 0.2 | 14./ | 0.0 | 0.0 | 3.75 | 11.1 | /./1 | 6.48 7.50 | 4.01 | 30.5 | 22.7 |
| 80.4 | 0.4 | 15.1 | 0.0 | 0.0 | 2.64 | 15.0 | 9.05 | 9.20 | 4.70 | 42.7 | 20.0 |
| 93.0 | 0.6 | 16.3 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.6 | 16.9 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.6 | 17.5 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.7 | 18.2 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 179 | 0.8 | 18.9 | 0.0 | 0.0 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 | 0.8 | 19.7 | 0.0 | 0.0 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.9 | 20.6 | 0.0 | 0.0 | 0.860 | 48.4 | 33.0 | 28.5 | 20.7 | 139 | 98.8 |
| 343 | 1.1 | 23.0 | 1.6 | 1.6 | 0.720 | 67.3 | 46.7 | 39.3 | 20.7 | 221 | 137 |
| 401 | 1.5 | 24.5 | 1.9 | 3.5 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 1.8 | 26.3 | 2.3 | 5.8 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 2.2 | 28.4 | 2.8 | 8.6 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 | 2.7 | 31.1 | 3.4 | 12.0 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| 757 | 3.2 | 34.3 | 4.1 | 16.1 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 1048 | 5.7 | 38.0 42.4 | 4.7 | 20.8 | 0.239 | 205 | 121 | 102 | 74.3 | 574 | 330 418 |
| 1227 | 47 | 47.1 | 6.0 | 32.4 | 0.173 | 203 | 142 | 140 | 86.7 | 788 | 491 |
| 1439 | 5.3 | 52.4 | 6.8 | 39.2 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 5.9 | 58.3 | 7.5 | 46.7 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 3.0 | 61.3 | 3.9 | 50.6 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 5.8 | 67.2 | 7.5 | 58.0 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 5.4 | 72.5 | 6.8 | 64.9 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | 4./ | //.2 81.2 | 5.0 5.0 | 70.9 | 0.0720 | 577 | 401 | 337 395 | 209 | 1900 2227 | 11/9 |
| 4040 | 3.3 | 84.5 | 4.2 | 80 2 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 3.7 | 88.2 | 4.7 | 84.9 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 1.2 | 89.4 | 1.5 | 86.4 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 2.2 | 91.5 | 2.8 | 89.2 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 1.9 | 93.5 | 2.5 | 91.7 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 7895 | 1.4 | 94.8 | 1.7 | 93.4 | 0.0269 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| 8920 | 1.4 | 96.2 | 1.8 | 95.2 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 35/4 |
| 10452 | 0.9 | 97.1 | 1.1 | 96.5 | 0.0220 | 2049 | 1314 | 1104 | 740 | 6209 | 3803 4185 |
| 12283 | 1.2 | 99.2 | 1.6 | 99.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.6 | 99.8 | 0.8 | 99.7 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.2 | 100.0 | 0.3 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 25149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 23064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | ∠808 3105 | 1//5 | 10130 | 10038 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5760 | 4000 | 3362 | 2081 | 1/4/5 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 | 4687 | 3939 | 2438 | 22164 | 13785 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 511/2 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 0908 | 2826 | 3025 | 32933 | 20494 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |
| | | | | V | | | | | | | · · · · · · |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well Sample | Depth | | | Sperm Wł 653.8 m | nale Head-1 | | | | | | |
|----------------|--------------|-----------------|-----------|---------------------|---------------------|----------------------------------|------------------|-----------------|-----------------|----------------|------------------------|
| Client | Geoscience | Victoria | | Density G | radients (nsi/foot) | 1 | Con | version Paramet | ers (dynes/cm) | | |
| Well | Sperm What | e Head-1 | | Density G | Typical | | Con | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | SWH1-1 | | | Gas: | 0.100 | Reservoir Theta Reservoir IFT | | 50.0 | | 30.0 | 26.0 |
| Depth | 653.80 m | | | CO2 Density | 0.165 | Laboratory Tcos | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| | | | | - | Estimated Column | Entry I | ressure (psia) | Displacement I | Pressure (psia) | Threshold P | ressure (psia) |
| Pore radius (µ | .m) | 0.056 | | System | Height (feet) | Lab | Res Con | Lab 2157 | Resv | Lab 2220 | Resv |
| | | | | G-W | 756 | 370 | 257 | 423 | 294 | 437 | 304 |
| | | | | O-W | 1215 | 123 | 134 | 141 | 153 | 146 | 158 |
| | | | | CO ₂ -W | 370 | 370 | 134 | 423 | 153 | 437 | 158 |
| | | | | | | Eminut | Iniantian Damana | Oil/Dain a | O:1/Daina | II | II.:-b4 Ab |
| | Raw | / Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine | Lab | Reservoir | Free Water | Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.0 | 0.0 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 2.0 | 2.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.7 | 2.6 | 0.0 | 0.0 | 66.7 56.9 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 4.38 | 0.4 | 3.4 | 0.0 | 0.0 | 48.4 | 0.75 | 0.60 | 0.43 | 0.20 | 2.40 | 1.49 |
| 5.18 | 0.4 | 3.8 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.3 | 4.1 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.3 | 4.4 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 9.97 | 0.3 | 4.7 5.0 | 0.0 | 0.0 | 21.3 | 1.02 | 1.15 | 1 14 | 0.59 | 5.55 6.42 | 3.52 3.97 |
| 11.5 | 0.5 | 5.5 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.3 | 5.8 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.3 | 6.1 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 21.6 | 0.3 | 6.4 | 0.0 | 0.0 | 9.83 | 4 24 | 2.52 | 2.12 | 1.51 | 13.9 | 8 65 |
| 25.3 | 0.3 | 7.1 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.4 | 7.5 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.5 | 8.0 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.1 | 8.1 8.2 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 7.71 | 5.40 6.48 | 5.54 4.01 | 30.4 | 18.9 |
| 66.3 | 0.1 | 8.4 | 0.0 | 0.0 | 3.20 | 13.0 | 9.03 | 7.59 | 4.70 | 42.7 | 26.6 |
| 80.4 | 0.2 | 8.5 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 0.2 | 8.8 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.2 | 9.0 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 152 | 0.2 | 9.5 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 179 | 0.3 | 9.7 | 0.0 | 0.0 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 | 0.3 | 10.0 | 0.0 | 0.0 | 1.01 | 41.2 | 28.6 | 24.0 | 14.9 | 135 | 84.1 |
| 247 | 0.3 | 10.3 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 343 | 0.3 | 10.0 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 20.7 | 221 | 137 |
| 401 | 0.4 | 11.3 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 0.4 | 11.6 | 0.0 | 0.0 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.4 | 12.0 | 0.0 | 0.0 | 0.383 | 108 | 75.0 | 63.3 74.0 | 39.2 | 356 | 221 |
| 757 | 0.5 | 12.4 | 0.0 | 0.0 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 887 | 0.6 | 13.5 | 0.0 | 0.0 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 0.7 | 14.2 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 0.9 | 15.0 | 0.0 | 0.0 | 0.173 | 241 | 167 | 140 | 86.7 | /88 | 491 |
| 1688 | 1.4 | 17.4 | 1.6 | 1.6 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 2.3 | 19.7 | 2.7 | 4.4 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 2.2 | 22.0 | 2.7 | 7.0 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 22.2 54 8 | 44.2 99.0 | 26.5 | 55.5 98.8 | 0.0845 | 492 | 342 401 | 287 | 1/8 | 1900 | 1006 |
| 3449 | 0.8 | 99.8 | 0.9 | 99.7 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4040 | 0.0 | 99.8 | 0.0 | 99.7 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 0.0 | 99.8 | 0.0 | 99.7 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.0 | 99.8 99.8 | 0.0 | 99.7 99.7 | 0.0415 | 1003 | 697 817 | 585 687 | 362 425 | 3291 | 2050 |
| 7033 | 0.0 | 99.8 | 0.1 | 99.8 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 7895 | 0.0 | 99.8 | 0.0 | 99.8 | 0.0269 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| 8920 | 0.1 | 99.9 | 0.1 | 99.9 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |
| 10452 | 0.0 | 99.9 100.0 | 0.0 | 99.9 100.0 | 0.0220 | 2049 | 1314 | 1104 | 683 740 | 6209 | 3865 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 | 3624 4016 | 2517 | 2115 | 1309 | 11900 | 7403 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 6749 | 4331 4687 | 3939 | 2438 | 20482 | 12/38 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47291 51172 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 10034 | 6440 6968 | 5412 5856 | 3350 | 30455 32955 | 18941 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |

Sperm Whale Head-1





⁽B) Capillary Pressure Plot



| Well Sample | Depth | | | 5perm Wl 718.10 m | hale Head-1 า | | | | | | |
|--------------------------------|----------------|-----------------|-----------|---------------------------|---------------------|-------------------------|---------------------|----------------|------------------------|----------------------------|----------------------------|
| Client | Geoscience | Victoria | | Density G | radients (psi/foot) | | Conv | ersion Paramet | ers (dvnes/cm) | | |
| Well | Sperm Whal | e Head-1 | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| Test Method | Air/Mercury | Capillary Press | aure | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 48.0 | 0.0 72.0 |
| rest witchiou | 7 mi/ wiereury | cupiliary ries. | Juic | Gas: | 0.100 | Reservoir Theta | 1 | 0.0 | 24.0 | 30.0 | 0.0 |
| Sample | 2 | | | CO. Density | 0.199 | Reservoir IFT | -Th -t- | 50.0 | 24.0 | 30.0 | 26.0 |
| Depth | /18.10 m | | | CO ₂ Density | 0.188 | Reservoir Tcos | Theta | 50.0 | 24.0 | 26.0 | 26.0 |
| Ambient Pern | neability | | | | Estimated Column | Entry F | Pressure (psia) | Displacement I | ressure (psia) | Threshold P | ressure (psia) |
| Ambient Poro pore radius (u | sity m) | 0.041 | | A-Hg | na na | Lab 2591 | Res Con | Lab 2794 | Resv - | Lab 3241 | Resv |
| F (1 |) | | | G-W | 1038 | 508 | 353 | 548 | 381 | 636 | 442 |
| | | | | O-W CO ₂ -W | 1669 522 | 169 508 | 184 | 183 548 | 198 198 | 212 636 | 230 230 |
| | | | | | L | | • | | | | |
| | Raw | Data | Conforms | ance Corrected | Pore | Equivalent Air/Brine | Injection Pressures | Oil/Brine | Oil/Brine Reservoir | Height Above Free Water | Height Above Free Water |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1.01 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.41 |
| 1.98 | 0.6 | 0.6 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 3.18 | 0.1 | 1.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.09 |
| 3.73 | 0.2 | 1.2 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 4.38 | 0.1 | 1.3 | 0.0 | 0.0 | 48.4 41.0 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 2.08 |
| 5.97 | 0.1 | 1.6 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 8.27 | 0.2 | 1.8 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 9.97 | 0.2 | 2.0 | 0.0 | 0.0 | 23.6 | 1.62 | 1.13 | 1.14 | 0.39 | 5.55 6.42 | 3.52 |
| 11.5 | 0.2 | 2.4 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.2 | 2.6 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 10.0 | 5.41 |
| 18.5 | 0.2 | 3.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.2 | 3.2 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 30.0 | 0.2 | 3.4 | 0.0 | 0.0 | 7.08 | 4.96 | 4.08 | 3.43 | 2.12 | 16.4 | 10.1 |
| 37.3 | 0.0 | 3.7 | 0.0 | 0.0 | 5.68 | 7.31 | 5.08 | 4.27 | 2.64 | 24.0 | 14.9 |
| 46.7 56.9 | 0.0 | 3.7 | 0.0 | 0.0 | 4.54 | 9.16 11.2 | 6.36 7.78 | 5.34 6.51 | 3.31 | 30.1 36.6 | 18.7 22.9 |
| 66.1 | 0.1 | 3.8 | 0.0 | 0.0 | 3.21 | 13.0 | 9.03 | 7.56 | 4.68 | 42.5 | 26.6 |
| 78.5 | 0.1 | 4.0 | 0.0 | 0.0 | 2.70 | 15.4 | 10.7 | 8.98 | 5.56 | 50.5 | 31.5 |
| 110 | 0.2 | 4.1 | 0.0 | 0.0 | 1.93 | 21.6 | 12.4 | 10.4 | 7.80 | 70.9 | 44.1 |
| 129 | 0.2 | 4.4 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.2 | 4.6 | 0.0 | 0.0 | 1.40 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 116 | 60.9 72.1 |
| 212 | 0.2 | 5.0 | 0.0 | 0.0 | 1.00 | 41.6 | 28.9 | 24.3 | 15.0 | 136 | 85.0 |
| 248 | 0.2 | 5.2 | 0.0 | 0.0 | 0.855 | 48.6 | 33.8 | 28.4 | 17.6 | 160 | 99.4 |
| 291 343 | 0.2 | 5.4 5.6 | 0.0 | 0.0 | 0.729 | 57.1 67.3 | 39.7 46.7 | 35.3 39.3 | 20.6 | 221 | 117 |
| 402 | 0.3 | 5.9 | 0.0 | 0.0 | 0.527 | 78.8 | 54.7 | 46.0 | 28.5 | 259 | 161 |
| 474 | 0.3 | 6.2 | 0.0 | 0.0 | 0.448 | 92.9 109 | 64.5 75.7 | 54.2 63.4 | 33.6 39.2 | 305 356 | 190 223 |
| 648 | 0.4 | 7.0 | 0.0 | 0.0 | 0.327 | 127 | 88.2 | 74.2 | 45.9 | 417 | 259 |
| 760 | 0.5 | 7.5 | 0.0 | 0.0 | 0.279 | 149 | 103 | 87.0 | 53.9 | 490 | 303 |
| 1049 | 0.5 | 8.0 | 0.0 | 0.0 | 0.239 | 206 | 121 | 102 | 74.3 | 675 | 421 |
| 1228 | 0.6 | 9.3 | 0.0 | 0.0 | 0.173 | 241 | 167 | 141 | 87.3 | 794 | 491 |
| 1439 1687 | 0.7 | 10.0 | 0.0 | 0.0 | 0.147 | 282 | 196 230 | 165 | 102 | 927 1082 | 576 676 |
| 1828 | 0.5 | 11.3 | 0.0 | 0.0 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 1.1 | 12.4 | 1.2 | 1.2 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2944 | 2.4 | 16.2 | 2.7 | 5.5 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3448 | 5.0 | 21.2 | 5.7 | 11.2 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4044 4734 | 11.8 | 33.0 45.1 | 13.5 | 24.5 | 0.0524 | 793 928 | 551 644 | 463 | 287 | 2609 | 1621 |
| 5122 | 3.4 | 48.5 | 3.9 | 42.0 | 0.0414 | 1004 | 697 | 586 | 363 | 3300 | 2050 |
| 6005 | 6.5 | 55.1 | 7.4 | 49.4 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7897 | 4.5 | 65.6 | 5.0 | 61.2 | 0.0268 | 1548 | 1075 | 904 | 560 | 5091 | 3162 |
| 8927 | 4.4 | 69.9 | 4.9 | 66.1 | 0.0237 | 1750 | 1215 | 1022 | 633 | 5755 | 3574 |
| 10465 | 3.0 | 72.9 | 3.4 | 73.1 | 0.0219 | 2052 | 1425 | 1106 | 742 | 6745 | 4191 |
| 12297 | 7.8 | 83.9 | 8.8 | 81.9 | 0.0172 | 2411 | 1674 | 1407 | 871 | 7918 | 4924 |
| 14346 | 6.9 5.2 | 90.8 96.0 | 7.7 | 89.6 95.5 | 0.0148 | 2813 | 1953 | 1642 1876 | 1016 | 9236 10555 | 5744 |
| 18496 | 3.2 | 99.2 | 3.6 | 99.1 | 0.0115 | 3627 | 2519 | 2117 | 1311 | 11918 | 7409 |
| 20495 | 0.7 | 99.9 | 0.8 | 99.9 | 0.0103 | 4019 | 2791 | 2345 | 1452 | 13200 | 8209 |
| 25155 | 0.1 | 100.0 | 0.1 | 100.0 | 0.0092 | 4540 4915 | 3413 | 2850 | 1640 | 16145 | 9274 10038 |
| 27141 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5322 | 3696 | 3106 | 1923 | 17482 | 10871 |
| 29379 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5761 6236 | 4001 | 3362 | 2081 | 18918 | 11768 |
| 34424 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6750 | 4688 | 3940 | 2439 | 22173 | 13788 |
| 37194 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4257 | 2635 | 23955 | 14897 |
| 40344 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7911 8548 | 5494 5936 | 4617 4989 | 2858 | 25982 | 16159 |
| 47294 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 51169 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10033 | 6967 | 5856 | 3625 | 32955 | 20491 |
| 59876 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11740 | 8153 | 6852 | 4242 | 38564 | 23979 |



(B) Capillary Pressure Plot



Well Sample Depth

Tuna-1 1160.00 m



| Client | Geoscience Vict | toria | | | | | | | Conversio | n Parameters | | |
|--------------|------------------|----------------------|------------------|-----------------|------------------|-----------|------------------------------------|-------------------------|------------|--------------|-------------------|-------------------|
| Well | Kingfish-3 | | | | | | T 1 . 71 . | | | air/water | air/oil | oil/water |
| Test Method | Air/Mercury Ca | nillary Pressure Dra | ainage | | | | Laboratory Theta Laboratory IFT | | | 0.0 | 0.0 | 30.0 48.0 |
| i est method | . in mercury cu | pinary riessure Die | iiiiuge | | | | Reservoir Theta | | | 0.0 | 21.0 | 30.0 |
| Sample | Tuna-1 | | | Ambient Permea | ability | | Reservoir IFT | | | 50.0 | | 30.0 |
| Depth | 1160.00 | m | | Ambient Porosit | у | | Laboratory TcosT | `heta | | 72.0 | 24.0 | 42.0 |
| | ส | | | | | | Reservoir TcosTh | ieta | | 50.0 | | 26.0 |
| 0 070 | Entry Pressure (| nsia) | Displacement Pro | essure (nsia) | Threshold Pressu | re (nsia) | D | ensity Gradients, psi/1 | Typical | ł | | |
| System | Lab | Resv | Lab | Resv | Lab | Resv | Water: | | 0.440 | 1 | | |
| A-Hg | 1520 | - | 2951 | - | 3192 | - | Oil: | | 0.330 | | | |
| G-W | 298.3 | 207.1 | 578.9 | 402.0 | 626.2 | 434.9 | Gas: | | 0.100 | 1 | | |
| 0-w | 99.4 | 107.7 | 195.0 | 209.1 | 208.7 | 220.1 | 1 | | | | | |
| | | | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free |
| Pressure | | Intrusion | | Saturation | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) |
| (psia) | | (percent) | | (percent) | | (µm) | | | | | Oil-Water | Gas-Water |
| - | | | | | | | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 209 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 |
| 1.99 | | 0.0 | | 0.0 | | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.80 |
| 2.74 | | 0.0 | | 0.0 | | 77.4 | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.10 |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 |
| 5.19 | | 0.0 | | 0.0 | | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.98 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 |
| 8.28 | | 0.0 | | 0.0 | | 25.6 | 1.6 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.98 | | 0.0 | | 0.0 | | 21.2 | 2.0 | 1.4 | 1.14 | 0.71 | 6.43 7.41 | 4.00 |
| 13.5 | | 0.0 | | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 |
| 15.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 |
| 18.5 | | 0.0 | | 0.0 | | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 |
| 30.0 | | 0.0 | | 0.0 | | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 |
| 37.9 | | 0.0 | | 0.0 | | 5.60 | 7.4 | 5.2 | 4.3 | 2.7 | 24.41 | 15.18 |
| 46.6 | | 0.0 | | 0.0 | | 4.55 | 9.1 | 6.3 | 5.3 | 3.3 | 30.01 | 18.66 |
| 57.6 | | 0.0 | | 0.0 | | 3.68 | 11.3 | 7.8 | 6.6 | 4.1 | 37.10 | 23.07 |
| 77.9 | | 0.0 | | 0.0 | | 2.72 | 15 | 9.2 | 89 | 4.8 | 43.28 | 31.20 |
| 92.1 | | 0.0 | | 0.0 | | 2.30 | 18 | 13 | 10.5 | 6.5 | 59.32 | 36.88 |
| 110 | | 0.0 | | 0.0 | | 1.94 | 22 | 15 | 13 | 7.8 | 70.84 | 44.05 |
| 128 | | 0.0 | | 0.0 | | 1.65 | 25 | 17 | 15 | 9.1 | 82.44 | 51.26 |
| 178 | | 0.0 | | 0.0 | | 1.19 | 35 | 24 | 20 | 13 | 114.64 | 71.29 |
| 210 | | 0.0 | | 0.0 | | 1.01 | 41 | 29 | 24 | 15 | 135.2 | 84.10 |
| 246 | | 0.0 | | 0.0 | | 0.862 | 48 | 33 | 28 | 17 | 158.4 | 98.52 |
| 290 | | 0.0 | | 0.0 | | 0.731 | 57 | 39 | 33 | 21 | 186.8 | 116.14 |
| 401 | | 0.0 | | 0.0 | | 0.529 | 87 79 | 47 | 39 46 | 24 | 220.9 | 160.6 |
| 472 | | 0.0 | | 0.0 | | 0.449 | 93 | 64 | 54 | 33 | 304.0 | 189.0 |
| 554 | | 0.0 | | 0.0 | | 0.383 | 109 | 75 | 63 | 39 | 356.8 | 221.9 |
| 648 | | 0.0 | | 0.0 | | 0.327 | 127 | 88 | 74 | 46 | 417.3 | 259.5 |
| 887 | | 0.0 | | 0.0 | | 0.239 | 148 | 103 | 102 | 63 | 571.3 | 355.2 |
| 1048 | | 0.0 | | 0.0 | | 0.202 | 205 | 143 | 120 | 74 | 675.0 | 419.7 |
| 1227 | | 0.0 | | 0.0 | | 0.173 | 241 | 167 | 140 | 87 | 790.2 | 491.4 |
| 1438 | | 0.0 | | 0.0 | | 0.147 | 282 | 230 | 165 | 102 | 926.1 | 575.9 |
| 1828 | | 0.8 | | 0.5 | | 0.116 | 358 | 249 | 209 | 130 | 1177 | 732.1 |
| 2143 | | 1.5 | | 2.1 | | 0.0989 | 420 | 292 | 245 | 152 | 1380 | 858.2 |
| 2509 | | 2.5 | | 4.6 | | 0.0845 | 492 | 342 | 287 | 178 | 1616 | 1004.8 |
| 3448 | | 4.2 9.6 | | 0.0 18.4 | | 0.0720 | 676 | 469 | 395 | 209 | 2221 | 1381 |
| 4042 | | 16.9 | | 35.2 | | 0.0524 | 793 | 550 | 463 | 286 | 2603 | 1619 |
| 4730 | | 18.6 | | 53.9 | | 0.0448 | 927 | 644 | 541 | 335 | 3046 | 1894 |
| 5115 | | 14.2 | | 64.1 71.9 | | 0.0414 | 1003 | 696 817 | 585 687 | 362 | 3294 | 2048 |
| 7032 | | 5.6 | | 77.5 | | 0.0301 | 1379 | 958 | 805 | 498 | 4529 | 2816 |
| 7896 | | 2.9 | | 80.4 | | 0.0268 | 1548 | 1075 | 904 | 559 | 5085 | 3162 |
| 8926 | | 3.1 | | 83.4 | | 0.0238 | 1750 | 1215 | 1022 | 632 | 5749 | 3575 |
| 9662 | | 1.7 | | 85.1 | | 0.0219 | 1895 | 1316 | 1106 | 685 | 6223 | 3870 |
| 12296 | | 2.8 | | 89.7 | | 0.0172 | 2411 | 1674 | 1407 | 871 | 7919 | 4924 |
| 14345 | | 2.3 | | 92.0 | | 0.0148 | 2813 | 1953 | 1642 | 1016 | 9239 | 5745 |
| 16397 | | 1.5 | | 93.5 | | 0.0129 | 3215 | 2233 | 1876 | 1162 | 10560 | 6567 |
| 18493 | | 1.4 | | 95.0 | | 0.0115 | 3626 | 2518 | 2116 | 1310 | 11910 | 7406 |
| 23151 | | 0.6 | | 97.0 | | 0.0103 | 4539 | 3152 | 2649 | 1640 | 14910 | 9272 |
| 25068 | | 1.0 | | 98.0 | | 0.0085 | 4915 | 3413 | 2869 | 1776 | 16145 | 10039 |
| 27135 | | 0.2 | | 98.3 | | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17476 | 10867 |
| 29379 | | 0.4 | | 98.7 | | 0.0072 | 5761 | 4000 | 3362 | 2081 | 18921 | 11/66 |
| 34428 | | 0.3 | | 99.4 | | 0.0062 | 6751 | 4688 | 3940 | 2439 | 22173 | 13788 |
| 37197 | | 0.1 | | 99.5 | | 0.0057 | 7294 | 5065 | 4257 | 2635 | 23956 | 14897 |
| 40346 | | 0.1 | | 99.6 | | 0.0053 | 7911 | 5494 | 4617 | 2858 | 25985 | 16158 |
| 43595 | | 0.1 | | 99.8 | | 0.0049 | 8548 | 5936 6440 | 4989 | 3088 | 28077 | 17459 |
| 51173 | | 0.0 | | 99.8 99.9 | | 0.0045 | 10034 | 6968 | 5856 | 3625 | 32958 | 20494 |
| 55386 | | 0.0 | | 99.9 | | 0.0038 | 10860 | 7542 | 6338 | 3924 | 35671 | 22181 |
| 59891 | | 0.1 | | 100.0 | | 0.0035 | 11743 | 8155 | 6854 | 4243 | 38572 | 23986 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot



Well Sample Depth

Woodside South-1 522.12 m



| Client | Gaasajanaa Viatoria | | | | | | 1 | | Conversio | n Paramators | | |
|------------------|-----------------------|---------------|-----------------|-----------------|------------------|-----------|------------------|-------------------------|-----------|--------------|-------------------|-------------------|
| Well | Woodside South -1 | | | | | | | | Conversio | air/water | air/oil | oil/water |
| wen | woodside bould 1 | | | | | | Laboratory Theta | | | 0.0 | 0.0 | 30.0 |
| Test Method | Air/Mercury Canillary | Pressure Dr | ainage | | | | Laboratory IFT | | | 72.0 | 24.0 | 48.0 |
| rest sitetiidu | , in mercury cupinary | r ressure isn | annuge | | | | Reservoir Theta | | | 0.0 | | 30.0 |
| Sample | Woodside South -1 | | | Ambient Permea | ability | | Reservoir IFT | | | 50.0 | | 30.0 |
| Depth | 522.12 m | | | Ambient Porosit | v | | Laboratory Tcos | 'heta | | 72.0 | 24.0 | 42.0 |
| | | | | | ~ | | Reservoir TcosTl | ieta | | 50.0 | | 26.0 |
| pore radius (um) |) | | | | | | D | ensity Gradients, psi/f | ìoot | | | |
| 4.000 | Entry Pressure (psia) | | Displacement Pr | ressure (psia) | Threshold Pressu | re (psia) | | | Typical | | | |
| System | Lab | Resv | Lab | Resv | Lab | Resv | Water: | | 0.440 | 1 | | |
| A-Hg | 26.6 | - | 46.1 | - | 65.8 | - | Oil: | | 0.330 | | | |
| G-W | 5.2 | 3.6 | 9.0 | 6.3 | 12.9 | 9.0 | Gas: | | 0.100 | | | |
| O-W | 1.7 | 1.9 | 3.0 | 3.3 | 4.3 | 4.7 | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | Pore | Equivalent | Injection Pressures | | | Height Above Free | Height Above Free |
| Pressure | 1 | Intrusion | | Saturation | | Diameter | A/B Lab | A/B Res | O/B Lab | O/B Res | Water (feet) | Water (feet) |
| (psia) | (| (percent) | | (percent) | | (µm) | | | | | Oil-Water | Gas-Water |
| | | a , | | u , | | | | | | | | |
| | | | | | | | | | | | | |
| 1.01 | | 0.0 | | 0.0 | | 209 | 0.20 | 0.14 | 0.12 | 0.07 | 0.65 | 0.40 |
| 1.99 | | 0.0 | | 0.0 | | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.80 |
| 2.74 | | 0.0 | | 0.0 | | 77.4 | 0.54 | 0.37 | 0.31 | 0.19 | 1.76 | 1.10 |
| 3.19 | | 0.0 | | 0.0 | | 66.5 | 0.63 | 0.43 | 0.37 | 0.23 | 2.05 | 1.28 |
| 3.74 | | 0.0 | | 0.0 | | 56.7 | 0.73 | 0.51 | 0.43 | 0.26 | 2.41 | 1.50 |
| 4.38 | | 0.0 | | 0.0 | | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.75 |
| 5.19 | | 0.0 | | 0.0 | | 40.9 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | | 0.0 | | 0.0 | | 35.4 | 1.2 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.98 | | 0.0 | | 0.0 | | 30.4 | 1.4 | 0.95 | 0.80 | 0.49 | 4.50 | 2.80 |
| 8.28 | | 0.0 | | 0.0 | | 25.6 | 1.6 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.98 | | 0.0 | | 0.0 | | 21.2 | 2.0 | 1.4 | 1.14 | 0.71 | 6.43 | 4.00 |
| 11.5 | | 0.0 | | 0.0 | | 18.5 | 2.3 | 1.6 | 1.3 | 0.81 | 7.41 | 4.61 |
| 13.5 | | 0.0 | | 0.0 | | 15.7 | 2.6 | 1.8 | 1.5 | 0.96 | 8.69 | 5.41 |
| 15.5 | | 0.0 | | 0.0 | | 13.7 | 3.0 | 2.1 | 1.8 | 1.10 | 9.98 | 6.21 |
| 18.5 | | 0.0 | | 0.0 | | 11.5 | 3.6 | 2.5 | 2.1 | 1.3 | 11.91 | 7.41 |
| 21.6 | | 0.0 | | 0.0 | | 9.83 | 4.2 | 2.9 | 2.5 | 1.5 | 13.91 | 8.65 |
| 25.3 | | 0.0 | | 0.0 | | 8.39 | 5.0 | 3.4 | 2.9 | 1.8 | 16.29 | 10.13 |
| 30.0 | | 0.9 | | 0.9 | | 7.08 | 5.9 | 4.1 | 3.4 | 2.1 | 19.32 | 12.01 |
| 38.8 | | 1.7 | | 2.6 | | 5.46 | 7.6 | 5.3 | 4.4 | 2.7 | 24.99 | 15.54 |
| 48.4 | | 2.1 | | 4.8 | | 4.38 | 9.5 | 6.6 | 5.5 | 3.4 | 31.17 | 19.38 |
| 56.9 | | 3.1 | | 7.9 | | 3.73 | 11.2 | 7.7 | 6.5 | 4.0 | 36.65 | 22.79 |
| 68.4 | | 3.7 | | 11.6 | | 3.10 | 13 | 9.3 | 7.8 | 4.8 | 44.05 | 27.39 |
| 79.8 | | 3.8 | | 15.4 | | 2.66 | 16 | 10.9 | 9.1 | 5.7 | 51.39 | 31.96 |
| 93.9 | | 4.8 | | 20.2 | | 2.26 | 18 | 13 | 10.7 | 6.7 | 60.48 | 37.61 |
| 108 | | 4.3 | | 24.5 | | 1.97 | 21 | 15 | 12 | 7.7 | 69.56 | 43.25 |
| 127 | | 4.8 | | 29.3 | | 1.67 | 25 | 17 | 15 | 9.0 | 81.79 | 50.86 |
| 152 | | 5.5 | | 34.7 | | 1.39 | 30 | 21 | 17 | 10.8 | 97.89 | 60.87 |
| 180 | | 4.6 | | 39.4 | | 1.18 | 35 | 25 | 21 | 13 | 115.93 | 72.09 |
| 209 | | 4.3 | | 43.7 | | 1.01 | 41 | 28 | 24 | 15 | 134.6 | 83.70 |
| 245 | | 4.3 | | 48.0 | | 0.865 | 48 | 33 | 28 | 17 | 157.8 | 98.12 |
| 290 | | 4.5 | | 52.5 | | 0.732 | 57 | 39 | 33 | 21 | 180.8 | 110.14 |
| 400 | | 4.2 | | 50.0 | | 0.531 | 78 | 40 54 | 16 | 24 | 219.0 | 160.2 |
| 400 | | 4.0 | | 64.7 | | 0.451 | 92 | 64 | 54 | 33 | 302.7 | 188.2 |
| 553 | | 3.9 | | 68.5 | | 0.383 | 108 | 75 | 63 | 39 | 356.2 | 221.5 |
| 645 | | 3.4 | | 71.9 | | 0.329 | 126 | 88 | 74 | 46 | 415.4 | 258.3 |
| 757 | | 3.2 | | 75.2 | | 0.280 | 148 | 103 | 87 | 54 | 487.5 | 303.2 |
| 885 | | 2.9 | | 78.1 | | 0.240 | 174 | 121 | 101 | 63 | 570.0 | 354.4 |
| 1045 | | 2.7 | | 80.8 | | 0.203 | 205 | 142 | 120 | 74 | 673.0 | 418.5 |
| 1227 | | 2.4 | | 83.2 | | 0.173 | 241 | 167 | 140 | 87 | 790.2 | 491.4 |
| 1435 | | 2.1 | | 85.3 | | 0.148 | 281 | 195 | 164 | 102 | 924.2 | 574.7 |
| 1684 | | 1.9 | | 87.2 | | 0.126 | 330 | 229 | 193 | 119 | 1084.6 | 674.4 |
| 1826 | | 1.7 | | 88.1 | | 0.116 | 358 | 249 | 209 | 129 | 1176 | 731.3 |
| 2144 | | 1.7 | | 89.8 | | 0.0989 | 420 | 292 | 245 | 152 | 1381 | 858.6 |
| 2508 | | 1.3 | | 91.1 | | 0.0845 | 492 | 342 | 287 | 178 | 1615 | 1004.4 |
| 2941 | | 1.0 | | 92.1 | | 0.0721 | 577 | 400 | 337 | 208 | 1894 | 1178 |
| 3445 | | 1.1 | | 93.2 | | 0.0615 | 675 | 469 | 394 | 244 | 2219 | 1380 |
| 4038 | | 1.1 | | 94.3 | | 0.0525 | 792 | 550 | 462 | 286 | 2601 | 1617 |
| 4732 | | 1.4 | | 95.7 | | 0.0448 | 928 | 644 | 542 | 335 | 3048 | 1895 |
| 5117 | | 1.0 | | 96.2 | | 0.0414 | 1003 | 697 | 586 | 363 | 3296 | 2049 |
| 5997 | | 0.8 | | 97.1 | | 0.0354 | 1176 | 817 | 686 | 425 | 3862 | 2402 |
| 7026 | | 0.9 | | 97.9 | | 0.0302 | 13/8 | 957 | 804 | 498 | 4525 | 2814 |
| 7883 | | 0.6 | | 98.5 | | 0.0269 | 1546 | 1073 | 902 | 558 | 50// | 3157 |
| 8913 | | 0.5 | | 99.0 | | 0.0238 | 1/48 | 1214 | 1020 | 631 | 5/40 | 3570 |
| 9649 | | 0.2 | | 99.3 | | 0.0220 | 1892 | 1314 | 1104 | 684 | 6214 | 3864 |
| 10451 | | 0.2 | | 99.4 | | 0.0203 | 2049 | 1423 | 1196 | /40 | 6/31 | 4185 |
| 12284 | | 0.5 | | 99.8 | | 0.01/3 | 2409 | 10/3 | 1400 | 870 | /911 | 4920 |
| 14330 | | 0.2 | | 99.9 | | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9229 | 5/39 |
| 10383 | | 0.1 | | 100.0 | | 0.0129 | 3213 | 2231 | 10/3 | 1101 | 10003 | 7401 |
| 164/9 | | 0.0 | | 100.0 | | 0.0115 | 3023 | 2010 | 2115 | 1309 | 11901 | /401 |
| 20464 | | 0.0 | | 100.0 | | 0.0103 | 4010 | 2/09 | 2344 | 1431 | 13193 | 0204 |
| 23140 | | 0.0 | | 100.0 | | 0.0092 | 4015 | 3132 | 2049 | 1040 | 14908 | 10029 |
| 23003 | | 0.0 | | 100.0 | | 0.0085 | 4913 | 3413 | 2000 | 1022 | 10145 | 10058 |
| 2/130 | | 0.0 | | 100.0 | | 0.0078 | 5740 | 4000 | 3363 | 1922 | 1/4// | 11766 |
| 27378 | | 0.0 | | 100.0 | | 0.00/2 | 6726 | 4000 | 3640 | 2001 | 204921 | 12727 |
| 31004 | | 0.0 | | 100.0 | | 0.0067 | 6750 | 4331 | 3040 | 2233 | 20463 | 12/3/ |
| 34423 | | 0.0 | | 100.0 | | 0.0062 | 7202 | +08/ | 1257 | 2439 | 22170 | 1/806 |
| 40242 | | 0.0 | | 100.0 | | 0.0057 | 7010 | 5402 | 4617 | 2000 | 25955 | 16157 |
| 40343 | | 0.0 | | 100.0 | | 0.0055 | 910 | 5026 | 401/ | 2020 | 23983 | 17/59 |
| 43393 | | 0.0 | | 100.0 | | 0.0049 | 0.040 | 5950 6//0 | 4709 | 3351 | 20070 | 1/438 |
| 51171 | | 0.0 | | 100.0 | | 0.0043 | 10034 | 6068 | 5856 | 3625 | 32056 | 20/03 |
| 55385 | | 0.0 | | 100.0 | | 0.0041 | 10054 | 7542 | 6338 | 3023 | 32930 | 20493 |
| 50990 | | 0.0 | | 100.0 | | 0.0038 | 11741 | 9154 | 6952 | 3724 4242 | 29565 | 22101 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

| Well Sample | Depth | | | Woound 389.3 m | ellah-10 | | | | | | |
|---|---|---|---|--|---|--|---|---|--|---|--|
| Client Well Test Method | Geoscience ' Wooundellal Air/Mercury | Victoria h-10 Capillary Pressu | ıre | Density O Water: Oil: | Typical 0.440 0.330 | Laboratory Thet Laboratory IFT | Conv | air/water 0.0 72.0 | ers (dynes/cm) air/oil 0.0 24.0 | oil/water 30.0 48.0 | CO ₂ /water 0.0 72.0 |
| Sample Depth | W10 389.30 m | | | Gas: CO ₂ Density | 0.100 | Reservoir Theta Reservoir IFT Laboratory Tcos Reservoir TcosT | Theta | 0.0 50.0 72.0 50.0 | 24.0 | 30.0 30.0 42.0 26.0 | 0.0 26.0 72.0 26.0 |
| Pore radius (µ | m) | 2.70 | | System A-Hg G-W | Estimated Column Height (feet) na 16 | Entry P Lab 39.5 7.74 | ressure (psia) Res Con - 5.38 | Displacement F Lab 41.1 8.05 | Resv - 5.59 | Threshold P Lab 42.9 8.42 | ressure (psia) Resv - 5.85 |
| | | | | O-W CO ₂ -W | 25 7 | 2.58 7.74 | 2.80 2.80 | 2.68 8.05 | 2.91 2.91 | 2.81 8.42 | 3.04 3.04 |
| Pressure (psia) | Raw Intrusion (percent) | Saturation (percent) | Conform Intrusion (percent) | ance Corrected Saturation (percent) | Pore Diameter (µm) | Equivalent Air/Brine Lab (psi) | Injection Pressures Air/Brine Res Con (psi) | Oil/Brine Lab Conditions (psi) | Oil/Brine Reservoir Conditions (psi) | Height Above Free Water Oil-Water (feet) | Height Above Free Water Gas-Water (feet) |
| Pressure (psia) 1.00 1.98 2.73 3.18 3.73 4.38 5.18 5.73 4.38 5.18 5.98 6.97 8.27 9.97 11.5 13.5 15.5 18.5 21.6 25.3 30.0 36.8 46.3 55.4 65.4 677 127 150 179 208 244 289 342 400 471 552 1436 1686 1826 2141 2509 2944 3448 4045 4732 5116 | Indusion (percent) 0.0 1.8 1.9 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.6 0.5 0.4 0.6 0.5 0.4 0.6 0.5 0.9 0.8 1.5 2.0 2.0 0.0 0.1 0.0 0.1 | 0.0 1.8 3.8 4.3 4.7 5.1 5.6 6.1 6.5 7.0 7.6 8.2 9.0 9.8 11.3 13.3 16.2 31.8 78.6 98.8 98.9 99.0 99.1 99.1 99.1 99.1 99.1 99.1 99.2 99.3 99.4 99.5 99.6 99.7 99.8 99.9 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.0 0.1 0.0 | Saturation (percent) 0.0 99.0 99.1 99.2 99.3 99.4 99.5 99.6 99.7 99.8 99.9 100.0 100.0 | 212 107 77.7 66.7 56.8 48.4 41.0 35.5 30.4 25.6 21.3 18.5 15.7 13.7 11.5 9.83 8.39 7.08 5.76 4.58 3.83 3.24 2.75 2.35 1.95 1.66 1.41 1.19 1.02 0.869 0.735 0.620 0.530 0.450 0.328 0.280 0.280 0.289 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.239 0.244 0.0444 0.0444 0.0444 | Lab (psi) 0.20 0.39 0.54 0.62 0.73 0.86 1.02 1.17 1.37 1.62 1.95 2.25 2.65 3.04 3.63 4.24 4.96 5.88 7.22 9.08 10.9 12.8 15.1 17.7 21.4 24.9 29.4 3.5.1 40.8 15.7 67.1 78.4 92.4 108 127 148 177 148 177 177 187 195 240 282 331 358 420 492 577 676 793 928 1003 | Res Con (psi) 0.14 0.27 0.37 0.43 0.51 0.60 0.71 0.81 0.95 1.13 1.35 1.56 1.84 2.11 2.52 2.94 3.44 4.08 5.01 6.31 7.57 8.89 10.5 12.3 14.9 17.3 20.4 24.4 28.3 33.2 39.4 46.6 54.4 64.2 75.0 88.2 103 121 142 167 196 230 249 292 342 401 469 551 644 697 | 0.11 0.23 0.31 0.36 0.33 0.33 0.36 0.43 0.37 0.59 0.68 0.80 0.95 1.14 1.32 1.54 1.77 2.12 2.47 2.90 3.43 4.21 5.30 6.34 7.48 8.82 10.3 12.5 14.5 17.2 20.5 23.8 27.9 33.1 39.1 45.8 45.8 53.9 63.2 74.0 74.0 86.5 101 120 140 164 193 209 245 287 337 395 463 542 | 0.07 0.14 0.19 0.23 0.26 0.31 0.37 0.42 0.49 0.59 0.71 0.82 0.895 1.10 1.31 1.53 1.80 2.12 2.61 3.28 3.92 4.63 5.46 6.38 7.74 8.98 8.06 12.7 14.7 17.3 20.5 24.2 28.4 33.4 39.1 45.8 5.35 62.5 74.3 86.7 102 119 129 152 178 209 245 287 336 362 | 0.1-water (feet) 0.64 1.28 1.75 2.05 2.40 2.82 3.34 3.85 4.49 5.33 6.42 7.43 8.66 10.0 11.9 13.9 16.4 19.3 23.7 29.8 35.6 42.1 49.6 58.0 70.4 81.6 96.4 115 134 157 186 220 258 304 355 416 486 558 675 788 927 1082 2173 1382 1618 1900 2227 2609 3055 3291 | 0.40 0.79 1.09 1.09 1.27 1.49 1.76 2.08 2.39 2.80 3.32 3.97 4.59 5.41 6.211 7.41 7.45 10.1 1.2.0 14.7 1.8.6 22.3 2.6.1 30.9 36.2 43.8 50.9 60.0 71.8 83.2 97.6 116 137 160 189 221 259 303 356 418 491 576 676 732 859 1006 1179 1379 1621 179 1379 1621 |
| 5999 7023 7887 8917 9650 10453 12286 14336 16385 18482 20486 23152 25067 27137 29381 31804 34424 37195 40343 | 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 | 0.0353 0.0302 0.0269 0.0238 0.0220 0.0203 0.0173 0.0148 0.0129 0.0115 0.0103 0.0092 0.0085 0.0072 0.0067 0.0067 0.0067 0.0053 | 1176 1377 1546 1748 1892 2050 2409 2811 3213 3624 4017 4540 4915 5321 5761 6236 6750 7293 7910 | 81/ 956 1074 1214 1314 1424 1673 1952 2231 2517 2790 3153 3413 3695 4001 4331 4688 5065 5493 | 687 804 903 1020 1104 1196 1406 1641 1875 2115 2344 2650 2869 3106 3362 3640 3362 3640 3940 4257 4617 | 425 498 559 631 683 740 870 1016 1161 1309 1451 1640 1776 1923 2081 2253 2439 2635 2858 | 3884 4527 5082 5736 6209 6727 7909 9236 10555 11900 13191 14909 16145 17482 18918 20482 22173 23955 25982 | 2403 2812 3159 3571 3865 4188 4921 5741 6562 7403 8206 9274 10038 10868 11768 11768 11768 12738 13788 14897 16156 |
| 43593 47293 51175 55389 59883 | 0.0 0.0 0.0 0.0 0.0 | 100.0 100.0 100.0 100.0 100.0 | 0.0 0.0 0.0 0.0 0.0 | 100.0 100.0 100.0 100.0 100.0 | 0.0049 0.0045 0.0041 0.0038 0.0035 | 8548 9273 10034 10861 11742 | 5936 6440 6968 7542 8154 | 4989 5412 5857 6339 6853 | 3088 3350 3626 3924 4242 | 28073 30455 32964 35673 38564 | 17459 18941 20494 22182 23982 |

55389 0.0 100.0 0.0 100.0 59883 0.0 100.0 0.0 100.0 (A) Interpreted Capillary Pressure Chart



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

ACS LABORATORIES

BORATOR

| Well Sample | Depth | | V 3 | Vooundel 89 m | lah-11 | | | | | | |
|-----------------|--------------|----------------------|-----------------------|------------------------------|-----------------------------------|--------------------------------|---|--------------------------------|--------------------------------------|---|---|
| Client | Geoscience A | A Victoria | | Density G | radients (psi/foot) | | Con | version Paramet | ters (dynes/cm) | - | - |
| Well | Wooundellal | n-11 | | Watar | Typical | Laboratory Tha | to | air/water | air/oil | oil/water | CO ₂ /water |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | la | 72.0 | 24.0 | 48.0 | 72.0 |
| Cl. | 3711 | | | Gas: | 0.100 | Reservoir Theta | L | 0.0 | | 30.0 | 0.0 |
| Sample Depth | 389.00 m | | | CO2 Density | 0.081 | Laboratory Tco: | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | | Reservoir Tcos | Theta | 50.0 | | 26.0 | 26.0 |
| Pore radius (u | m) | 1 69 | | System | Estimated Column Height (feet) | Entry I Lab | Pressure (psia) Res Con | Displacement I | Pressure (psia) Resv | Threshold P Lab | ressure (psia) Resv |
| |) | | | A-Hg | na | 62.9 | - | 89.7 | - | 112 | - |
| | | | | G-W O-W | 25 | 12.3 | 8.57 4.46 | 17.6 | 6.35 | 21.9 | 15.2 |
| | | | | CO ₂ -W | 11 | 12.3 | 4.46 | 17.6 | 6.35 | 21.9 | 7.90 |
| Pressure | Raw | / Data Saturation | Conforma Intrusion | ance Corrected Saturation | Pore Diameter | Equivalent Air/Brine Lab | Injection Pressures Air/Brine Res Con | Oil/Brine Lab Conditions | Oil/Brine Reservoir Conditions | Height Above Free Water Oil-Water | Height Above Free Water Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (µm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 2.73 | 0.0 | 0.0 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.25 | 0.19 | 1.20 | 1.09 |
| 3.18 | 0.0 | 0.0 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 3.73 4.38 | 0.0 | 0.0 | 0.0 | 0.0 | 56.9 48.4 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 2.82 | 1.49 |
| 5.18 | 0.0 | 0.0 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.0 | 0.0 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 8.27 | 0.0 | 0.0 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.0 | 0.0 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.0 | 0.0 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.52 | 0.82 | 8.66 | 4.59 5.41 |
| 15.5 | 0.0 | 0.0 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.0 | 0.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 25.3 | 0.0 | 0.0 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 47.2 | 0.0 | 0.0 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 4.26 5.40 | 3.34 | 30.4 | 14.9 |
| 56.6 | 0.3 | 0.4 | 0.3 | 0.3 | 3.75 | 11.1 | 7.71 | 6.48 | 4.01 | 36.5 | 22.7 |
| 66.3 80.4 | 0.4 | 0.8 | 0.4 | 0.7 | 3.20 2.64 | 13.0 15.8 | 9.03 11.0 | 7.59 9.20 | 4.70 5.70 | 42.7 51.8 | 26.6 32.4 |
| 93.0 | 2.7 | 5.2 | 2.7 | 5.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 4.6 | 9.8 | 4.6 | 9.7 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 6.8 | 23.7 | 6.8 | 23.5 | 1.05 | 25.5 | 20.7 | 14.8 | 10.8 | 83.3 98.2 | 60.9 |
| 179 | 9.2 | 32.9 | 9.3 | 32.8 | 1.18 | 35.1 | 24.4 | 20.5 | 12.7 | 115 | 71.8 |
| 210 247 | 6.9 5.6 | 39.8 45.4 | 6.9 5.7 | 39.7 45.3 | 1.01 | 41.2 48.4 | 28.6 | 24.0 | 14.9 17.5 | 135 | 84.1 98.8 |
| 292 | 9.5 | 54.9 | 9.5 | 54.8 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 6.1 | 61.0 | 6.1 | 60.9 67.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 472 | 5.7 | 72.8 | 5.7 | 72.8 | 0.328 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 5.9 | 78.7 | 5.9 | 78.7 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 757 | 5.7 | 84.4 89.7 | 5.7 | 84.4 89.7 | 0.328 | 127 | 103 | 74.0 86.6 | 43.8 53.6 | 416 | 303 |
| 887 | 5.2 | 94.9 | 5.3 | 94.9 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 4.0 | 99.0 100.0 | 4.1 | 99.0 100.0 | 0.202 | 205 241 | 142 | 120 140 | 74.3 86.7 | 675 788 | 418 491 |
| 1439 | 0.0 | 100.0 | 0.0 | 100.0 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 0.0 | 100.0 | 0.0 | 100.0 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 2142 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0990 | 420 | 249 292 | 209 | 129 | 1382 | 859 |
| 2510 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 3449 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0720 0.0615 | 577 676 | 401 469 | 337 395 | 209 245 | 1900 2227 | 1179 |
| 4040 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 6002 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 7895 8920 | 0.0 0.0 | 100.0 | 0.0 | 100.0 | 0.0269 | 1548 1749 | 1075 | 904 1021 | 560 632 | 5091 5745 | 3162 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 870 | 6727 | 4185 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 1875 | 1161 | 10555 | 6562 |
| 18481 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0115 0.0104 | 3624 4016 | 2517 2789 | 2115 | 1309 1451 | 11900 13191 | 7403 8203 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 2/135 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 5760 | 3095 4000 | 3362 | 2081 | 1/4/3 18918 | 10868 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6236 | 4331 | 3640 | 2253 | 20482 | 12738 |
| 34421 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0062 | 6749 7293 | 4687 | 3939 4256 | 2438 | 22164 | 13785 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47291 51172 | 0.0 0.0 | 100.0 100.0 | 0.0 | 100.0 100 0 | 0.0045 | 9273 10034 | 6440 6968 | 5412 5856 | 3350 3625 | 30455 32955 | 18941 20494 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0038 | 10860 | 7542 | 6339 | 3924 | 35673 | 22182 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |







(C) Pore Size Distribution plot

| Well Sample | Depth | | W 2 | /rasse-1 589.89 r | n | | | | | | |
|-----------------|---|-----------------|------------|-------------------------|----------------------|-------------------------|---------------------|-----------------|------------------------|---------------------|------------------------|
| Client | Geoscience A | Victoria | | Density (| Gradients (psi/foot) | T | Con | version Paramet | ers (dvnes/cm |) | |
| Well | Wrasse-1 | | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory The | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Press | ure | Oil: | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| | | | | Gas: | 0.100 | Reservoir Theta | 1 | 0.0 | | 30.0 | 0.0 |
| Sample | W1 | | | 00 D 1 | 0.577 | Reservoir IFT | | 50.0 | 21.0 | 30.0 | 26.0 |
| Depth | 2589.89 m | | | CO ₂ Density | 0.567 | Laboratory Ico | s I heta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | | Estimated Column | Reservoir I cos | I heta | 50.0 | Dragaura (ncia) | 26.0 Threshold B | 26.0 |
| Pore radius (| um) | 0.017 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv |
| i ore radius (j | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 0.017 | | A-Hg | na | 6149 | - | 7271 | - | 8025 | - |
| | | | | G-W | 2464 | 1206 | 838 | 1426 | 991 | 1574 | 1093 |
| | | | | O-W | 3960 | 402 | 436 | 475 | 515 | 525 | 569 |
| | | | | CO ₂ -W | 2326 | 1206 | 436 | 1426 | 515 | 1574 | 569 |
| | | | | | | E 1 1 4 | L' C D | 0.1/0 | 0.1/D : | TT 1 1 41 | 11 1 1 4 1 |
| | Pau | Data | Conform | maa Corrected | Doro | Equivalent Air/Prino | Injection Pressures | Oil/Brine | Oil/Brine Basaruair | Height Above | Height Abov |
| Pressure | Intrusion | Saturation | Intrusion | Saturation | Diameter | Lab | Res Con | Conditions | Conditions | Oil-Water | Gas-Water |
| (psia) | (percent) | (percent) | (percent) | (percent) | (μm) | (psi) | (psi) | (psi) | (psi) | (feet) | (feet) |
| · · · | ų , | ų , | ų , | ч , | N 2 | <i>u</i> , | ч.У. | ч.) | ч <i>ў</i> | | . , |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 0.0 | 0.0 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 2.7 | 2.7 | 0.0 | 0.0 | 77.6 | 0.54 | 0.37 | 0.31 | 0.19 | 1.75 | 1.09 |
| 3.18 | 0.7 | 3.4 | 0.0 | 0.0 | 66.7 | 0.62 | 0.43 | 0.36 | 0.23 | 2.05 | 1.27 |
| 5.75 4.38 | 0.4 | 5.7 | 0.0 | 0.0 | 50.9 48.4 | 0.73 | 0.51 | 0.43 | 0.26 | 2.40 | 1.49 |
| 5.18 | 0.4 | 4.4 | 0.0 | 0.0 | 41.0 | 1.02 | 0.00 | 0.50 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.3 | 4.8 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 | 0.3 | 5.1 | 0.0 | 0.0 | 30.4 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 8.27 | 0.3 | 5.4 | 0.0 | 0.0 | 25.6 | 1.62 | 1.13 | 0.95 | 0.59 | 5.33 | 3.32 |
| 9.97 | 0.3 | 5.7 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.4 | 6.1 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 15.5 | 0.3 | 6.7 | 0.0 | 0.0 | 13.7 | 2.65 | 2.11 | 1.34 | 0.93 | 8.00 | 5.41 |
| 18.5 | 0.3 | 7.0 | 0.0 | 0.0 | 11.5 | 3.63 | 2.52 | 2.12 | 1.31 | 11.9 | 7.41 |
| 21.6 | 0.4 | 7.3 | 0.0 | 0.0 | 9.83 | 4.24 | 2.94 | 2.47 | 1.53 | 13.9 | 8.65 |
| 25.3 | 0.3 | 7.6 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 0.3 | 8.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.5 | 8.4 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.1 | 8.5 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 66.3 | 0.1 | 8.6 | 0.0 | 0.0 | 3 20 | 13.0 | 9.03 | 7 59 | 4.01 | 42.7 | 26.6 |
| 80.4 | 0.1 | 8.8 | 0.0 | 0.0 | 2.64 | 15.8 | 11.0 | 9.20 | 5.70 | 51.8 | 32.4 |
| 93.0 | 0.1 | 8.9 | 0.0 | 0.0 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 0.1 | 9.0 | 0.0 | 0.0 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 0.2 | 9.2 | 0.0 | 0.0 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 0.2 | 9.4 | 0.0 | 0.0 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 210 | 0.2 | 9.0 | 0.0 | 0.0 | 1.18 | 55.1 41.2 | 24.4 | 20.5 | 12.7 | 115 | /1.8 |
| 247 | 0.3 | 10.0 | 0.0 | 0.0 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 0.2 | 10.3 | 0.0 | 0.0 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 0.3 | 10.5 | 0.0 | 0.0 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 | 0.3 | 10.8 | 0.0 | 0.0 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 472 | 0.3 | 11.1 | 0.0 | 0.0 | 0.449 | 92.5 | 64.2 | 54.0 | 33.4 | 304 | 189 |
| 553 | 0.3 | 11.4 | 0.0 | 0.0 | 0.383 | 108 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 757 | 0.3 | 12.0 | 0.0 | 0.0 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 887 | 0.3 | 12.3 | 0.0 | 0.0 | 0.239 | 174 | 103 | 102 | 63.1 | 574 | 356 |
| 1048 | 0.4 | 12.7 | 0.0 | 0.0 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1227 | 0.5 | 13.2 | 0.0 | 0.0 | 0.173 | 241 | 167 | 140 | 86.7 | 788 | 491 |
| 1439 | 0.5 | 13.6 | 0.0 | 0.0 | 0.147 | 282 | 196 | 165 | 102 | 927 | 576 |
| 1688 | 0.5 | 14.2 | 0.0 | 0.0 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 0.6 | 14.8 | 0.0 | 0.0 | 0.116 | 358 420 | 249 | 209 | 129 | 1173 | 732 |
| 2510 | 0.5 | 15.8 | 0.0 | 0.0 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | 0.8 | 16.5 | 0.0 | 0.0 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 1179 |
| 3449 | 0.9 | 17.4 | 0.0 | 0.0 | 0.0615 | 676 | 469 | 395 | 245 | 2227 | 1379 |
| 4040 | 1.0 | 18.4 | 0.0 | 0.0 | 0.0525 | 792 | 550 | 462 | 286 | 2600 | 1618 |
| 4728 | 1.2 | 19.5 | 0.0 | 0.0 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 2.1 | 21.6 | 0.0 | 0.0 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 1.0 | 22.6 | 1.3 | 1.3 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7895 | 2.7 4.5 | 23.5 29.9 | 5.5 5.8 | 4.8 | 0.0301 | 1579 | 958 1075 | 805 904 | 498 | 4027 5091 | 2010 |
| 8920 | 5.4 | 35.2 | 6.9 | 17.4 | 0.0238 | 1749 | 1215 | 1021 | 632 | 5745 | 3574 |



3865 4185

4918 5738

6562 7403

8203 9271

10038 10868

11765 12738

13785

14897

16156 17456

18941

20494

22182 23979

55387 59880 100.0 100.0 100.0 100.0 (A) Interpreted Capillary Pressure Chart

42.9 49.8

57.6 71.8

87.6 100.0

100.0 100.0

100.0

100.0

100.0 100.0

100.0

100.0

100.0 100.0

100.0 100.0

5.8 6.9 9.7 8.9 9.9 18.1

20.2 15.8

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0

0.0

27.1 36.0

45.9

64.0 84.2 100.0

100.0 100.0

100.0 100.0

100.0 100.0

100.0 100.0

100.0 100.0

100.0 100.0

0.0220 0.0203

0.0173

0.0148

0.0129 0.0115

0.0104 0.0092

0.0085 0.0078

0.0072 0.0067

0.0062

0.0057

0.0053 0.0049

0.0045

0.0041

0.0038 0.0035

1892 2049

2408 2810

3212 3624

4016 4539

4915 5321

5760 6236

6749 7293

7910 8547

9273

10034

10860

11741

1314 1423

1672 1951

2231 2517

2789 3152

3413

3695

4000 4331

4687 5065

5493 5935

6440

6968

7542 8153

1104 1196

1406

1640

1875 2115

2344 2649

2868

3105

3362 3640 3939

4256

6339

6853

683 740

870 1015

1161 1309

1451 1640

1775

1922

2081 2253

2438

2635

2858 3088

3350

3625

3924 4242

6209 6727

7909 9227

10555 11900

13191 14909

16136 17473

18918 20482

22164

23955

25982 28073

30455

32955

35673 38564

2.7 4.5 5.4 7.6 7.0 7.7 14.2 15.8 12.4

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0 0.0

0.0

0.0

9649 10452

12283 14333

16381 18481

20481 23149

25064 27135

29376 31804

34421

37192







(C) Pore Size Distribution plot

| Well Sample | Depth | | \ I | Wurruk W 584.9 m | urruk-13 | | | | | | |
|----------------|--------------|------------------|-----------|-------------------------|---------------------|----------------------------------|----------------------|-----------------|-----------------|--------------|------------------------|
| Client | Geoscience A | Victoria | | Density G | radients (psi/foot) | | Con | version Paramet | ers (dynes/cm) |) | |
| Well | Wurruk Wur | ruk-13 | | | Typical | | | air/water | air/oil | oil/water | CO ₂ /water |
| | | | | Water: | 0.440 | Laboratory Thet | ta | 0.0 | 0.0 | 30.0 | 0.0 |
| Test Method | Air/Mercury | Capillary Pressu | ire | Oil: Gasi | 0.330 | Laboratory IFT | | 72.0 | 24.0 | 48.0 | 72.0 |
| Sample | WW13 | | | Gas: | 0.100 | Reservoir Theta Reservoir IET | l | 50.0 | | 30.0 | 26.0 |
| Denth | 584 90 m | | | CO ₂ Density | 0 145 | Laboratory Tcos | sTheta | 72.0 | 24.0 | 42.0 | 72.0 |
| | | | | 2 | | Reservoir TcosT | Theta | 50.0 | | 26.0 | 26.0 |
| | | | | | Estimated Column | Entry P | Pressure (psia) | Displacement I | Pressure (psia) | Threshold F | ressure (psia) |
| Pore radius (µ | m) | 0.702 | | System | Height (feet) | Lab | Res Con | Lab | Resv | Lab | Resv |
| | | | | A-Hg C W | na 61 | 152 | - 20.7 | 41.3 | - 28.7 | 234 | - 21.0 |
| | | | | O-W | 98 | 9.92 | 10.7 | 13.8 | 14.9 | 15.3 | 16.6 |
| | | | | CO ₂ -W | 29 | 29.8 | 10.7 | 41.3 | 14.9 | 45.9 | 16.6 |
| | | | | | | | | | | | |
| | | | | | | Equivalent | Injection Pressures | Oil/Brine | Oil/Brine | Height Above | Height Above |
| Draggura | Intrusion | Data | Conform | ance Corrected | Pore | Air/Brine | Air/Brine Bac Con | Lab | Reservoir | Free Water | Free Water |
| (nsia) | (nercent) | (percent) | (percent) | (percent) | (um) | (nsi) | (nsi) | (nsi) | (nsi) | (feet) | (feet) |
| (1.1.1.) | (1) | (†) | (J) | (1) | (1111) | (1.0.) | (1) | (1) | (1) | () | () |
| | | | | | | | | | | | |
| 1.00 | 0.0 | 0.0 | 0.0 | 0.0 | 211 | 0.20 | 0.14 | 0.11 | 0.07 | 0.64 | 0.40 |
| 1.98 | 1.4 | 1.4 | 0.0 | 0.0 | 107 | 0.39 | 0.27 | 0.23 | 0.14 | 1.28 | 0.79 |
| 2.73 | 0.0 | 2.0 | 0.0 | 0.0 | 66 7 | 0.54 | 0.57 | 0.31 | 0.19 | 2.05 | 1.09 |
| 3.73 | 0.4 | 2.7 | 0.0 | 0.0 | 56.9 | 0.73 | 0.51 | 0.43 | 0.25 | 2.40 | 1.49 |
| 4.38 | 0.4 | 3.1 | 0.0 | 0.0 | 48.4 | 0.86 | 0.60 | 0.50 | 0.31 | 2.82 | 1.76 |
| 5.18 | 0.4 | 3.5 | 0.0 | 0.0 | 41.0 | 1.02 | 0.71 | 0.59 | 0.37 | 3.34 | 2.08 |
| 5.98 | 0.3 | 3.8 | 0.0 | 0.0 | 35.5 | 1.17 | 0.81 | 0.68 | 0.42 | 3.85 | 2.39 |
| 6.97 8.27 | 0.4 | 4.2 | 0.0 | 0.0 | 30.4 25.6 | 1.37 | 0.95 | 0.80 | 0.49 | 4.49 | 2.80 |
| 9.97 | 0.5 | 5.2 | 0.0 | 0.0 | 21.3 | 1.95 | 1.35 | 1.14 | 0.71 | 6.42 | 3.97 |
| 11.5 | 0.4 | 5.5 | 0.0 | 0.0 | 18.5 | 2.25 | 1.56 | 1.32 | 0.82 | 7.43 | 4.59 |
| 13.5 | 0.4 | 6.0 | 0.0 | 0.0 | 15.7 | 2.65 | 1.84 | 1.54 | 0.95 | 8.66 | 5.41 |
| 15.5 | 0.4 | 6.3 | 0.0 | 0.0 | 13.7 | 3.04 | 2.11 | 1.77 | 1.10 | 10.0 | 6.21 |
| 18.5 | 0.5 | 7.3 | 0.0 | 0.0 | 9.83 | 5.05 4.24 | 2.52 | 2.12 | 1.51 | 11.9 | 7.41 |
| 25.3 | 0.5 | 7.9 | 0.0 | 0.0 | 8.39 | 4.96 | 3.44 | 2.90 | 1.80 | 16.4 | 10.1 |
| 30.0 | 1.2 | 9.0 | 0.0 | 0.0 | 7.08 | 5.88 | 4.08 | 3.43 | 2.12 | 19.3 | 12.0 |
| 37.2 | 0.2 | 9.2 | 0.0 | 0.0 | 5.70 | 7.29 | 5.06 | 4.26 | 2.64 | 24.0 | 14.9 |
| 47.2 | 0.2 | 9.4 | 0.0 | 0.0 | 4.49 | 9.25 | 6.42 | 5.40 | 3.34 | 30.4 | 18.9 |
| 56.6 | 0.2 | 9.6 | 0.2 | 0.2 | 3.75 | 11.1 | 7.71 | 6.48 7.59 | 4.01 | 36.5 | 22.7 |
| 80.4 | 0.5 | 10.1 | 0.5 | 1.5 | 2.64 | 15.8 | 11.0 | 9.20 | 5 70 | 51.8 | 32.4 |
| 93.0 | 0.9 | 11.7 | 1.0 | 2.5 | 2.28 | 18.2 | 12.6 | 10.6 | 6.56 | 59.6 | 37.1 |
| 111 | 1.1 | 12.9 | 1.3 | 3.8 | 1.91 | 21.8 | 15.1 | 12.7 | 7.86 | 71.5 | 44.4 |
| 129 | 1.4 | 14.3 | 1.6 | 5.4 | 1.65 | 25.3 | 17.6 | 14.8 | 9.16 | 83.3 | 51.8 |
| 152 | 1.8 | 16.2 | 2.0 | 7.4 | 1.39 | 29.8 | 20.7 | 17.4 | 10.8 | 98.2 | 60.9 |
| 210 | 3.4 | 22.3 | 3.8 | 10.4 | 1.18 | 35.1 41.2 | 24.4 | 20.5 | 12.7 | 135 | /1.8 |
| 247 | 5.6 | 27.9 | 6.2 | 20.4 | 0.860 | 48.4 | 33.6 | 28.3 | 17.5 | 159 | 98.8 |
| 292 | 8.9 | 36.8 | 9.8 | 30.2 | 0.726 | 57.3 | 39.8 | 33.4 | 20.7 | 188 | 117 |
| 343 | 11.9 | 48.6 | 13.1 | 43.3 | 0.619 | 67.3 | 46.7 | 39.3 | 24.3 | 221 | 137 |
| 401 | 13.4 | 62.1 | 14.8 | 58.1 | 0.528 | 78.6 | 54.6 | 45.9 | 28.4 | 258 | 161 |
| 553 | 17.8 | 96.5 | 10.5 | 96.1 | 0.383 | 92.5 | 75.0 | 63.3 | 39.2 | 356 | 221 |
| 647 | 0.9 | 97.4 | 1.0 | 97.1 | 0.328 | 127 | 88.2 | 74.0 | 45.8 | 416 | 259 |
| 757 | 0.0 | 97.4 | 0.0 | 97.2 | 0.280 | 148 | 103 | 86.6 | 53.6 | 487 | 303 |
| 887 | 0.0 | 97.5 | 0.0 | 97.2 | 0.239 | 174 | 121 | 102 | 63.1 | 574 | 356 |
| 1048 | 0.1 | 97.5 | 0.1 | 97.3 | 0.202 | 205 | 142 | 120 | 74.3 | 675 | 418 |
| 1439 | 0.2 | 97.7 | 0.2 | 97.4 | 0.173 | 241 282 | 107 | 140 | 102 | 927 | 576 |
| 1688 | 0.4 | 98.4 | 0.5 | 98.2 | 0.126 | 331 | 230 | 193 | 119 | 1082 | 676 |
| 1828 | 0.2 | 98.6 | 0.2 | 98.4 | 0.116 | 358 | 249 | 209 | 129 | 1173 | 732 |
| 2142 | 0.2 | 98.8 | 0.3 | 98.7 | 0.0990 | 420 | 292 | 245 | 152 | 1382 | 859 |
| 2510 | 0.2 | 99.0 | 0.3 | 98.9 | 0.0845 | 492 | 342 | 287 | 178 | 1618 | 1006 |
| 2945 | 0.3 | 99.3 | 0.3 | 99.2 | 0.0720 | 577 | 401 | 337 | 209 | 1900 | 11/9 |
| 4040 | 0.2 | 99.8 | 0.2 | 99.7 | 0.0525 | 792 | 550 | 462 | 245 | 2600 | 1618 |
| 4728 | 0.1 | 99.9 | 0.2 | 99.9 | 0.0448 | 927 | 644 | 541 | 335 | 3045 | 1894 |
| 5114 | 0.0 | 100.0 | 0.1 | 100.0 | 0.0415 | 1003 | 697 | 585 | 362 | 3291 | 2050 |
| 6002 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0353 | 1177 | 817 | 687 | 425 | 3864 | 2403 |
| 7033 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0301 | 1379 | 958 | 805 | 498 | 4527 | 2818 |
| 8920 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0209 | 1749 | 1075 | 1021 | 632 | 5745 | 3574 |
| 9649 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0220 | 1892 | 1314 | 1104 | 683 | 6209 | 3865 |
| 10452 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0203 | 2049 | 1423 | 1196 | 740 | 6727 | 4185 |
| 12283 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0173 | 2408 | 1672 | 1406 | 870 | 7909 | 4918 |
| 14333 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0148 | 2810 | 1951 | 1640 | 1015 | 9227 | 5738 |
| 16381 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0129 | 3212 | 2231 | 18/5 | 1161 | 10555 | 6562 7403 |
| 20481 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0104 | 4016 | 2789 | 2344 | 1451 | 13191 | 8203 |
| 23149 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0092 | 4539 | 3152 | 2649 | 1640 | 14909 | 9271 |
| 25064 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0085 | 4915 | 3413 | 2868 | 1775 | 16136 | 10038 |
| 27135 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0078 | 5321 | 3695 | 3105 | 1922 | 17473 | 10868 |
| 29376 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0072 | 5760 | 4000 | 3362 | 2081 | 18918 | 11765 |
| 31804 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0067 | 6749 | 4331 4687 | 3040 | 2253 | 20482 | 12/38 |
| 37192 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0057 | 7293 | 5065 | 4256 | 2635 | 23955 | 14897 |
| 40343 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0053 | 7910 | 5493 | 4617 | 2858 | 25982 | 16156 |
| 43591 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0049 | 8547 | 5935 | 4989 | 3088 | 28073 | 17456 |
| 47291 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0045 | 9273 | 6440 | 5412 | 3350 | 30455 | 18941 |
| 55387 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0041 | 10034 | 0908 7542 | 5856 | 3625 | 32933 | 20494 |
| 59880 | 0.0 | 100.0 | 0.0 | 100.0 | 0.0035 | 11741 | 8153 | 6853 | 4242 | 38564 | 23979 |



(B) Capillary Pressure Plot



(C) Pore Size Distribution plot

Appendix 3

Values used in the calculation of $\mathrm{CO}_{\rm 2}$ column heights

| | Sample | | | At sample depth | | CO ₂ | Interfacial | Brine | Threshold | CO ₂ |
|-------------------------|---------|----------|--------------------------|-----------------|---------------|----------------------|-------------|---------|--------------|-----------------|
| Well | Depth | Core/SWC | Formation | Temperature | Pore pressure | Density | Tension | Density | Pressure | column |
| | (m) | | | (°C) | (MPa) | (g/cm ³) | (mN/m) | (g/cm³) | Air-Hg (psi) | height (m) |
| Barracouta-1 | 1021.95 | Core | Lakes Entrance Formation | 58.3 | 10.26 | 0.3205 | 30.52 | 1.0179 | 3001 | 250 |
| Bengworden South-6 | 914.9 | Core | Lakes Entrance Formation | 59 | 8.96 | 0.2372 | 34.53 | 0.9978 | 3248 | 282 |
| Bundalaguah-10 | 599.8 | Core | Gippsland Limestone | 34 | 5.87 | 0.1551 | 38.85 | 1.0077 | 467 | 41 |
| Cod-1 | 1711.89 | Core | Lakes Entrance Formation | 71.1 | 17.25 | 0.58 | 26.92 | 1.0144 | 5787 | 683 |
| Colquhoun East-6 | 180.7 | Core | Lakes Entrance Formation | 24 | 1.77 | 0.0349 | 59.7 | 1.0032 | 1389 | 164 |
| Dulungalong-2 | 478.1 | Core | Lakes Entrance Formation | 36 | 4.68 | 0.1065 | 45.74 | 1.0048 | 806 | 78 |
| Flounder-6 | 1929.38 | SWC | Lakes Entrance Formation | 86.6 | 19.29 | 0.5319 | 27.1 | 1.0053 | 4223 | 460 |
| Fortescue-2 | 2420 | Core | Lakes Entrance Formation | 104 | 24.22 | 0.5561 | 25.78 | 0.9781 | 3636 | 425 |
| Fortescue-2 | 2430 | Core | Gurnard Formation | 104 | 24.33 | 0.5582 | 25.76 | 0.9781 | 2587 | 303 |
| Fortescue-3 | 2411.5 | Core | Lakes Entrance Formation | 100.5 | 24.12 | 0.5679 | 25.91 | 0.9982 | 5634 | 641 |
| Gippsland Frome Lakes-4 | 503.5 | Core | Lakes Entrance Formation | 42 | 4.93 | 0.1092 | 45.85 | 1.0022 | 185 | 18 |
| Gippsland Frome Lakes-4 | 506.6 | Core | Lakes Entrance Formation | 42 | 4.96 | 0.1101 | 45.71 | 1.0023 | 1228 | 120 |
| Golden Beach West-1 | 667.68 | Core | Lakes Entrance Formation | 30.6 | 6.64 | 0.2133 | 32.82 | 1.0288 | 1138 | 87 |
| Goon Nure-9 | 726.3 | Core | Lakes Entrance Formation | 35 | 7.11 | 0.2302 | 32.25 | 1.0089 | 2686 | 213 |
| Groper-1 | 909.15 | Core | Lakes Entrance Formation | 62 | 9.12 | 0.2347 | 34.89 | 0.9961 | 2807 | 246 |
| Groper-1 | 926.1 | Core | Lakes Entrance Formation | 63.9 | 9.29 | 0.2357 | 34.94 | 1.0154 | 347 | 29 |
| Groper-1 | 932 | Core | Lakes Entrance Formation | 64.2 | 9.35 | 0.2385 | 34.78 | 1.0154 | 285 | 24 |
| Groper-2 | 747.86 | Core | Lakes Entrance Formation | 60.7 | 7.48 | 0.171 | 39.69 | 1.0157 | 151 | 13 |
| Hunters Lane-1 | 377 | Core | Lakes Entrance Formation | 31.2 | 3.74 | 0.0815 | 49.65 | 1.0265 | 182 | 18 |
| Kingfish-3 | 2143.05 | Core | Lakes Entrance Formation | 85.2 | 21.62 | 0.6003 | 26.59 | 1.0097 | 3730 | 463 |
| Meerlieu-4 | 722 | Core | Lakes Entrance Formation | 46.6 | 7.07 | 0.1828 | 37.53 | 1.0028 | 2131 | 186 |
| Meerlieu-4 | 769 | Core | Lakes Entrance Formation | 44 | 7.53 | 0.2152 | 34.56 | 1.0048 | 3602 | 301 |
| Meerlieu-15001 | 699.9 | Core | Lakes Entrance Formation | 53 | 6.85 | 0.1611 | 40.19 | 0.999 | 1033 | 95 |
| Mullungdung-7 | 363 | Core | Lakes Entrance Formation | 19 | 3.55 | 0.0833 | 47.72 | 1.0099 | 126 | 12 |
| Sale-13 | 748.1 | Core | Lakes Entrance Formation | 53 | 7.33 | 0.1795 | 38.42 | 0.9995 | 1922 | 172 |
| Sale-13 | 795.6 | Core | Lakes Entrance Formation | 51 | 7.79 | 0.2054 | 36.06 | 1.0012 | 1962 | 170 |
| Sale-15 | 628.6 | Core | Gippsland Limestone | 35.4 | 6.16 | 0.1657 | 37.86 | 1.0075 | 620 | 53 |
| Seacombe-7 | 947.6 | Core | Lakes Entrance Formation | 61 | 9.28 | 0.2459 | 34.15 | 0.9969 | 3520 | 306 |
| Sole-1 | 805.9 | SWC | Lakes Entrance Formation | 43 | 8.07 | 0.2594 | 31.64 | 1.0059 | 666 | 54 |
| Sperm Whale Head-1 | 653.8 | Core | Lakes Entrance Formation | 40.8 | 6.4 | 0.1649 | 38.67 | 1.005 | 2229 | 196 |
| Sperm Whale Head-1 | 718.1 | Core | Lakes Entrance Formation | 44 | 7.03 | 0.1877 | 36.8 | 1.0042 | 3241 | 285 |
| Tuna-1 | 1160 | Core | Lakes Entrance Formation | 57.8 | 11.66 | 0.4326 | 27.86 | 1.0207 | 3192 | 289 |
| Woodside South-1 | 522.12 | Core | Lakes Entrance Formation | 31.2 | 5.25 | 0.1329 | 41.23 | 1.029 | 65 | 6 |
| Wooundellah-10 | 389.3 | Core | Gippsland Limestone | 36 | 3.81 | 0.0809 | 50.17 | 1.0032 | 43 | 4 |
| Wooundellah-11 | 389 | Core | Gippsland Limestone | 36 | 3.81 | 0.0808 | 50.19 | 1.0032 | 112 | 11 |
| Wrasse-1 | 2589.89 | Core | Lakes Entrance Formation | 109 | 26.05 | 0.5674 | 25.16 | 0.9754 | 8025 | 947 |
| Wurruk Wurruk-13 | 584.9 | Core | Lakes Entrance Formation | 36 | 5.73 | 0.1449 | 40.34 | 1.0065 | 234 | 21 |

Corrected temperature gradient from GeoScience Victoria database. Onshore surface temperature =13°C onshore.

Offshore well temperature calculated from database TD gradient (horner plot corrected temperature based on inspection of multiple temperature measurements).

Pore pressure calculation for onshore wells estimated from depth without correction for RT or KB and assuming freshwater pore fluid density. Pressure gradient = 0.433 psi/ft.

Offshore wells depth is corrected for KB elevation and seawater composition is assumed for the pore water density. Pressure gradient = 0.448 psi/ft.

 CO_2 density from CO2CRC website calculator. Assumed reservoir entry pressure = 0.28 psi.